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The Company Announcements Office, ASX Limited

2 August, 2023

Ashburton Magnetite, Pilbara

CZR to run strategic partner process amid surging demand for high-quality magnetite

Strategy to unlock value of Ashburton Magnetite deposit follows completion of study which reveals potential for a large, long-life magnetite concentrate project, suitable for low carbon emission steel production

- CZR's Ashburton Magnetite deposit is an 11km long, outcropping magnetite schist, located only 20km north of CZR's Robe Mesa DSO project and 50km south of Citic Pacific's Sino Iron magnetite mine
- An extensive technical review completed by CZR has found Ashburton has the potential to become a substantial deposit, capable of producing high-quality magnetite concentrate
- Ashburton is strategically located close to critical energy, water and transport infrastructure
- The drilling, which took place from 2014-2016, included 29 reverse circulation (RC) and 3 diamond drill holes for 7,349m, intersecting extensive magnetite mineralisation
- Comprehensive Davis Tube Recovery (DTR) and bench-scale magnetic separation test work has been completed on drill hole samples, with concentrates reporting + 65% Fe on a mass yield ranging from 26 to 39% from magnetite separation (Appendix D)
- CZR undertook the review following inbound inquiries from steel makers seeking high-grade magnetite concentrate to fuel the growing demand for magnetite due to its suitability for low-carbon emission steel production
- The review has resulted in an **Exploration Target of 450Mt – 880Mt at 24-30% Fe**, generating a **magnetite concentrate of 65-68% Fe at a 25-30% mass yield**, based on geological modelling of drill holes to a depth of 200m, guided by magnetic and gravity data and metallurgical test work
- The Exploration Target is based on the information detailed in this announcement. The potential quantity and grade is conceptual in nature and there has been insufficient work completed to estimate a Mineral Resource. It remains uncertain that further exploration will result in the estimation of a Mineral Resource
- In light of the outstanding results of the technical review, CZR has initiated a strategic partner process to canvass joint venture and other opportunities to unlock the value of the Ashburton magnetite deposit for CZR shareholders

CZR Resources Ltd (ASX: CZR) is pleased to announce that following a highly successful technical review of its Ashburton Magnetite deposit in WA's Pilbara, it has initiated a strategic partnership process aimed at unlocking the value of this asset in a timely manner.

The review has resulted in a significant Exploration Target of 450Mt – 880Mt at 24-30% Fe, demonstrating the potential for a large, long-life project than can produce high-quality magnetite concentrate.

CZR Managing Director Stefan Murphy said: "The company is excited to release the findings from this technical review, which draws attention to significant potential of the Ashburton Magnetite deposit.

"Drilling has already confirmed the large scale of the deposit and preliminary metallurgical testwork confirms that the iron-bearing rocks are suitable for producing high grade magnetite concentrate.

"Magnetite's suitability for production of low emissions steel means its time has come. Given the size of the project and its potential to create substantial value for CZR shareholders, we have initiated a process to consider a range of strategic and joint venture partnership options to advance Ashburton.

"While the company remains focussed on delivering the Robe Mesa iron ore DFS and bringing the project into production, Ashburton has the scale and future-facing attributes required for long-term company growth.

"Given the continued strength of the iron-ore price and the global shift towards decarbonisation solutions, it is clear that the investment case for CZR Resources remains strong".

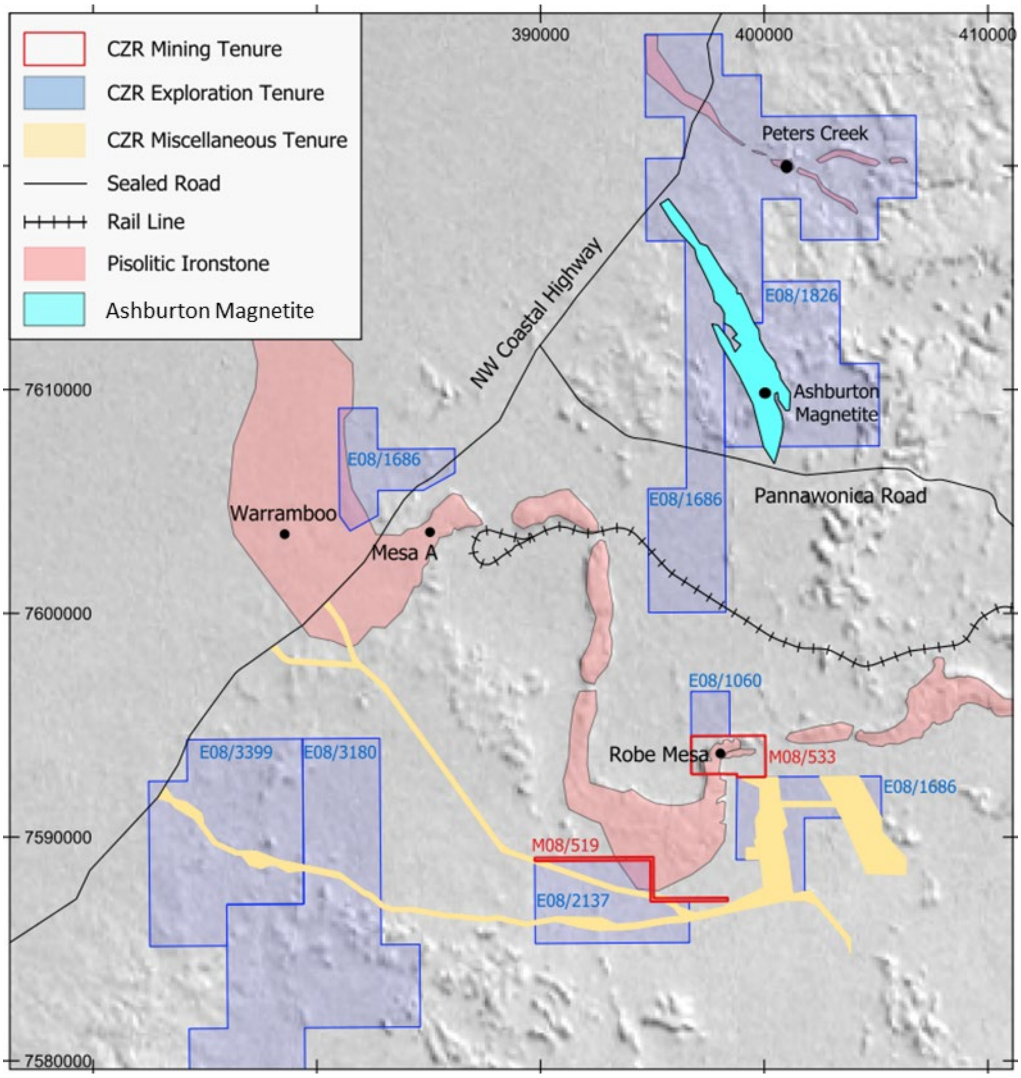

Figure 1. Yarraloola Project showing location of the Ashburton Magnetite deposit

Table 1. Exploration Target summary[1]

	Tonnage Range		Fe Grade Range	
Domain	**Tonnes - Upper**	**Tonnes - Lower**	**% Fe - Upper**	**% Fe - Lower**
A	264	198	31.6	25.8
B	299	179	28.8	23.6
D	138	55	27.9	22.9
C[2]	179	18		
	880	**450**	**29.7**	**24.3**

1. Refer to Geological Interpretation section and Table 3 for a detailed description of the Exploration Target
2. No grade allocated to Domain C as there is no drilling – based on magnetic and gravity interpretation

Technical Review

Extensive drilling, geophysical surveys and metallurgical test work was completed on the Ashburton Magnetite deposit between 2014 and 2019 (refer to Appendix A), which highlighted the conceptual size and high-quality magnetite concentrate that could be produced from the project.

Based on the extensive data set and geological modelling completed by CZR geologists, an Exploration Target of 450-880Mt has been generated for the Ashburton magnetite deposit. The tonnage range was derived from full realisation of the modelled domains (upper tonnes) and a down-side risk-weighted average for the lower tonnes. A +10% and -10% factor was applied to the modelled grade for each domain to derive the grade range of 24-30% Fe (Table 3)

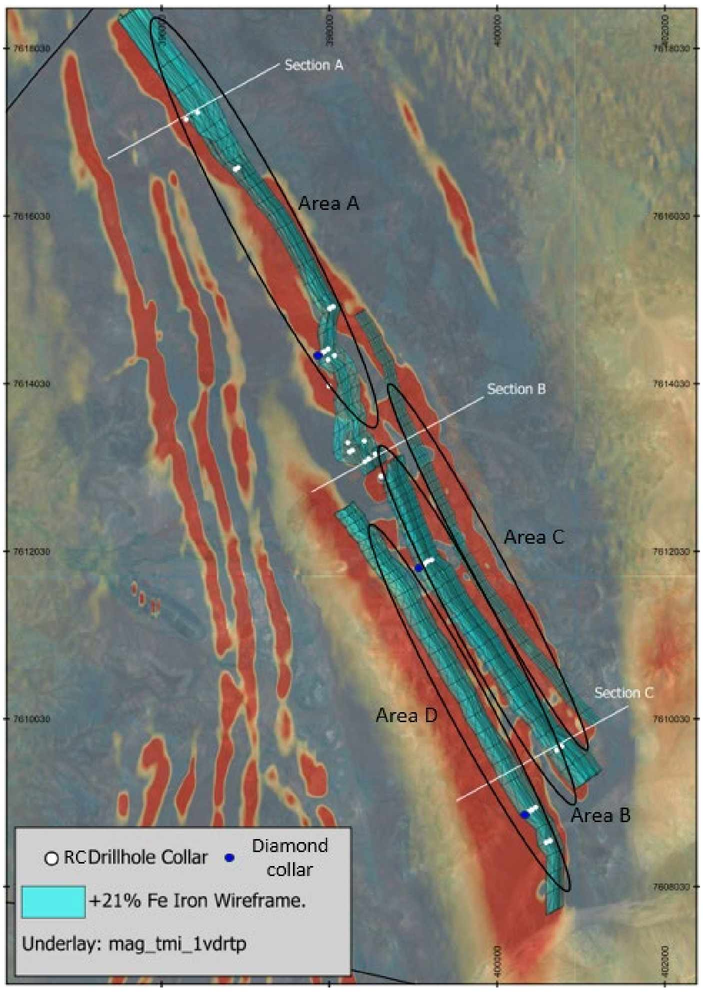

Figure 2. Geological interpretation and domains of the Ashburton magnetite deposit, showing drill holes and magnetics

A review was completed of all historical work on Ashburton, with a particular focus on assessing the potential to produce 4-5Mtpa of high quality magnetite concentrate over +20 years (approx. 400Mt with a mass yield of +25%). CZR geologists modelled four distinct domains, based on magnetic/gravity response over 11km and 7,349m of RC and diamond drilling. The domains were modelled down to a depth of 200m below surface, using a 21% Fe cut-off to achieve an average magnetite mass yield of +25%, based on metallurgical test work already completed on the Ashburton magnetite deposit.

The geological modelling generated 880Mt at 27% Fe from the four domains, using density measurements taken from the Ashburton magnetite deposit (Table 2). The Exploration Target range was derived by applying a risk factor to the individual domains based on drilling density. The modelled grade of 27% Fe was derived from the weighted average of drill hole intercepts within each individual domain. The grade range was derived by applying a +10% and -10% factor to the modelled grade.

In addition to the RC and diamond drilling on the Ashburton magnetite deposit, CZR also completed two phases of metallurgical test work in 2016, comprising Davis Tube Recovery (DTR), magnetic separation and mineralogical assessment of RC and diamond core samples. The results showed that the project can produce a high quality, +65% Fe magnetite concentrate at high mass recovery rates of 26-39% (refer to below Metallurgy section for additional details).

Given the large size of the Exploration Target and positive metallurgical results, CZR has designed an exploration program to drill the deposit on a 200m x 100m grid to generate a maiden Mineral Resource estimate. Approximately 285 RC and 10 diamond drill holes are initially planned, with the diamond core to provide additional geotechnical and metallurgical core samples.

With CZR's immediate focus on delivering the Robe Mesa DFS, the company has formalised a strategic partner process, seeking joint venture funding and/or partial acquisition proposals to fund development of the Ashburton Magnetite deposit and which will determine the timeframe of these works being completed.

Overview

The Ashburton Magnetite deposit is part of CZR's Yarraloola tenement suite in the West Pilbara region of Western Australia. The deposit contains magnetite bearing rocks of the Shingle Creek Group and have a strong magnetic signature outlining a 11km long and 1km wide airborne magnetic anomaly.

The prospect is only 20km to the north of CZR's flagship Robe Mesa deposit, which hosts a Channel Iron Deposit (CID) iron ore reserve of 27 million tonnes and currently the subject of a definitive feasibility study.

There has been extensive exploration activity on the Ashburton Magnetite deposit, mostly between 2016-2017 (Appendix A) inclusive of geophysical surveys, RC drilling, diamond drilling and subsequent metallurgical test work. CZR's focus on the Yarraloola tenements has been on developing the Robe Mesa deposit and as such there has been limited work completed at Ashburton in recent years.

Currently in Australia and across the globe there is a strong focus on decarbonisation and reducing fossil fuel emissions. The steel making industry, which is a contributor of carbon emission through traditional steel making processes utilising blast furnaces, is not exempt from this.

DRI (Direct Reduced Iron) processing as an alternative to traditional blast furnace processing, has been recognised as a primary opportunity in the transition to a sustainable steelmaking route. DRI involves the removal of oxygen from iron-ore through a reducing agent, such as natural gas or hydrogen, rather than smelting in the blast furnace. When paired with hydrogen as a reducing agent, produced through renewable energy, the DRI method has a significantly lower emission footprint compared to the current dominant method.

DRI requires higher grade iron ore to be effective, meaning that traditional direct shipping iron ore (rich in goethite and haematite) are not considered a suitable feed source. Magnetite ore, characterized by much higher iron content, is favoured for DRI processing. It is apparent that the supply of higher-grade iron ore, such as magnetite, is going to be a crucial part of the global shift towards decarbonisation and investment in magnetite exploration and development is crucial. For this reason, CZR decided to review the potential of the Ashburton Magnetite deposit as a future source of high-quality magnetite concentrate.

Exploration Summary

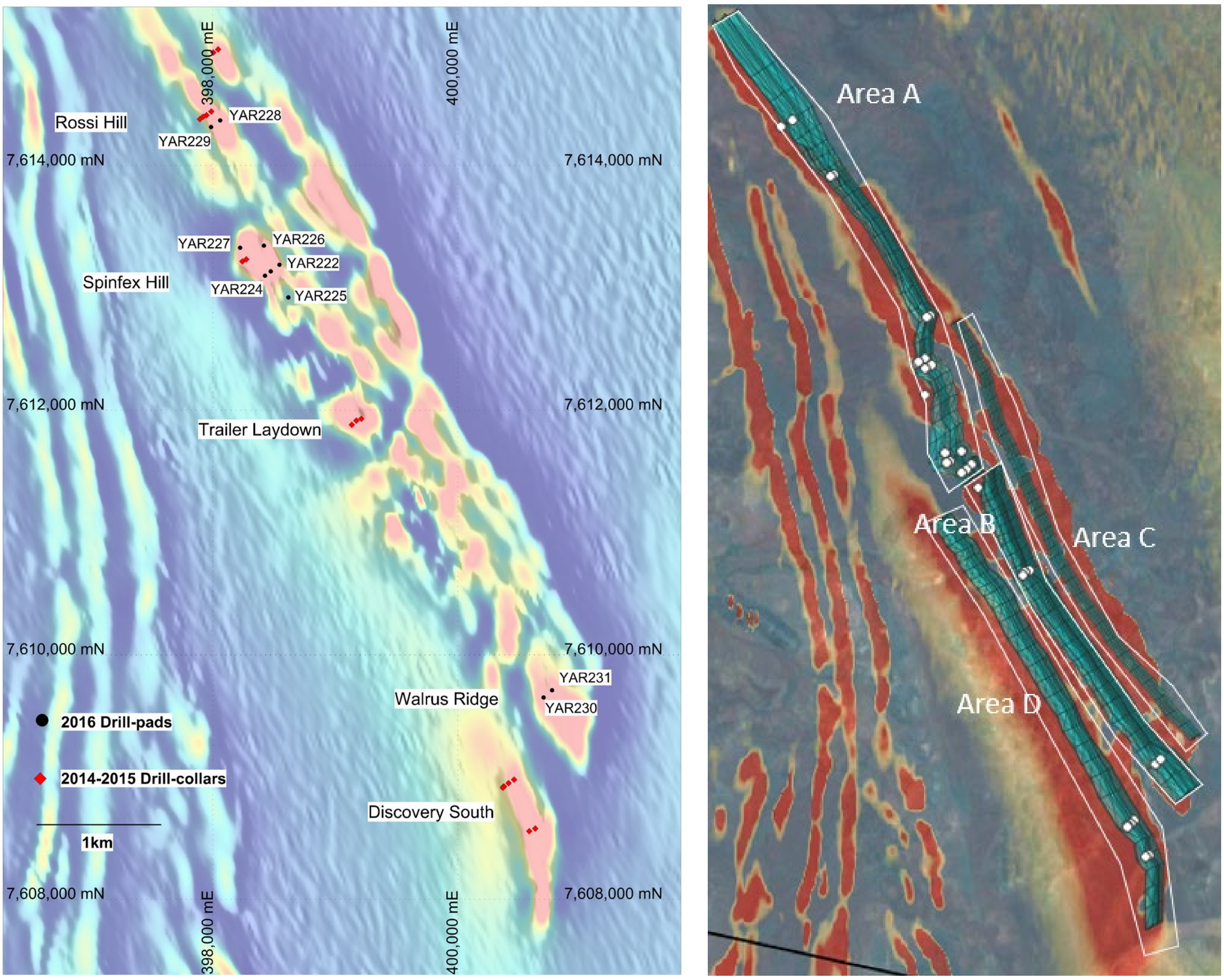

Figure 3. Left: RC drill-collar locations into the magnetite-bearing sequence from the Ashburton deposit overlain on magnetic imagery. Right: Wireframed mineralisation (Domains A-D) used to estimate the Exploration Target over magnetics

Geophysical Programs

CZR commissioned an aeromagnetic survey flown by UTS Geophysics in 2006. The survey included 50m line spacing covering almost all the Yarraloola tenements, including the full extents of Ashburton. In 2013 Spinifex Geophysics was engaged to complete a data review and some inversion modelling of magnetic features and in 2014/2015, Resource Potentials completed data processing and some additional magnetic inversion modelling of the available datasets for Ashburton Magnetite area. Results of the magnetic modelling was used to design and implement the 2014-15 drill program.

A ground-based gravity and passive seismic survey was completed in 2019 by Atlas Geophysics. The survey included 1,530 gravity stations achieving a 100m spacing across and along 8km strike of the Ashburton Magnetite deposit. 151 passive seismic stations were also completed, representing 5 lines along the deposit with stations spaced 100m across the strike.

Drilling Summary

There has been 29 RC drillholes drilled into the Ashburton deposit with an average depth 200m for a total of 5,778m (refer to Appendix A for previous ASX announcements). All of the holes were drilled at an inclined ~50° angle and most holes were orientated with a 050 azimuth across strike of the ore body. All holes were sampled at 1m intervals and assayed for extended suite of elements through XRF method. RC drilling along strike is sparse compared to orebody extent outlined in magnetic feature, although RC holes on same line have been spaced 50m across strike. All significant intercepts are listed in Appendix B.

3 Diamond holes average depth 523 for a total of 1571m. Inclined ~50 with a 050 azimuth across strike of the ore body. The diamond holes do not twin RC holes and whilst limited assays have been determined, the primary objective of the core was for metallurgical test work and assessment.

The magnetite-rich rocks are fine grained and range from finely laminated to bedded with magnetic susceptibility ranging from 5,000 to 60,000 SI units (Fig 4). Magnetite is typically laminated with quartz, sericite and chlorite but some samples contain an abundance of carbonate or traces of garnet. The quartz and carbonate are generally distributed as an interstitial matrix to the magnetite but in some samples there are well rounded grains that are typical of detrital material.

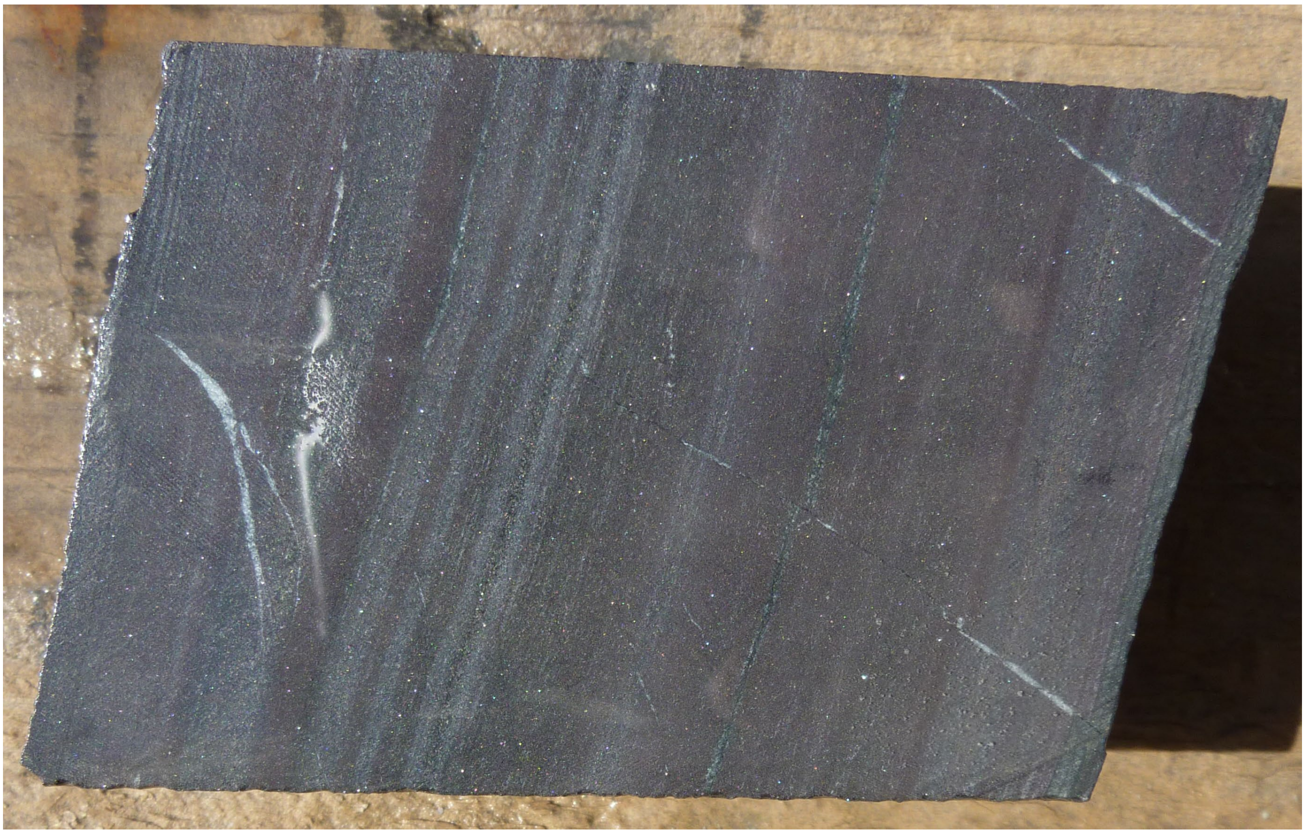

Figure 4. Half-NQ drill core through laminated iron-formation from YARDDH002 at 398.7m high lighting darker oxide-rich and leucocratic oxide-poor laminae.

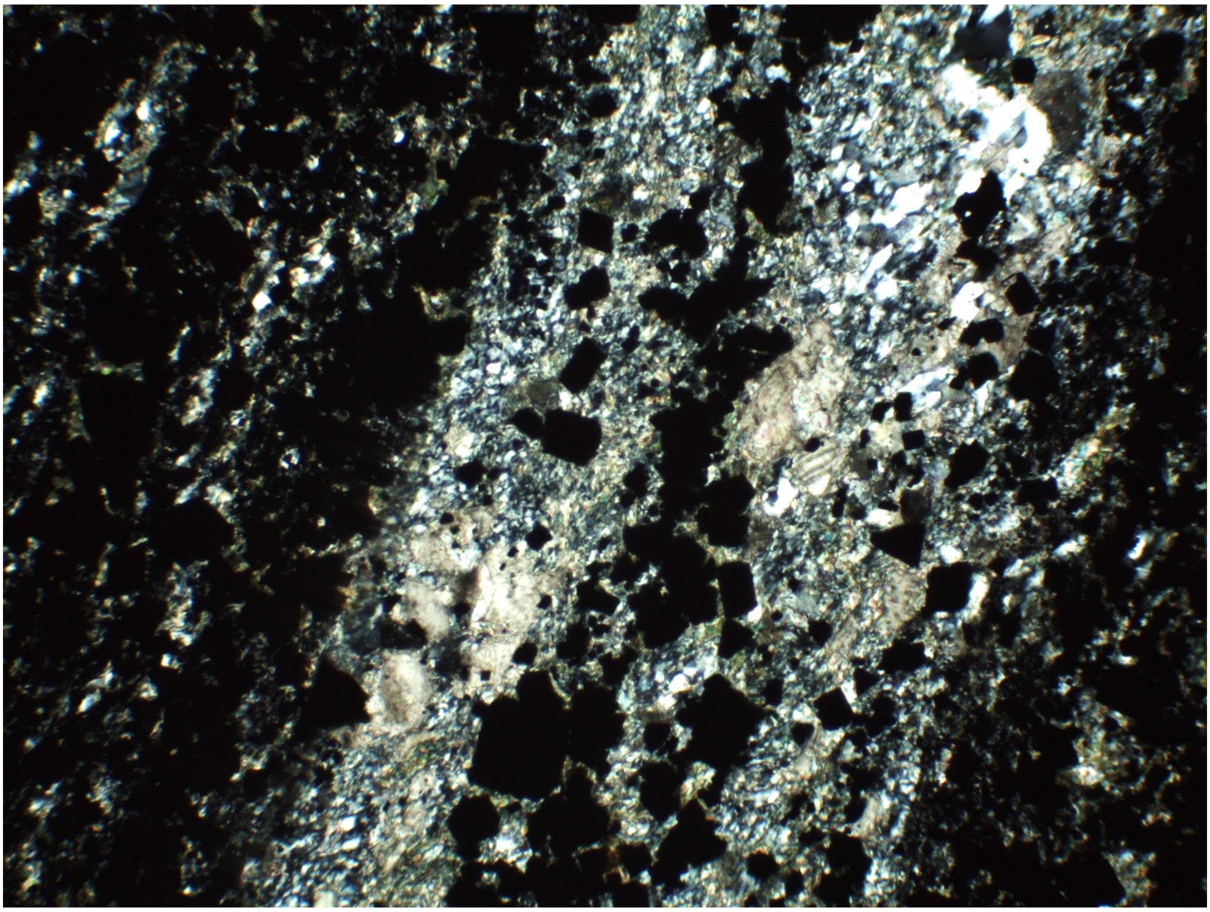

Figure 5. Photomicrograph of the laminated iron-formation showing magnetite euhedra supported by a matrix of carbonate (pale pinkish grey), quartz and mica

Metallurgy

Density

In 2015 CZR completed three 500-metre drillholes, with each drillhole intersecting a sequence of magnetite-rich siliciclastic sediments dipping steeply to the west and striking north-west. The drill core was geologically logged and cut in half for sampling, prior to being submitted to the Geological Survey of Western Australia (GSWA) Core Library in Perth.

Table 2: Summary of rock density measurements from the Ashburton Magnetite Prospect

Rock Type	Average Density	Sample Count	Sampling Frequency
Large (>20cm) magnetite band	3.8	2	Discrete samples
Chert-magnetite banding	3.3	35	Every 5 metres
Magnetite-chlorite-chert schist	3.27	10	Every 5 metres
Chlorite-magnetite schist	2.85	6	Every 5 metres
Chert	2.8	5	Every 10 metres
Chlorite schist	2.75	15	Every 10 metres

The mineralised domains predominantly host chert-magnetite banding and magnetite-chlorite-chert schist, with the Exploration Target using an average density of 3.27 (Magnetite-chlorite-chert schist equivalent).

Metallurgical Test work

DTR test work was completed on 5m composite samples by collecting 1-2kg of representative material from the 1 metre RC drill-bags that report magnetic susceptibility greater than 10,000 SI units. These were processed at Bureau Veritas Laboratories in Perth using the grind-size optimisation parameters to produce a standard -38 micron product. A high proportion of the samples report a mass-recovery greater than 10%, SiO_2 less than 5% and Fe greater than 66%, the target for DRI magnetite concentrate feed.

A summary of the DTR results are presented in Appendix C (refer to Appendix A for previous ASX announcements)

Following the DTR test work, Engenium Limited was contracted to prepare and supervise a metallurgical programme on three exploratory diamond-drill holes into the Ashburton Magnetite Prospect. The half-core was jaw crushed to -19 mm, then riffle split into sub-samples for Abrasive Index, grind size optimisation, Bond Work Index, Davis Tube recovery and Wet LIMS (Low Intensity Magnet Separation) tests.

Grind size optimisation samples were crushed to six different target p80 sizes (125, 90, 63, 45, 38 and 28µm) and analysed by DTR to determine the best grind size for Bond Work Index and Wet LIMS.

A two-stage LIMS programme was undertaken on the four diamond-core samples (drilled 2015). The first stage was a grind to a P80 of 45µm, followed by rougher LIMS at 1000 Gauss field strength and this was followed by a regrind of the rougher LIMS concentrate to a P80 of 20 µm, followed by two stages of cleaner LIMS. Both stages used three passes of concentrate through the LIMS machine, with all concentrates reported Fe > 65% on a mass yield ranging from 26 to 39%.

A summary of the LIMS results are presented in Appendix D (refer to Appendix A for previous ASX announcements).

Geological Interpretation

Wireframe modelling was undertaken on the Ashburton Magnetite deposit with the primary objective of establishing the size potential of the prospective lithology. The wireframing was completed with Surpac modelling software and incorporated all the available RC drillholes, which have complete assay information at 1m intervals. Wireframes were created by digitising control strings between intercepts and then using triangulation tools to create solids.

Fe % was used as the attribute to guide the wireframe creation with histogram analysis of the dataset suggesting that 21% was an appropriate cut-off grade. Digitising within sections, with drillholes closely spaced on the same lines, allowed for general trend and dip to be established with the strike N-NW and dipping steeply (70-80 degrees) to the W-SW. For the along strike extensions, where drilling was limited, interval width was projected to the halfway point between drill-lines along strike of the magnetic high feature detailed in the aeromag dataset. This approach is validated by drill lines on the northern and southern extent of the magnetic feature, which both intercept the iron rich unit.

All mineralisation is open at depth but wireframes have been projected to -100m RL to represent a 200m deep potential open pit mining extent.

Preliminary assessment of the drilling has resulted in the deposit being broken down into 4 segments, named as Domain A – D, based upon the number of iron rich lodes. Whilst all the iron rich lodes appear to demonstrate the same structure, the number of lodes intercepted varies across the deposit as follows:

- Domain A: Two separate lodes. Thinner and not as steep as centre of deposit
- Domain B: Four Separate lodes. Thick intercepts up to 100m downhole width. 70-80 degree dip
- Domain C: One lode
- Domain D: Two Separate lodes

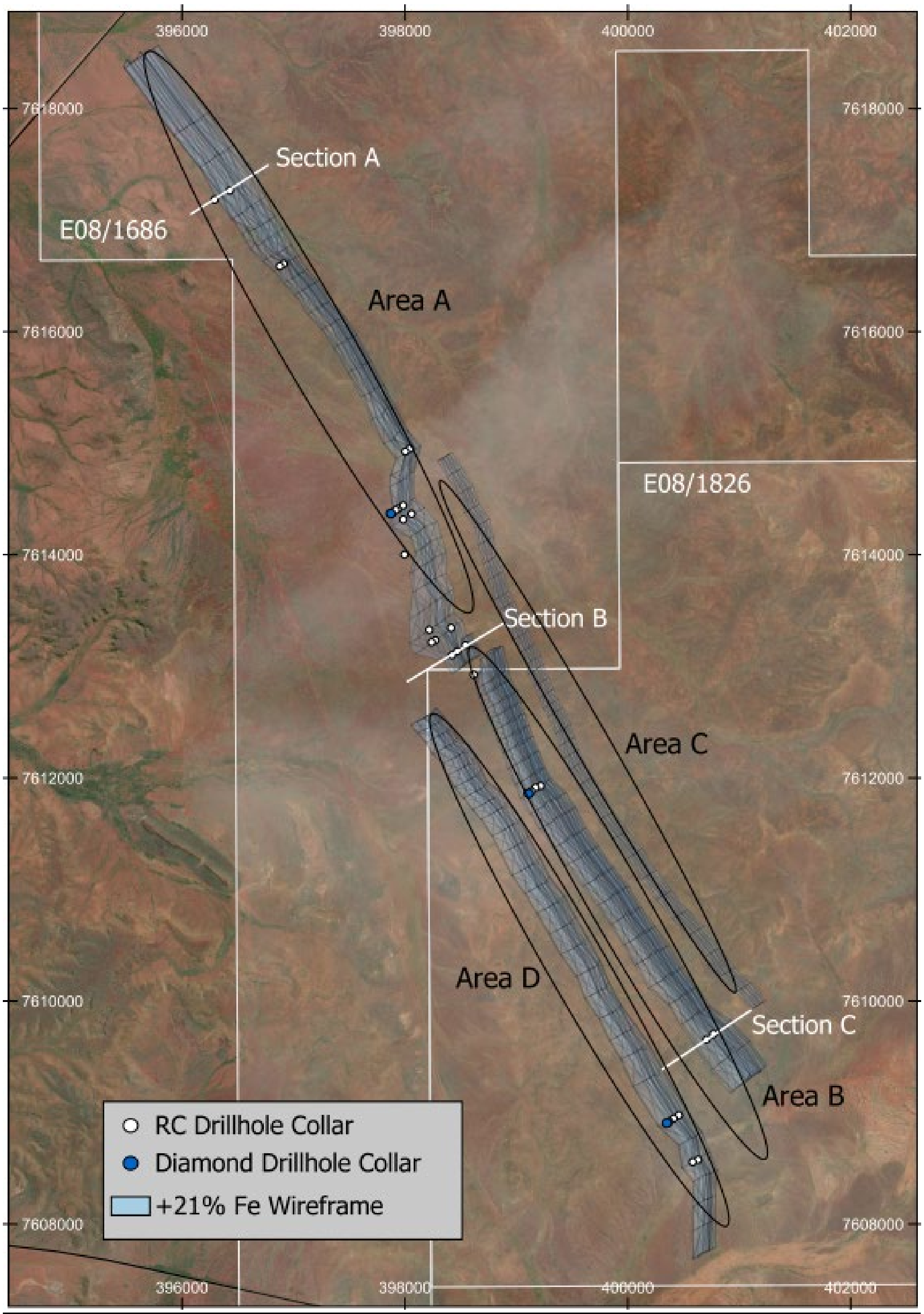

Figure 6. Geological interpretation and domains of the Ashburton magnetite deposit, showing cross section locations

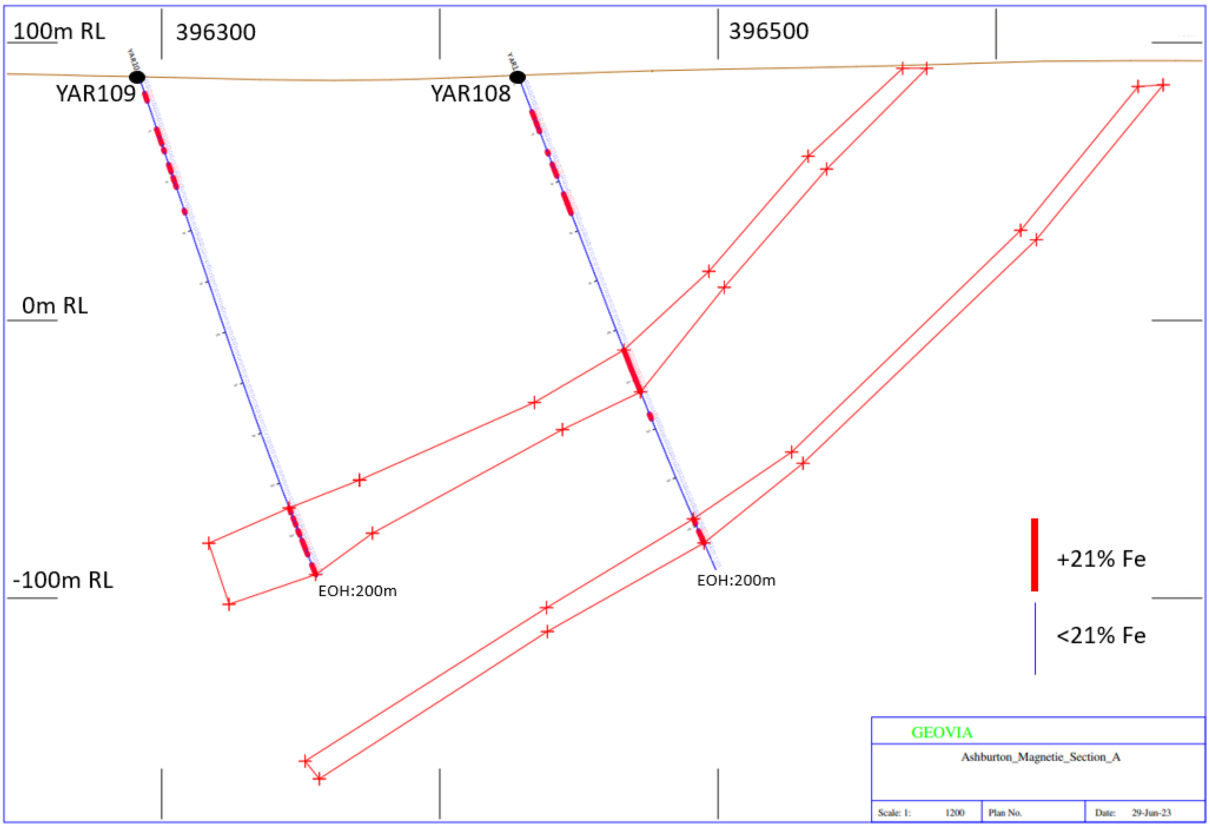

Figure 7a. Cross section A.

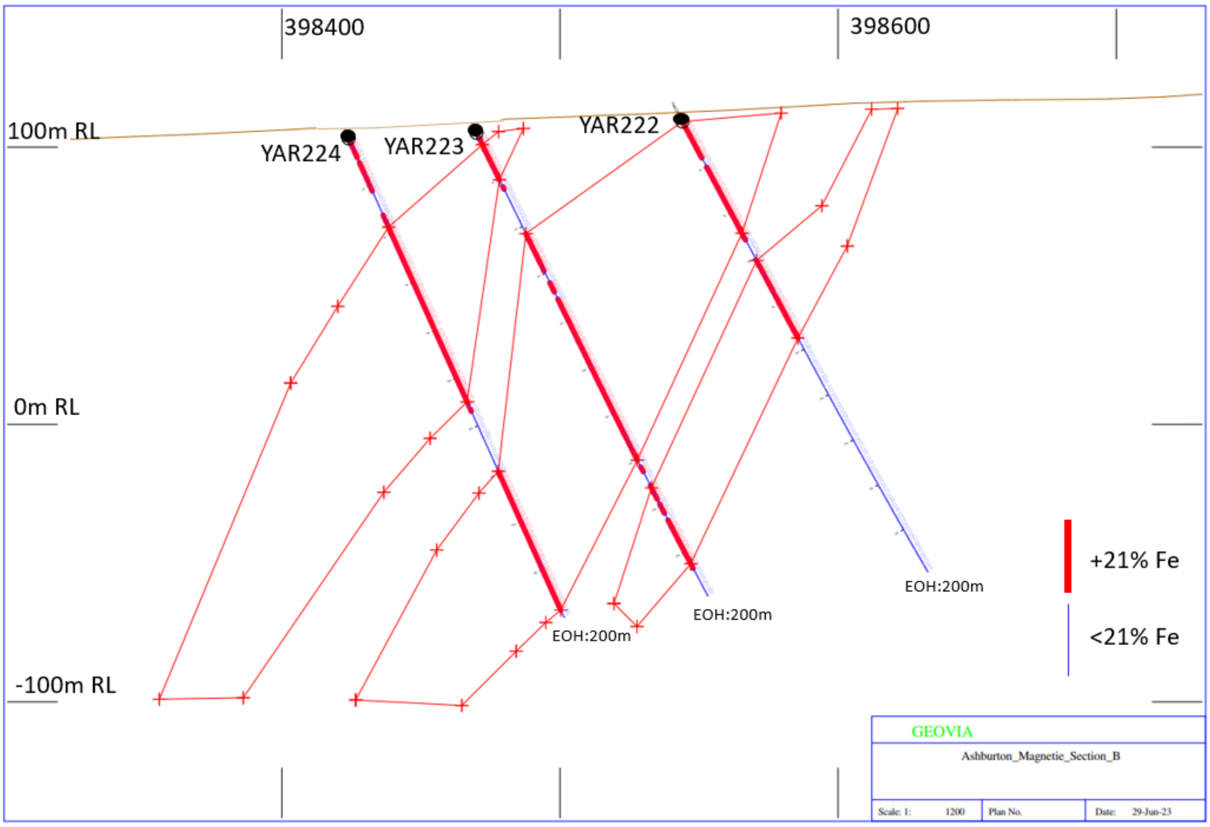

Figure 7b. Cross section B.

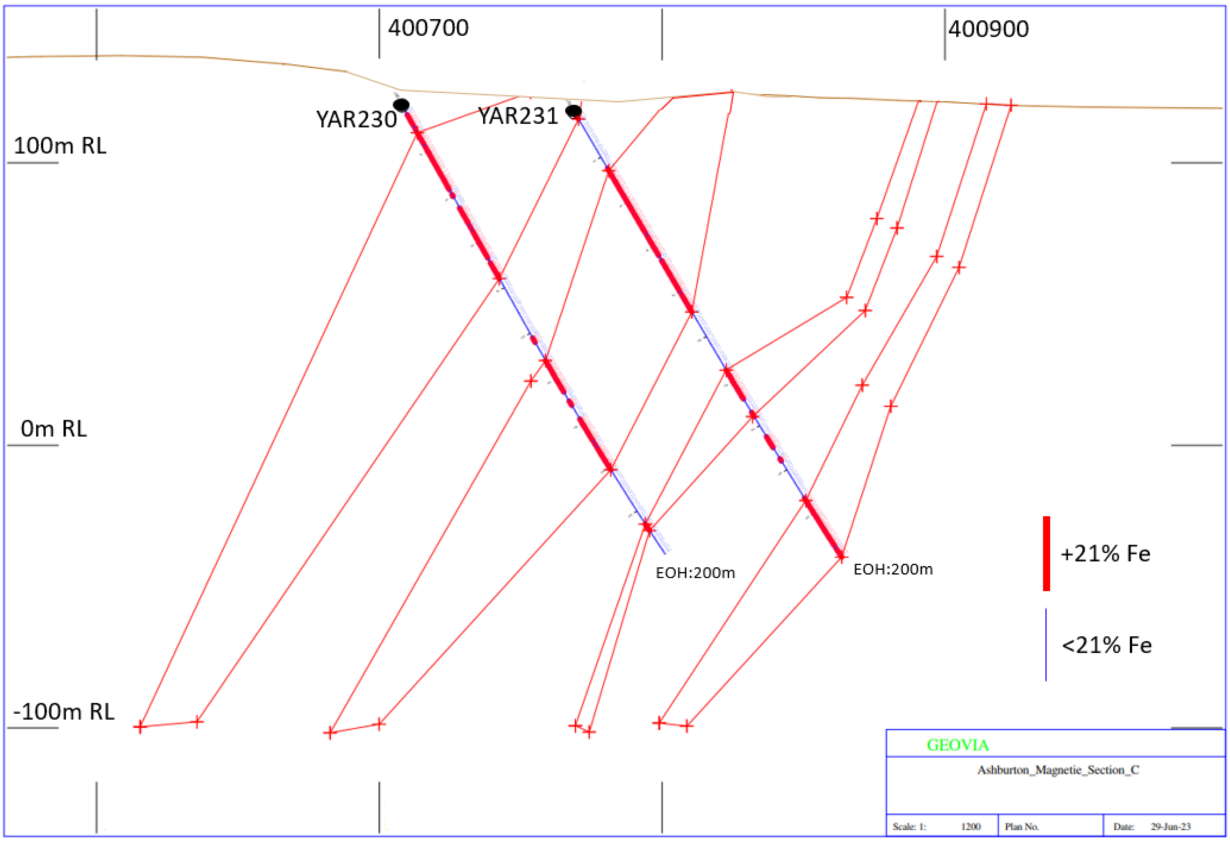

Figure 7c. Cross section C.

The wireframe solids were validated to ensure that all edges were closed, and no overlapping was occurring. The volumes of the solids were then calculated through Surpac algorithms and the results were input into an excel worksheet. The volumes were recorded as bulked cubed meters (bcm).

The grade for the wireframe solids were calculated by taking a weighted average of all the 1m grade intervals which occurred within the wireframe extent for each domain. Domain A to the north has the highest drilling density, and subsequently more downhole grade composites with 1,507. Domain B and D contained 496 and 254 composites respectively. Domain C does not contain any RC drillholes and subsequently a grade was not calculated. The results are shown in the table below, with the grade of the total deposit weighted averaged by the volume of each area.

Table 3: Exploration Target grade - tonnage summary

Ashburton Magnetite >21% Fe Wireframe.								
Domain	**Volume**	**Density**	**Modelled Tonnes**	**Downside Risk %**	**Downside Tonnes**	**Fe %**	**SiO2 %**	**Al2O3 %**
A	80,827,676	3.27	264,306,501	75%	198,229,875	28.7	47.1	3.3
B	91,335,731	3.27	298,667,840	60%	179,200,704	26.2	49.9	4.0
D	42,343,293	3.27	138,462,568	40%	55,385,027	25.4	50.8	4.3
C	54,854,075	3.27	179,372,825	10%	17,937,283			
	269,360,775	3.27	880,809,734	51%	450,752,889	27.0	49.0	3.8
			Upper Grade	10%		29.7	44.1	3.4
			Lower Grade	-10%		24.3	53.9	4.1

This announcement is authorised for release to the market by the Board of Directors of CZR Resources Ltd.

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Forward Looking Statements

This announcement contains "forward-looking information" that is based on CZR's expectations, estimates and projections as of the date on which the statements were made. This forward-looking information includes, among other things, statements with respect to CZR's business strategy, plan, development, objectives, performance, outlook, growth, cashflow, projections, targets and expectations, mineral resources, ore reserves, results of exploration and related expenses. Generally, this forward looking information can be identified by the use of forward-looking terminology such as 'outlook', 'anticipate', 'project', 'target', 'likely', 'believe', 'estimate', 'expect', 'intend', 'may', 'would', 'could', 'should', 'scheduled', 'will', 'plan', 'forecast', 'evolve' and similar expressions. Persons reading this announcement are cautioned that such statements are only predictions, and that CZR's actual future results or performance may be materially different. Forward-looking information is subject to known and unknown risks, uncertainties and other factors that may cause CZR's actual results, level of activity, performance or achievements to be materially different from those expressed or implied by such forward-looking information.

Forward-looking information is developed based on assumptions about such risks, uncertainties and other factors set out herein, including but not limited to general business, economic, competitive, political and social uncertainties; the actual results of current exploration activities; conclusions of economic evaluations; changes in project parameters as plans continue to be refined; future prices and demand of iron and other metals; possible variations of ore grade or recovery rates; failure of plant, equipment or processes to operate as anticipated; accident, labour disputes and other risks of the mining industry; and delays in obtaining governmental approvals or financing or in the completion of development or construction activities. This list and the further risk factors detailed in the remainder of this announcement are not exhaustive of the factors that may affect or impact forward-looking information. These and other factors should be considered carefully, and readers should not place undue reliance on such forward-looking information. CZR disclaims any intent or obligations to revise any forward-looking statements whether as a result of new information, estimates, or options, future events or results or otherwise, unless required to do so by law.

Statements regarding plans with respect to CZR's mineral properties may contain forward-looking statements in relation to future matters that can only be made where CZR has a reasonable basis for making those statements. Competent Person Statements regarding plans with respect to CZR's mineral properties are forward looking statements. There can be no assurance that CZR's plans for development of its mineral properties will proceed as expected. There can be no assurance that CZR will be able to confirm the presence of mineral deposits, that any mineralisation will prove to be economic or that a mine will successfully be developed on any of CZR's mineral properties.

Competent Persons Statements

The information in this announcement that relates to exploration activities and exploration results is based on information compiled by Stefan Murphy (BSc), a Competent Person who is a Member of the Australian Institute of Geoscientists. Stefan Murphy is Managing Director of CZR Resources, holds options in the Company and has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a 'Competent Person' as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves' (JORC Code). Stefan Murphy has given his consent to the inclusion in this announcement of the matters based on his information in the form and context in which it appears.

Appendix A – ASX Announcements related to Ashburton Magnetite Project

ASX Announcement 11 February 2015 - New Volcanic-hosted High-grade Magnetite Discovery
ASX Announcement 6 October 2015 - Yarraloola Project Ashburton Trough Drilling Results
ASX Announcement 28 April 2016 - Significant Davis Tube results from Ashburton Magnetite
ASX Announcement 3 August 2016 - Positive Initial Metallurgical Results - Ashburton Magnetite
ASX Announcement 22 December 2016 - Yarraloola Iron Ore Project Drilling Program Complete
ASX Announcement 15 March 2017 - Ashburton Magnetite Drilling Update
ASX Announcement 21 March 2017 - Ashburton Magnetite Drilling Update - Additional Information
ASX Announcement 29 March 2017 - Retraction
ASX Announcement 1 June 2017 - Ashburton Magnetite Project Drilling Intercept Summary
ASX Announcement 10 October 2019 - Ashburton Magnetite Project Update on Field Programmes

Appendix B – Summary of the magnetite-rich intercepts

Hole Number	Depth From	Depth To	Interval m	Weathering	Fe %	SiO_2 %	Al_2O_3 %	P %	S %	LOI% 1000°
YAR091	0	56	56	oxide	23.5	53.1	6.48	0.07	0.06	3.11
YAR091	56	104	48	fresh	24.0	54.3	3.93	.12	.06	2.83
YAR093	28	57	29	fresh	31.9	47.5	2.80	0.11	0.15	1.61
YAR093	76	132	56	fresh	31.6	44.8	2.68	0.12	0.05	1.34
YAR094	4	42	38	oxide	20.59	50.96	9.15	0.080	0.008	5.27
YAR094	56	124	68	fresh	20.13	52.13	5.99	0.09	0.14	4.48
YAR094	124	133	9	fresh	12.76	62.81	7.67	0.08	0.19	3.30
YAR094	144	163	19	fresh	16.03	50.08	5.10	0.07	0.15	10.63
YAR095	36	81	45	oxide	26.22	53.69	3.30	0.12	0.06	1.69
YAR095	83	147	64	fresh	21.46	51.29	6.31	0.09	0.09	3.85
YAR096	19	51	32	oxide	21.41	57.17	5.64	0.07	0.01	3.09
YAR096	63	102	39	fresh	25.73	47.79	4.50	0.11	0.06	4.12
YAR096	162	168	6	fresh	15.40	53.21	3.81	0.11	0.21	9.35
YAR097	107	112	5	fresh	19.84	51.53	8.18	0.09	0.10	4.78
YAR097	119	132	13	fresh	23.39	53.75	1.80	0.11	0.10	4.00
YAR098	3	53	50	oxide	22.57	53.87	6.18	0.08	0.01	3.41
YAR098	3	78	75	oxide	19.87	55.11	7.17	0.09	0.02	3.28
YAR098	104	117	13	oxide	18.76	50.01	10.04	0.09	0.08	3.56
YAR098	121	136	15	fresh	19.87	50.73	8.00	0.08	0.05	3.73
YAR098	144	151	7	fresh	20.15	50.03	9.23	0.13	0.08	3.15
YAR098	155	177	22	fresh	21.71	46.37	4.60	0.11	0.17	7.63
YAR098	183	201	18	fresh	21.54	50.31	3.82	0.10	0.25	6.57
YAR099	5	58	53	oxide	24.74	52.98	5.42	0.08	0.01	3.10
YAR099	81	112	31	fresh	24.77	47.64	3.50	0.10	0.08	4.51
YAR099	117	120	3	fresh	26.63	50.37	2.10	0.07	0.05	4.10
YAR099	125	187	62	fresh	26.35	49.88	2.33	0.12	0.06	3.27
YAR100	43	62	19	oxidised	29.03	51.23	2.52	0.13	0.00	2.12
YAR100	62	198	136	fresh	28.30	47.70	2.49	0.13	0.03	2.81
YAR101	31	63	32	oxidised	20.10	59.92	5.34	0.07	0.01	3.31
YAR101	63	143	80	fresh	31.05	45.60	1.91	0.13	0.03	2.25
YAR101	156	163	7	fresh	27.08	44.00	2.13	0.12	0.09	7.19
YAR101	174	163	-11	fresh	29.26	43.13	2.78	0.13	0.08	3.67
YAR102	3	65	62	oxide	34.54	44.37	2.57	0.11	0.00	1.55

Hole Number	Depth From	Depth To	Interval m	Weathering	Fe %	SiO_2 %	Al_2O_3 %	P %	S %	LOI% 1000°
YAR102	72	96	24	fresh	24.85	49.45	5.71	0.14	0.04	1.94
YAR102	119	132	13	fresh	17.39	50.69	9.51	0.08	0.10	4.90
YAR102	139	155	16	fresh	19.55	50.95	8.11	0.09	0.07	4.29
YAR102	174	180	6	fresh	23.14	47.85	5.60	0.10	0.13	5.39
YAR103	67	76	9	oxidised	25.20	52.94	4.17	0.12	0.02	2.67
YAR103	148	197	49	fresh	26.94	43.09	4.19	0.10	0.20	4.51
YAR104	35	52	17	oxidised	29.96	48.57	3.30	0.16	0.00	2.48
YAR104	82	104	22	fresh	19.98	54.48	7.08	0.10	0.03	3.51
YAR105	71	106	35	fresh	33.28	45.88	2.35	0.13	0.02	1.03
YAR105	134	143	9	fresh	18.40	51.35	8.28	0.09	0.07	5.10
YAR106	73	88	15	fresh	32.42	44.71	3.28	0.12	0.01	2.40
YAR106	118	138	20	fresh	19.84	51.34	6.12	0.12	0.63	4.77
YAR107	98	132	34	fresh	31.69	44.63	2.58	0.12	0.05	1.66
YAR107	138	144	6	fresh	25.97	46.80	4.59	0.10	0.27	3.58
YAR107	170	177	7	fresh	18.44	50.69	8.93	0.08	0.12	5.53
YAR108	108	126	18	fresh	27.60	46.65	4.53	0.10	0.09	2.20
YAR108	168	187	19	fresh	19.47	51.13	7.87	0.09	0.07	4.53
YAR109	169	198		fresh	20.41	51.12	6.66	0.08	0.11	4.17
YAR222	3	33	30	oxide	29.29	48.95	4.17	0.102	0.003	2.91
YAR222	63	95	32	oxide	28.70	49.89	3.76	0.112	0.004	1.62
YAR223	0	20	20	oxide	26.33	48.10	4.51	0.049	0.012	5.09
YAR223	43	59	16	ox/fr	27.65	50.52	2.40	0.143	0.024	2.49
YAR223	64	185	121	fresh	26.37	48.46	3.45	0.128	0.075	2.79
YAR224	0	18	18	oxide	25.37	49.74	7.68	0.025	0.009	4.12
YAR224	37	115	78	ox/fr	28.89	47.43	2.28	0.128	0.037	2.37
YAR224	139	198	59	fresh	29.89	45.57	2.24	0.126	0.037	2.53
YAR225	122	134	12	fresh	23.44	50.19	4.17	0.092	0.129	3.58
YAR225	166	200*	34	fresh	28.83	47.56	1.89	0.125	0.045	2.80
YAR226	5	15	10	oxide	26.34	52.76	3.38	0.054	0.006	3.63
YAR226	43	51	8	oxide	26.24	50.90	4.94	0.118	0.002	2.86
YAR226	63	70	7	oxide	27.78	50.52	4.08	0.119	0.002	2.25
YAR226	85	141	56	fresh	29.22	47.51	1.91	0.121	0.042	2.00
YAR226	153	174	21	fresh	21.52	48.16	7.40	0.114	0.091	3.30
YAR226	186	200*	14	fresh	22.76	46.78	5.44	0.098	0.054	4.97

Hole Number	Depth From	Depth To	Interval m	Weathering	Fe %	SiO_2 %	Al_2O_3 %	P %	S %	LOI% 1000°
YAR227	44	181	137	ox/fr	28.32	46.93	2.55	0.124	0.029	3.29
YAR227	192	198	6	fresh	27.84	45.83	2.45	0.156	0.113	3.78
YAR228	0	7	7	oxide	29.98	45.61	4.28	0.032	0.008	4.07
YAR228	15	97	82	ox/fr	32.15	45.58	3.20	0.129	0.018	1.57
YAR228	122	135	13	fresh	20.26	51.10	7.22	0.094	0.066	4.28
YAR229	21	73	52	Ox/fr	29.91	45.30	3.61	0.115	0.025	2.28
YAR229	108	156	48	fresh	31.44	44.71	2.48	0.096	0.038	1.88
YAR229	190	198	8	fresh	20.00	50.22	7.41	0.099	0.081	4.32
YAR230	4	37	33	oxide	28.07	52.52	3.42	0.089	0.007	2.68
YAR230	45	76	31	ox/fr	29.16	50.28	3.30	0.113	0.019	2.23
YAR230	100	104	4	fresh	20.48	53.71	4.69	0.080	0.131	5.64
YAR230	112	161	49	fresh	24.07	47.51	3.28	0.104	0.105	6.36
YAR230	186	190	4	fresh	25.99	45.35	3.56	0.082	0.078	5.78
YAR231	25	89	64	ox/fr	28.83	50.06	3.57	0.122	0.064	2.33
YAR231	115	128	13	fresh	31.20	43.52	2.46	0.106	0.041	3.38
YAR231	133	137	4	fresh	19.57	52.24	6.87	0.106	0.076	4.83
YAR231	145	151	6	fresh	28.40	45.98	3.67	0.132	0.199	2.58
YAR231	173	200*	27	fresh	31.98	44.31	2.40	0.102	0.032	2.02

Appendix C – Davis Tube Recovery (DTR) head grade, magnetite-concentrate grade and yields

	Davis Tube Head Assays							Davis Tube Con Assays and Yields				
Hole ID	From	To	Interval	Fe %	SiO2 %	Al2O3 %	P %	Fe %	SiO2 %	Al2O3 %	P %	Recovery %
YAR091	0	85	85	26.1	52.1	5.0	0.10	67.7	3.4	0.3	0.02	12%
YAR093	28	53	25	31.8	47.6	2.9	0.10	67.6	3.7	0.2	0.01	21%
YAR093	76	86	10	30.9	47.1	3.0	0.13	66.6	6.2	0.4	0.02	35%
YAR093	89	129	40	32.9	44.2	2.1	0.11	67.4	5.8	0.3	0.02	31%
YAR098	38	53	15	22.6	51.0	7.6	0.10	66.3	5.3	0.3	0.01	12%
YAR098	121	131	10	24.4	48.5	5.3	0.09	68.5	4.3	0.3	0.01	26%
YAR098	155	173	18	23.2	45.7	4.4	0.13	64.8	8.9	0.4	0.03	22%
YAR099	34	59	25	21.9	53.7	7.2	0.10	66.9	4.5	0.3	0.01	10%
YAR099	94	187	93	24.7	52.3	2.3	0.11	67.6	5.5	0.2	0.02	28%
YAR100	43	198	155	28.7	47.7	2.3	0.13	67.0	5.9	0.3	0.02	33%
YAR101	58	143	85	30.9	46.1	1.9	0.12	68.8	3.9	0.2	0.01	32%
YAR102	45	65	20	32.9	45.0	3.2	0.16	68.3	2.5	0.2	0.02	19%
YAR102	72	80	8	28.3	48.4	3.3	0.14	68.6	4.0	0.2	0.01	30%
YAR103	66	76	10	25.1	52.9	4.2	0.13	67.7	4.0	0.3	0.02	15%
YAR103	149	179	30	28.5	42.9	3.5	0.11	67.6	5.4	0.3	0.02	31%
YAR103	182	197	15	26.7	42.9	3.2	0.09	68.1	4.9	0.2	0.02	27%

Appendix D – Composite Low Intensity Magnetic Separation (LIMS) testwork results

YARDDH002: 138.8-186.2m									
Stream	Yield (%)	Fe (wt%)	SiO2 (wt%)	Al2O3 (wt%)	P (wt%)	LOI (wt%)	FeO (wt%)	Fe3O4 (wt%)	Fe3O4 Rec (wt%)
Calc. Feed	100.0	30.2	45.1	1.9	0.132	3.0	10.2	31.2	100
R Conc	44.3	55.3	19.2	0.8	0.058	-1.4			
Cl 1 Con	37.5	63.5	9.9	0.4	0.034	-2.5			
Cl 2 Con	35.8	65.9	7.2	0.3	0.026	-2.8	28.5	86.6	99.6
YARDDH003:103.5-110.5m									
Stream	Yield (%)	Fe (wt%)	SiO2 (wt%)	Al2O3 (wt%)	P (wt%)	LOI (wt%)	FeO (wt%)	Fe3O4 (wt%)	Fe3O4 Rec (wt%)
Calc. Feed	100.0	27.3	46.4	2.4	0.127	5.9	7.5	22.9	100
R Conc	36.1	50.5	24.2	1.2	0.073	0.0			
Cl 1 Con	26.7	64.2	9.2	0.5	0.036	-2.3			
Cl 2 Con	25.9	65.6	7.6	0.4	0.030	-2.5	29.1	87.9	99.5
YARDDH003: 110.5-137.6m									
Stream	Yield (%)	Fe (wt%)	SiO2 (wt%)	Al2O3 (wt%)	P (wt%)	LOI (wt%)	FeO (wt%)	Fe3O4 (wt%)	Fe3O4 Rec (wt%)
Calc. Feed	100.0	33.3	44.4	1.7	0.087	1.4	9.4	29.6	100
R Conc	42.3	56.4	18.9	0.8	0.048	-1.9			
Cl 1 Con	33.7	66.4	7.0	0.4	0.022	-2.9			
Cl 2 Con	32.7	67.7	5.6	0.3	0.019	-3.0	28.7	90.4	99.7
YARDDH003: 137.6-146.2m									
Stream	Yield (%)	Fe (wt%)	SiO2 (wt%)	Al2O3 (wt%)	P (wt%)	LOI (wt%)	FeO (wt%)	Fe3O4 (wt%)	Fe3O4 Rec (wt%)
Calc. Feed	100.0	31.0	46.1	2.9	0.137	0.8	10.8	33.5	100
R Conc	51.6	52.0	23.6	1.5	0.075	-1.8			
Cl 1 Con	41.0	62.5	11.5	0.8	0.037	-2.7			
Cl 2 Con	38.9	65.1	8.4	0.6	0.028	-2.9	27.9	85.7	100

Appendix E – JORC Code, 2012 Edition Table 1

Section 1: Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	*Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*	RC samples are derived from 5.5" (140mm) reverse circulation drilling holes with continuous down-hole sampling. Samples for the metallurgical program were recovered from the deposit area by use of HQ and NQ sized diamond drilling.
	Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.	All RC drill cuttings pass through a cone splitter and samples are collected on 1m intervals. During the drilling of each meter, 2-3kg of drill chips were split off and collected in a labelled calico sample bag. Diamond core is continuous. After logging representative 10cm lengths of core were cut along their length with a fragment dispatched for thin-section preparation and the remainder used for geochemical analysis.
	Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	The entire 2-3kg RC drill-chip sample was dried and pulverized at Bureau Veritas Laboratories in Perth. Western Australia. A sub sample was fused with a lithium carbonate flux and the "extended iron-ore suite" of major oxide and selected trace-element analysis obtained by XRF Spectrometry on the disk. Au, Pt Pd has also been obtained by fire assay on a 50g sample charge. Diamond-core samples were pulverised at Bureau Veritas Laboratories in Perth. A sub-sample was fused with a lithium carbonate flux and analysed for major elements by XRF and a full suite of trace-elements from the same disk by LASER ablation ICP-MS.
Drilling techniques	*Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	Reverse circulation (RC) holes using a 5.5" (140mm) face-sampling percussion hammer. Diamond drilling uses HQ to approximately 200m and NQ recovery to the end of hole.
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.*	RC sample size was monitored by Geologists during the drilling programme. The volume of sample derived from each meter drilled was approximately equal. Diamond-core is measured between the depth markers reported by the drillers to establish the percentage recovery. In the interval below the base of oxidation, there is

Criteria	JORC Code explanation	Commentary
		rarely less than 100% recovery from the intercepts of the Shingle Creek Group.
	Measures taken to maximise sample recovery and ensure representative nature of the samples.	Standard RC sampling techniques were employed and deemed adequate for sample recovery. Some water was injected into the sample stream during drilling to minimise the loss of fine particles. Diamond core provides a continuous record of the rocks.
	Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	The loss of fine material has been minimized during drilling. Sample recovery is regarded as being representative. Measurements indicate diamond core recovery beneath the uppermost interval of intense weathering is excellent.
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	Each metre of reverse circulation chips is described geologically for mineralogy, colour and texture and magnetic susceptibility measured by handheld MagRock metre. No mineral resource estimates are included in this report. All the diamond core was photographed, described geologically for colour, texture and have an estimate of mineralogical abundance.
	Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.	Logging of diamond core and RC chips is qualitative.
	The total length and percentage of the relevant intersections logged.	Entire drill-holes are logged.
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.*	For geochemical sampling of representative rock-types, 10cm intervals of diamond core were ¼ cut along their length by a diamond bladed core-saw. Geological and physical properties are reported on whole core.
	If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.	Reverse circulation drill chip samples were collected dry and split by a continuously operating rotary cone splitter during drilling.
	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	Reverse circulation drilling is an appropriate method of recovering representative samples though the interval of mineralization. The drilling contractor used suitable sample collection and handling procedures to maintain sample integrity.
	Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.	Duplicate samples were simultaneously collected in mineralized intervals, using the cone splitter attached to the drill rig. Approximately 1 in 20 duplicate samples were analysed to ensure representivity.

Criteria	JORC Code explanation	Commentary
	Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.	The reverse circulation method samples continuously and the cone-splitter selects a representative proportion of the sample, providing an indication of compositional variations associated with each lithology or mineralized interval. Intervals of diamond-core samples are selected according to rock-type based on texture and rock-type.
	Whether sample sizes are appropriate to the grain size of the material being sampled.	The 2-3kg of homogenized drill chips that was recovered for each sample is sufficient to provide a representative indication of the material being sampled.
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	The geochemical data being reported is whole rock XRF and LASER ablation ICP-MS on a fused disk and is a total assay method for major element oxide analysis. Loss on ignition was completed using TGA.
	For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.	A hand-held magnetic susceptibility meter was used to record the response from the drill-chips and the response highlights the highly magnetic intercepts of magnetite schist in drill-holes.
	Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	Standard lab procedures were employed for standards and blanks. CZR introduces field-collected duplicates at a ratio of about 1:20.
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.*	No independent of alternative company personnel were used to verify the intersections.
	The use of twinned holes.	The drill intercepts reported are from an early stage exploratory drill programme.
	Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.	Data is delivered as both an electronic file and in pdf format by Bureau Veritas and the data is loaded into a Microsoft access database. The loaded data is regularly checked by a competent person against the pdf file to ensure all the oxides and elements are loaded into the correct fields
	Discuss any adjustment to assay data.	No adjustments made to assay data
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	Drill hole locations were derived from a hand held Garmin 72h GPS units, with an average accuracy of ±3m.

Criteria	JORC Code explanation	Commentary
	Specification of the grid system used.	The grid system is MGA GDA94, zone 50, all Easting's and Northing's are reported in MGA co-ordinates.
	Quality and adequacy of topographic control.	SRTM90 data is used to provide topographic control and is regarded as being adequate for early stage exploration.
Data spacing and distribution	*Data spacing for reporting of Exploration Results.*	The drill holes are located to examine the sub-surface geology associated with a series of different magnetic targets within the Ashburton Trough sequence
	Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	No Mineral Resources or Ore Reserve estimations are being presented in this report. The drill spacing is discussed and displayed within the exploration target methodology discussed in report.
	Whether sample compositing has been applied.	All geochemical data from RC samples is derived from the 1m interval samples. Diamond-drill orientation geochemistry for the characterisation of rock-types is obtained from 10cm intervals showing representative texture of ¼ core cut along its length
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	Mineralization is contained within a sequence that dips at about 50 to the south-west
	If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	The drill orientation was selected to minimise any sampling bias.
Sample security	*The measures taken to ensure sample security.*	Sample chain of custody supervised by CZR geologists.
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	No audits or reviews conducted.
Bulk Density	*Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.*	Density testwork was completed on the diamond core samples collected from the 3 diamond holes. Sample bulk density was measured by a wax coated water immersion method. Density measurements ranged from 2.75 to 3.8 with detailed sample description occurring to allow density to be attributed to different geological domains.

Criteria	JORC Code explanation	Commentary
	The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit,	Density was measured using a standard well-documented water immersion procedure. Samples selected across multiple rock types to develop a robust understanding of variation between units.
	Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.	Samples taken were coded by the lithology. Averages were derived within each lithology and this value then used to create the estimation target tonnes for the ore-bearing units.

Section 2: Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*	All mining, exploration and miscellaneous licenses owned 85% by Zanthus Resources Ltd and 15% by ZanF Pty Ltd. The tenements are covered by the Kuruma Marthudunera Native Title Claim and relevant heritage agreements are in place.
	The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	The tenements are in good standing and no known impediments exist.
Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	In 1990-1991, Aberfoyle Resources held tenements covering the Ashburton Trough which partially overlapped Yarraloola. They collected 26 rock-chip and 73 stream sediment samples for gold and base-metal exploration but encountered no significant results and surrendered the ground.
		In 1991-1992, Poseidon Exploration Ltd held exploration tenements covering the Ashburton Trough which partially overlapped Yarraloola for base-metals, gold and iron-ore. They collected 54 rock-chips, 236 soil samples, 492 stream sediment samples and completed 159 RAB holes for 2410m but encountered no significant mineralisation and surrendered the tenements.
		In 1997-1998, Sipa Resources NL held tenements over the Ashburton Trough that partially covered Yarraloola for gold and base-metals. A field trip after the interpretation of LANDSAT and air-photos collected six rock-chip samples which failed to detect mineralisation and the tenements were surrendered.
		In 2005-2009, Red Hill Iron Ltd held a tenement 15km northwest of Pannawonica which partially overlapped Yarraloola for gold and base-metal prospectivity. Following an aeromagnetic survey and air-photo interpretation, 16 rock-chips and 207 soil samples were collected but no targets were generated and the ground was surrendered.

Criteria	JORC Code explanation	Commentary
Geology	*Deposit type, geological setting and style of mineralisation.*	The eastern section of the Yarraloola tenements covers Archaean-age chemical and clastic sediments overlying basalts in the Hamersley Basin. The western part of the tenements covers deformed Palaeoproterozoic mostly clastic sediments of the Ashburton Basin which are overlain by more recent undeformed detritus associated with the Carnarvon Basin. Sediments of the Hamersley and Carnarvon Basins are known to host economic deposits of iron-ore. The magnetite mineralization described in this report is hosted within graphitic and chloritized volcanic schists of the attributed by the Geological Survey of Western Australia to the Shingle Creek Group..
Drill hole Information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*	
	o *easting and northing of the drill hole collar*	Drill hole collar Eastings and Northings are reported using map projection GDA Zone50, entered into an Access database and the map locations have been checked by the competent person
	o *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar*	The area has only minor relief and a nominal RL of 140m above sea level from the SRTM90 is used for results in this report. A differential GPS survey will provide future surface control.
	o *dip and azimuth of the hole*	All holes in the Ashburton are -50 to 050
	o *down hole length and interception depth*	Down hole lengths and intercept depths are calculated from 1m interval samples that are progressively collected as the holes are drilled.
	o *hole length.*	Hole lengths are reported both on the geological and drillers logs, entered into the access database and have been checked by a competent person.
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.*	Reported down-hole intercepts have magnetic susceptibility greater than 5000 times the host-rock sequence. The reported intervals provide guidance for future drilling to determine true thickness. No upper cut has been applied.
	Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	The aggregate intercepts reported are calculated averages of 1m interval samples.
	The assumptions used for any reporting of metal equivalent values should be clearly stated.	No metal equivalents are presented.

Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	*If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.*	The -50 inclined drill-holes are designed to intercept the moderately to steeply dipping geology and obtain sections across the geological units.
	If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').	Down-hole widths are regarded as true widths of mineralisation based of initial understanding of the ore-body strike and dip. Additional drillholes will assist to further refine the structural understanding of the ore-bearing lodes.
	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	No significant results reported in this announcement. There is a detailed map showing location of RC and Diamond drillcollars across the deposit.
Diagrams	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	The exploration target contains 4 domains which have been well illustrated in maps and linked to grade targets for each domain.
Balanced reporting	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	The report is believed to include all representative and relevant information and is believed to be comprehensive. Exploration results are not being reported for the first time.
Other substantive exploration data	*The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).*	Drilling has already confirmed the large scale of the deposit revealed by the geophysical anomalies and the preliminary metallurgical testwork confirms that the iron-bearing rocks are suitable for beneficiation. These results are very encouraging and allow for a strong foundation to be established for deposit evaluation. Future work will be focussed on proving the exploration target discussed in this announcement by completing infill grade drilling.

Criteria	JORC Code explanation	Commentary
Metallurgical factors and assumptions	*The metallurgical process proposed and the appropriateness of that process to the style of factors or mineralisation.* *Whether the metallurgical process is well-tested technology or novel in nature.* *The nature, amount and representativeness of metallurgical testwork undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.* *Any assumptions or allowances made for deleterious elements.* *The existence of any bulk sample or pilot-scale testwork and the degree to which such samples are considered representative of the orebody as a whole.* *For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications.*	The metallurgical testwork summarised in this announcement include bulk density, abrasive Index, grind size optimisation, bond work index, davis tube recovery (DTR) and Low Intensity Magnetic Separation (LIMS). These metallurgical tests are accepted as industry standard and were executed by licenced laboratory facility in Perth and results analysed by technically competent professional contractors.
Further work	*Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	The deposit extent is well delineated by geophysical feature and that is well documented in this announcement. Future work will be focused on proving this geophysical signature with RC grade drilling. The metallurgical properties of the deposit will require additional diamond drilling and testwork to be completed to build further upon the deposit understanding.