ASX ANNOUNCEMENT

15 APRIL 2024

# FURTHER HIGH-GRADE INFILL HITS CONTINUE TO BUILD CONFIDENCE AT SUNDAY CREEK

## 9 mineralised structures over 473 m, 8 assayed intervals > 50 g/t Au (up to 684 g/t Au)

### Includes 0.9 m @ 327.7 g/t Au

**Melbourne, Australia — Southern Cross Gold Ltd ("SXG" or the "Company") (ASX:SXG)** announces results from three diamond drill holes (SDDSC110, 113 and 114) from the Rising Sun prospect, at the 100%-owned Sunday Creek Project in Victoria (Figures 1 to 7).

## HIGHLIGHTS

- **SDDSC113** was drilled to test the strike extent and continuity of four high-grade vein sets. All high-grade targets were intersected as expected, with drill highlights:
  - **0.9 m @ 156.8 g/t AuEq** (156.0 g/t Au, 0.4% Sb) from 468.1 m
  - **15.5 m @ 5.0 g/t AuEq** (3.4 g/t Au, 0.9% Sb) from 558.0 m
  - **5.3 m @ 13.7 g/t AuEq** (10.5 g/t Au, 1.7% Sb) from 575.6 m
  - **0.9 m @ 332.9 g/t AuEq** (327.7 g/t Au, 2.8% Sb) from 702.4 m
  - **1.2 m @ 17.4 g/t AuEq** (16.9 g/t Au, 0.3% Sb) from 736.0 m
  - **4.1 m @ 23.4 g/t AuEq** (22.6 g/t Au, 0.4% Sb) from 751.0 m
- SDDSC113 intercepted **nine mineralised structures over 473 m @ 1.7 g/t AuEq (1.6 g/t Au, 0.1% Sb) uncut** and contains **eight assayed intervals > 50 g/t Au (up to 684 g/t Au) and six intervals > 5% Sb (up to 18.4% Sb).** Cumulatively the hole returned **794 AuEq g/t x m.**
- **SDDSC114** was designed to test a specific target on the RS100 vein set. It also tested a new vein set (RS55_L) now defined from two adjacent holes:
  - **2.7 m @ 18.1 g/t AuEq** (14.5 g/t Au, 1.9% Sb) from 628.5 m
  - **2.7 m @ 19.7 g/t AuEq** (19.2 g/t Au, 0.3% Sb) from 766.5 m
- Six drillholes at Sunday Creek are being processed and analysed, with four holes in progress.

**Southern Cross Gold's Managing Director, Michael Hudson, states**, *"Sunday Creek's systematic and unabated production of multiple high-grade gold and antimony drill results continues. Holes released here were targeted primarily at 30 m to 50 m spacing between previous high-grade intersections at Rising Sun. On multiple occasions the high-grade target zones were intersected as expected, showing the understanding and resultant predictability of the Sunday Creek gold-antimony project. A gold system that demonstrates predictability at these drill spacings ultimately delivers mineralisation that can potentially produce ounces at a much lower cost.*

*"Our strategy is to focus on grade and volume expansion to demonstrate the district scale of Sunday Creek.*

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*Big systems have big footprints. With only one third of our core 1 km x 1 km drill area tested, and with a 10 km strike extension to the system, we are still in the early days of our discovery journey.*

*"Sunday Creek compares extremely favourably with globally significant high-grade gold discoveries at this stage of the project's development. Cumulatively, 113 drill holes for 46,289 m have been reported from Sunday Creek. The project now contains a total of thirty-four >100 g/t AuEq x m and thirty-eight 50 to 100 g/t AuEq x m drill holes by applying a 2 m @ 1 g/t lower cut.*

*"SXG is fully permitted and has four drill rigs operating. Our intention is to increase drill capacity over the next quarter. Ten holes are being processed or in progress and we look forward to continued news flow."*

**Drill Hole Discussion**

Longitudinal sections of the vein seta are shown in Figures 3-5. Each figure shows the intersection pierce points, separation from adjacent holes, grades and estimated true widths ("ETW").

**SDDSC113** was drilled from the west to east at a high angle to mineralised vein sets. The hole was designed to test the strike extent and continuity of four separate >50 g/t Au vein sets of which three (RS10 (Figure 3), RS80 (Figure 4) and RS100 (Figure 5)) are shown in longitudinal section. All high-grade targets were intersected as planned. Five additional vein sets were also drilled to further test vein set strike extensions and demonstrate continuity of mineralised structures.

**SDDSC113** drilled nine mineralised structures in total over a 473 m @ 1.7 g/t AuEq (1.6 g/t Au, 0.1% Sb) (uncut) downhole interval and contains **eight assayed intervals > 50 g/t Au (up to 684 g/t Au) and six intervals > 5% Sb (up to 18.4% Sb).** Cumulatively the hole returned **794 AuEq g/t x m.**

An example of a vein set, RS10 (Figure 3) was originally mined to 42 m vertically in the Rising Sun shaft in the early 1900s. Drilling by SXG has now extended RS10 over 580 m from surface. **SDDSC113** drilled RS10 (**0.9 m @ 156.8 g/t AuEq from 468.1 m** ETW 0.5 m) in the altered footwall sediment This intersection is located respectively 52 m down dip from previously reported drillhole SDDSC077B (13.9 m @ 6.0 g/t AuEq (ETW 6.1 m)) and 34 m up dip from SDDSC100 (2.1 m @ 16.8 g/t AuEq (ETW 0.9 m)) which increases confidence in continuity of high grades.

Highlights from SDDSC113 (2m @ 1g/t Au lower cut) include:

- **2.0 m @ 3.8 g/t AuEq** (3.1 g/t Au, 0.4% Sb) from 337.0 m, including:
  - **0.7 m @ 7.0 g/t AuEq** (7.0 g/t Au, 0.0% Sb) from 338.3 m
- **0.3 m @ 5.6 g/t AuEq** (4.2 g/t Au, 0.7% Sb) from 345.4 m
- **5.9 m @ 3.7 g/t AuEq** (2.3 g/t Au, 0.7% Sb) from 406.3 m, including:
  - **2.1 m @ 5.9 g/t AuEq** (2.4 g/t Au, 1.8% Sb) from 408.7 m
- **0.3 m @ 10.0 g/t AuEq** (8.0 g/t Au, 1.1% Sb) from 465.5 m
- **0.9 m @ 156.8 g/t AuEq** (156.0 g/t Au, 0.4% Sb) from 468.1 m
- **0.4 m @ 16.3 g/t AuEq** (14.8 g/t Au, 0.8% Sb) from 518.5 m
- **6.3 m @ 2.0 g/t AuEq** (1.4 g/t Au, 0.3% Sb) from 536.8 m, including:
  - **0.2 m @ 41.0 g/t AuEq** (26.7 g/t Au, 7.6% Sb) from 538.7 m
- **3.0 m @ 2.3 g/t AuEq** (1.5 g/t Au, 0.4% Sb) from 552.0 m
- **15.5 m @ 5.0 g/t AuEq** (3.4 g/t Au, 0.9% Sb) from 558.0 m, including:
  - **1.2 m @ 6.7 g/t AuEq** (4.8 g/t Au, 1.0% Sb) from 559.5 m
  - **1.7 m @ 10.6 g/t AuEq** (8.5 g/t Au, 1.1% Sb) from 562.9 m

- **0.2 m @ 81.0 g/t AuEq** (61.1 g/t Au, 10.6% Sb) from 566.9 m
- **0.6 m @ 37.0 g/t AuEq** (27.7 g/t Au, 4.9% Sb) from 572.3 m

- **5.3 m @ 13.7 g/t AuEq** (10.5 g/t Au, 1.7% Sb) from 575.6 m, including:
  - **1.1 m @ 66.7 g/t AuEq** (51.5 g/t Au, 8.1% Sb) from 579.8 m
- **0.9 m @ 332.9 g/t AuEq** (327.7 g/t Au, 2.8% Sb) from 702.4 m, including:
  - **0.5 m @ 598.9 g/t AuEq** (589.8 g/t Au, 4.8% Sb) from 702.4 m
- **0.9 m @ 10.4 g/t AuEq** (9.7 g/t Au, 0.4% Sb) from 730.3 m
- **1.2 m @ 17.4 g/t AuEq** (16.9 g/t Au, 0.3% Sb) from 736.0 m, including:
  - **0.2 m @ 128.4 g/t AuEq** (125.0 g/t Au, 1.8% Sb) from 737.1 m
- **4.1 m @ 23.4 g/t AuEq** (22.6 g/t Au, 0.4% Sb) from 751.0 m, including:
  - **1.4 m @ 67.0 g/t AuEq** (66.9 g/t Au, 0.0% Sb) from 751.0 m
  - **0.5 m @ 9.9 g/t AuEq** (4.5 g/t Au, 2.9% Sb) from 753.5 m
- **0.3 m @ 10.9 g/t AuEq** (10.9 g/t Au, 0.0% Sb) from 791.4 m

**SDDSC114** was designed to test a target point on the RS100 vein set and intercepted **2.7 m @ 19.7 g/t AuEq from 766.5 m** (figure 5) as well as **2.7 m @ 18.1 g/t AuEq from 628.5 m** in vein set RS55_L. SDDSC114 provides two further examples of high-grade gold-antimony continuity. This hole also provided peripheral infill data for three other vein sets. Highlights include:

- **2.7 m @ 18.1 g/t AuEq** (14.5 g/t Au, 1.9% Sb) from 628.5 m
- **0.3 m @ 7.2 g/t AuEq** (6.6 g/t Au, 0.3% Sb) from 724.5 m
- **2.7 m @ 19.7 g/t AuEq** (19.2 g/t Au, 0.3% Sb) from 766.5 m, including:
  - **1.0 m @ 48.7 g/t AuEq** (48.0 g/t Au, 0.4% Sb) from 767.5 m
- **0.2 m @ 69.9 g/t AuEq** (69.9 g/t Au, 0.0% Sb) from 825.4 m
- **0.6 m @ 10.5 g/t AuEq** (10.5 g/t Au, 0.0% Sb) from 844.7 m

**SDDSC110 (0.7 m @ 11.2 g/t AuEq from 401.2 m)** intercepted the RS01 vein 23 m up plunge from SDDSC082 (3.8 m @ 180.3 g/t AuEq from 413.6 m). However, the remainder of the hole was drilled too far into the low-grade footwall and is considered a near-miss.

**Pending Results and Update**

Six holes (SDDSC111-112, 112W1, 115A, 116, 117) are currently being processed and analysed, with four holes (SDDSC118, 119, 120, 121) in progress (Figures 1 and 2).

**About Sunday Creek**

The Sunday Creek epizonal-style gold project is located 60 km north of Melbourne within 19,365 hectares of granted exploration tenements. SXG is also the freehold landholder of 133.29 hectares that form the key portion in and around the main drilled area at the Sunday Creek Project.

Gold and antimony form in a relay of vein sets that cut across a steeply dipping zone of intensely altered rocks (the “host”). When observed from above, the host resembles the side rails of a ladder, where the sub-vertical mineralised vein sets are the rungs that extend from surface to depth. At Apollo and Rising Sun these individual ‘rungs’ have been defined over 350 m depth extent from surface to 550 m below surface, are 10 m to 20 m wide, and 20 m to 100 m in strike.

Our systematic drill program is strategically targeting these significant vein formations. Initially these have

been defined over 1,350 m strike of the host from the Christina to the Apollo prospect, of which approximately 620 m has been more intensively drill tested (Rising Sun to Apollo). At least 45 'rungs' have been discovered to date, defined by high-grade intercepts (20 g/t to >7,330 g/t Au) along with lower grade edges. Ongoing step-out drilling is aiming to uncover the potential extent of this mineralised system.

Geologically, the project is located within the Melbourne Structural Zone in the Lachlan Fold Belt. The regional host to the Sunday Creek mineralisation is an interbedded turbidite sequence of siltstones and minor sandstones metamorphosed to sub-greenschist facies and folded into a set of open north-west trending folds.

**Other News**

The Company announces that it has informed Nagambie Resources Limited (NAG:ASX) ("Nagambie") that it will not proceed with its earn in on the Whroo Option and Joint Venture due to its focus on the 100% owned Sunday Creek Project. SXG still maintains a right of first refusal to take up or match proposals being considered over the Waranga Basin tenement package held by Nagambie. This package includes the Nagambie Gold Mine and the Whroo area. SXG maintains its 70% interest in the Redcastle JV area with Nagambie.

**Further Information**

Further discussion and analysis of the Sunday Creek project is available through the interactive Vrify 3D animations, presentations and videos all available on the SXG website. These data, along with an interview on these results with Managing Director Michael Hudson, with a 3D Leapfrog presentation, can be viewed at www.southerncrossgold.com.au

No upper gold grade cut is applied in the averaging and intervals are reported as drill thickness. However, during future Mineral Resource studies the requirement for assay top cutting will be assessed.

Figures 1 to 7 show project location, plan, longitudinal and cross-sectional views of drill results reported here and Tables 1 to 3 provide collar and assay data. The true thickness of the mineralised intervals reported individually as estimated true widths ("ETW"), otherwise they are interpreted to be approximately 50% to 60% of the sampled thickness for other reported holes. Estimated true widths ("ETW") are shown on Figure 3-5. Lower grades were cut at 1.0 g/t AuEq lower cutoff over a maximum width of 2 m with higher grades cut at 5.0 g/t Au lower cutoff over a maximum of 1 m width.

**Gold Equivalent Calculation**

SXG considers that both gold and antimony that are included in the gold equivalent calculation ("AuEq") have reasonable potential to be recovered at Sunday Creek, given current geochemical understanding, historic production statistics and geologically analogous mining operations. Historically, ore from Sunday Creek was treated onsite or shipped to the Costerfield mine, located 54 km to the northwest of the project, for processing during WW1. The Costerfield mine corridor, now owned by Mandalay Resources Ltd contains two million ounces of equivalent gold (Mandalay Q3 2021 Results), and in 2020 was the sixth highest-grade global underground mine and a top 5 global producer of antimony.

SXG considers that it is appropriate to adopt the same gold equivalent variables as Mandalay Resources Ltd in its Mandalay Technical Report, 2024 dated 28 March 2024. The gold equivalence formula used by Mandalay Resources was calculated using Costerfield's 2023 production costs, using a gold price of US$1,900 per ounce, an antimony price of US$12,000 per tonne and 2021 total year metal recoveries of 93% for gold and 95% for antimony, and is as follows:

$$AuEq = Au\ (g/t) + 1.88 \times Sb\ (\%).$$

Based on the latest Costerfield calculation and given the similar geological styles and historic toll treatment of Sunday Creek mineralisation at Costerfield, SXG considers that a $AuEq = Au\ (g/t) + 1.88 \times Sb\ (\%)$ is appropriate to use for the initial exploration targeting of gold-antimony mineralisation at Sunday Creek.

- Ends -

This announcement has been approved for release by the Board of Southern Cross Gold Ltd.

**Competent Person Statement**

Information in this announcement that relates to new exploration results contained in this report is based on information compiled by Mr. Michael Hudson, a Fellow of the Australasian Institute of Mining and Metallurgy. He is the Managing Director of Southern Cross Gold Ltd. He has sufficient experience which is relevant to the style of mineralisation and types of deposits under consideration and to the activity being undertaking to qualify as a Competent Person as defined in the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (the JORC Code). Michael Hudson has consented to the inclusion in this report of the matters based on this information in the form and context in which it appears.

Certain information in this announcement that relates to prior exploration results is extracted from the Independent Geologist's Report dated 16 March 2022 which was issued with the consent of the Competent Person, Mr Terry C. Lees. The report is included the Company's prospectus dated 17 March 2022 which was released as an announcement to ASX on 12 May 2022 and is available at www2.asx.com.au under code "SXG". The Company confirms that it is not aware of any new information or data that materially affects the information related to exploration results included in the original market announcement. The Company confirms that the form and context of the Competent Persons' findings in relation to the report have not been materially modified from the original market announcement.

Certain information in this announcement also relates to prior drill hole exploration results, are extracted from the following announcements, which are available to view on www.southerncrossgold.com.au:

- 7 October, 2020 MDDSC003, 27 October, 2021 MDDSC021, 4 October, 2022 SDDSC043 & 46, 21 November, 2022 SDDSC050, 14 December, 2022 SDDSC050, 16 May, 2023 SDDSC064, 3 July, 2023 SDDSC070, 23 August, 2023 SDDSC078, 5 September, 2023 SDDSC077B, 12 October, 2023 SDDLV003 & 4, 23 October, 2023 SDDSC082, 14 December, 2023 SDDSC092, 8 February, 2024 SDDSC094A,100 & 104, 27 February, 2024 SDDSC108A, 5 March, 2024 SDDSC107.
- The Company confirms that it is not aware of any new information or data that materially affects the information included in the original document/announcement and the Company confirms that the form and context in which the Competent Person's findings are presented have not materially modified from the original market announcement.

**For further information, please contact:**

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**Figure 1: Sunday Creek plan view showing SDDSC110, 113, 114 reported here (grey box, blue highlight), selected prior reported drill holes and pending holes. For location see Figure 4.**

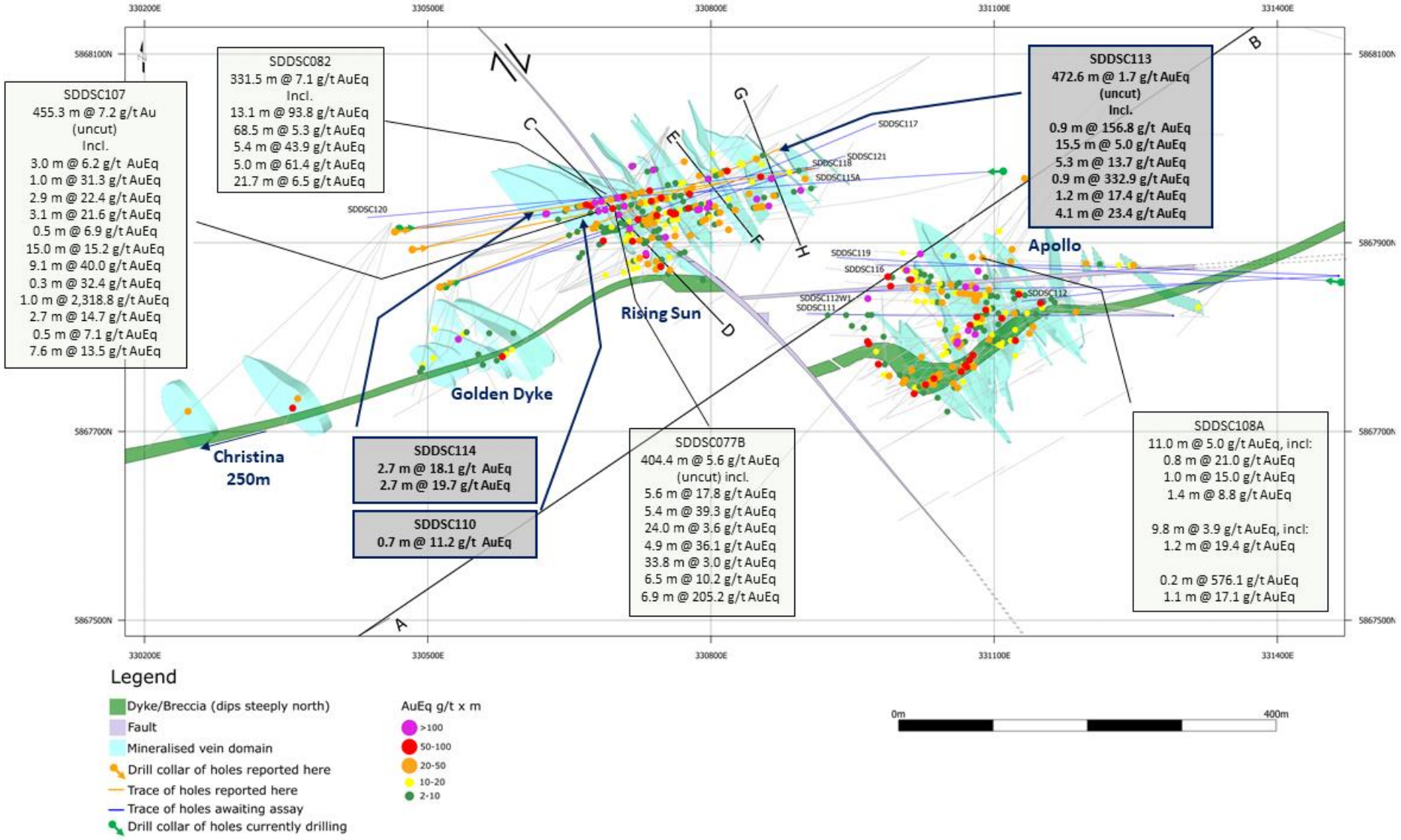

**Figure 2: Sunday Creek longitudinal section across A-B in the plane of the dyke breccia/altered sediment host (see Figure 1) looking towards the north (striking 236 degrees) showing mineralised veins sets. Showing SDDSC110, 113, 114 reported here and prior reported drill holes.**

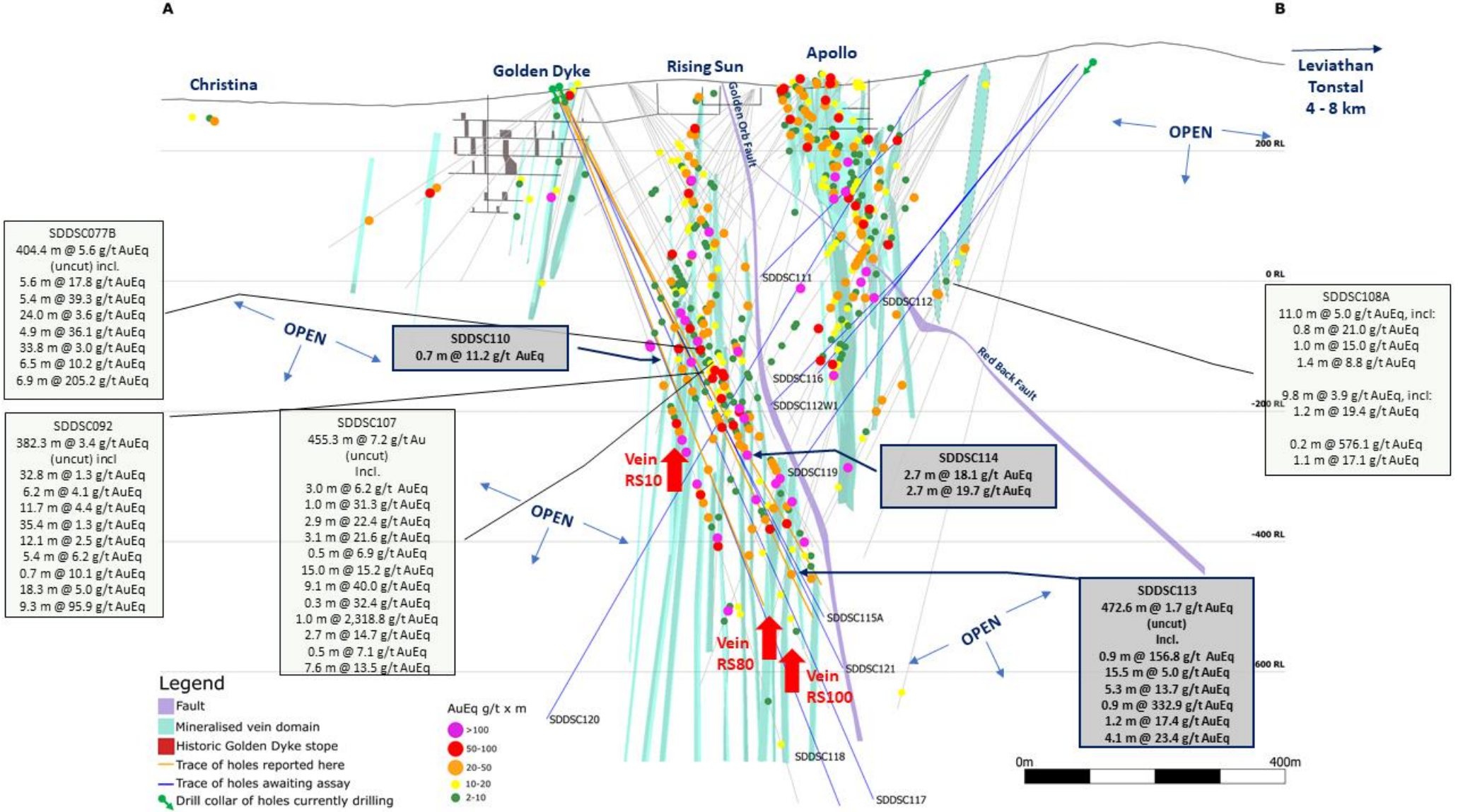

**Figure 3: Sunday Creek longitudinal section across C-D in the plane of the modelled vein set RS10, looking towards the south-west (striking 136 degrees). Showing SDDSC110, 113 (orange trace and text) reported here and prior reported drill holes.**

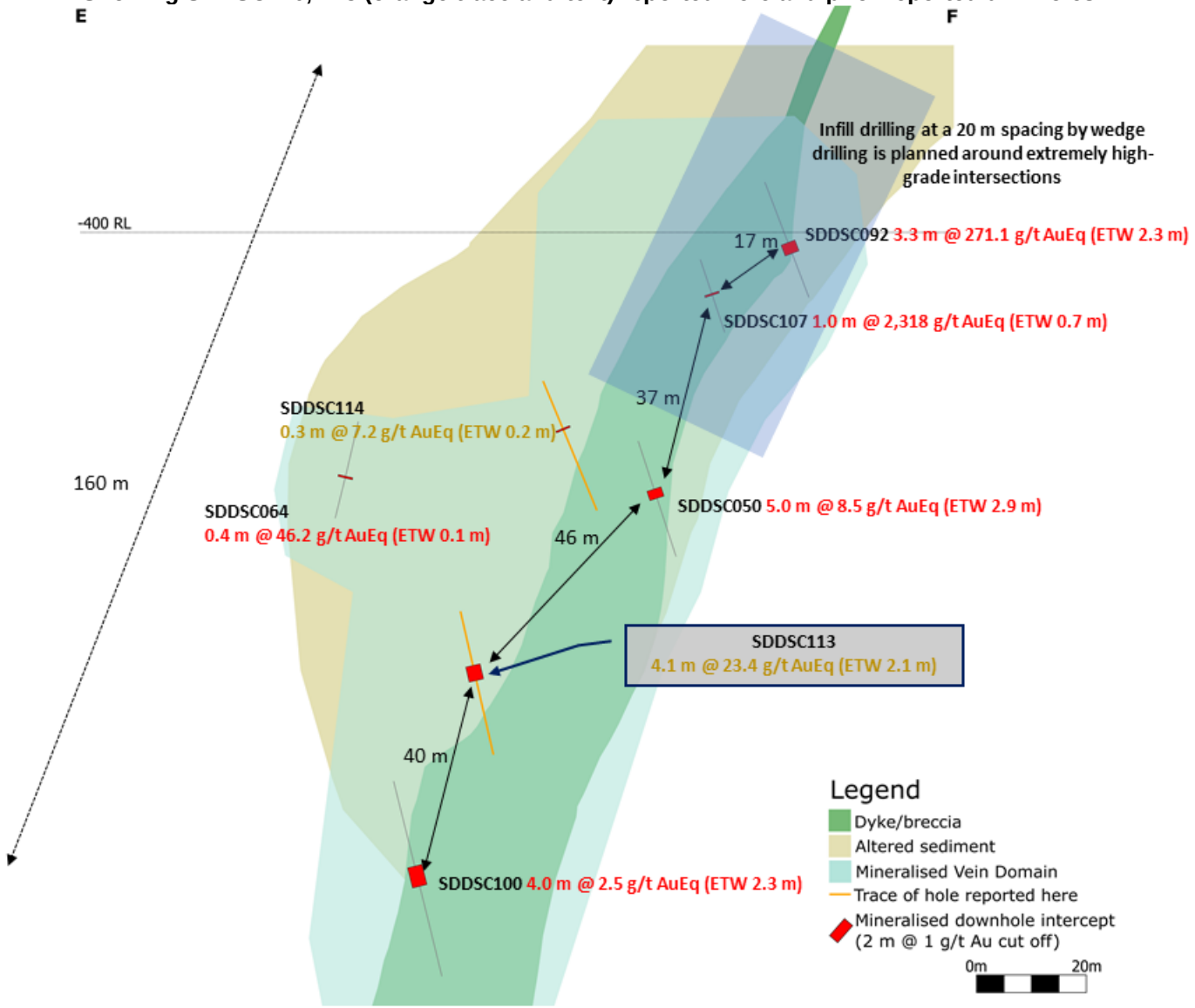

**Figure 4: Sunday Creek longitudinal section across E-F in the plane of the modelled vein set RS80, looking towards the south-west (striking 141 degrees). Showing excellent continuity of vein set in SDDSC113 (orange trace and text) reported here and prior reported drill holes.**

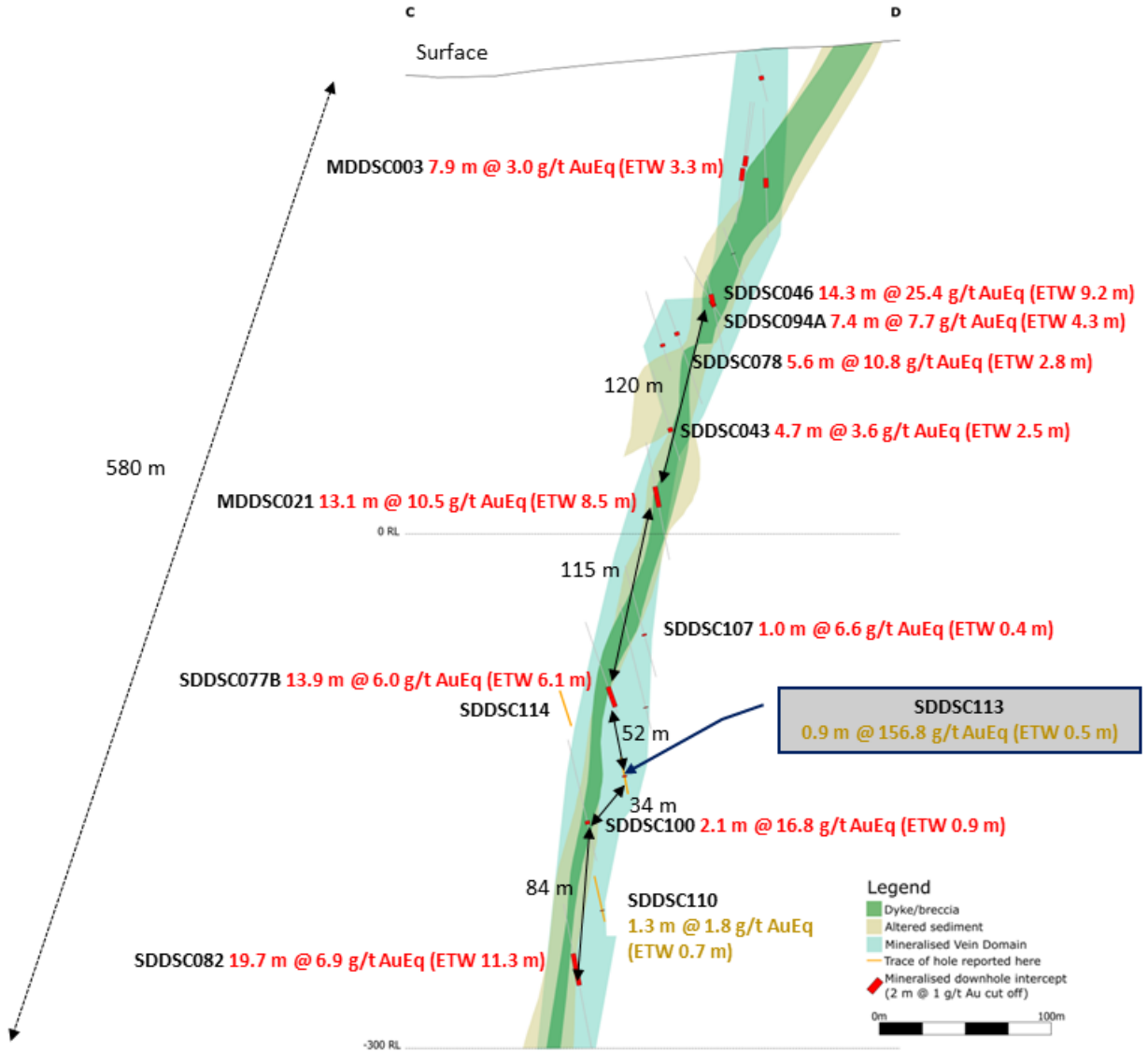

**Figure 5: Sunday Creek longitudinal section across G-H in the plane of the modelled vein set RS100, looking towards the south-west (striking 161 degrees). Showing SDDSC114 (orange trace and text) reported here and prior reported drill holes.**

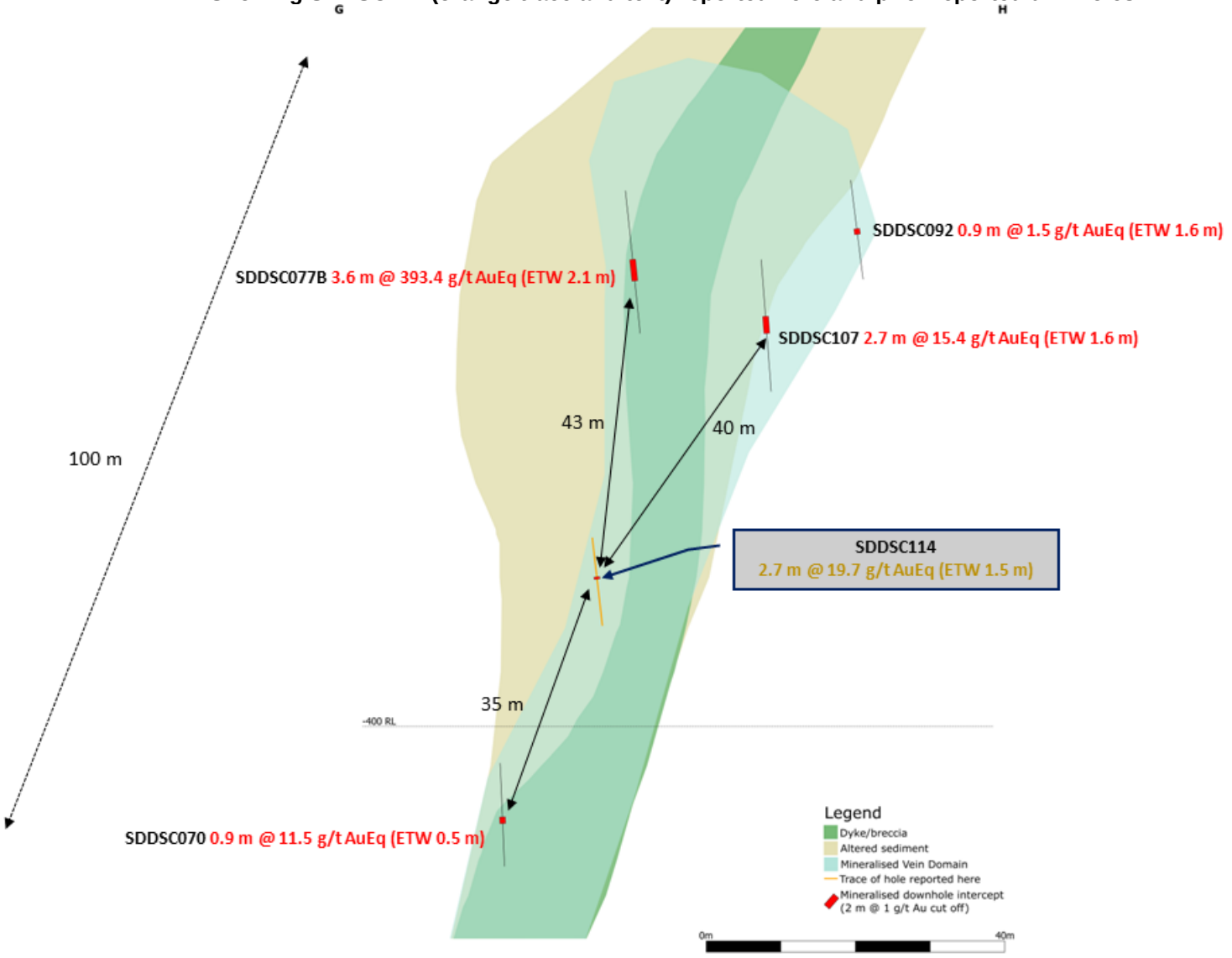

**Figure 6: Sunday Creek regional plan view showing LiDAR, soil sampling, structural framework, regional historic epizonal gold mining areas and broad regional areas (Tonstal, Consols and Leviathan) tested by 12 holes for 2,383 m drill program. The regional drill areas are at Tonstal, Consols and Leviathan located 4,000-7,500 m along strike from the main drill area at Golden Dyke- Apollo.**

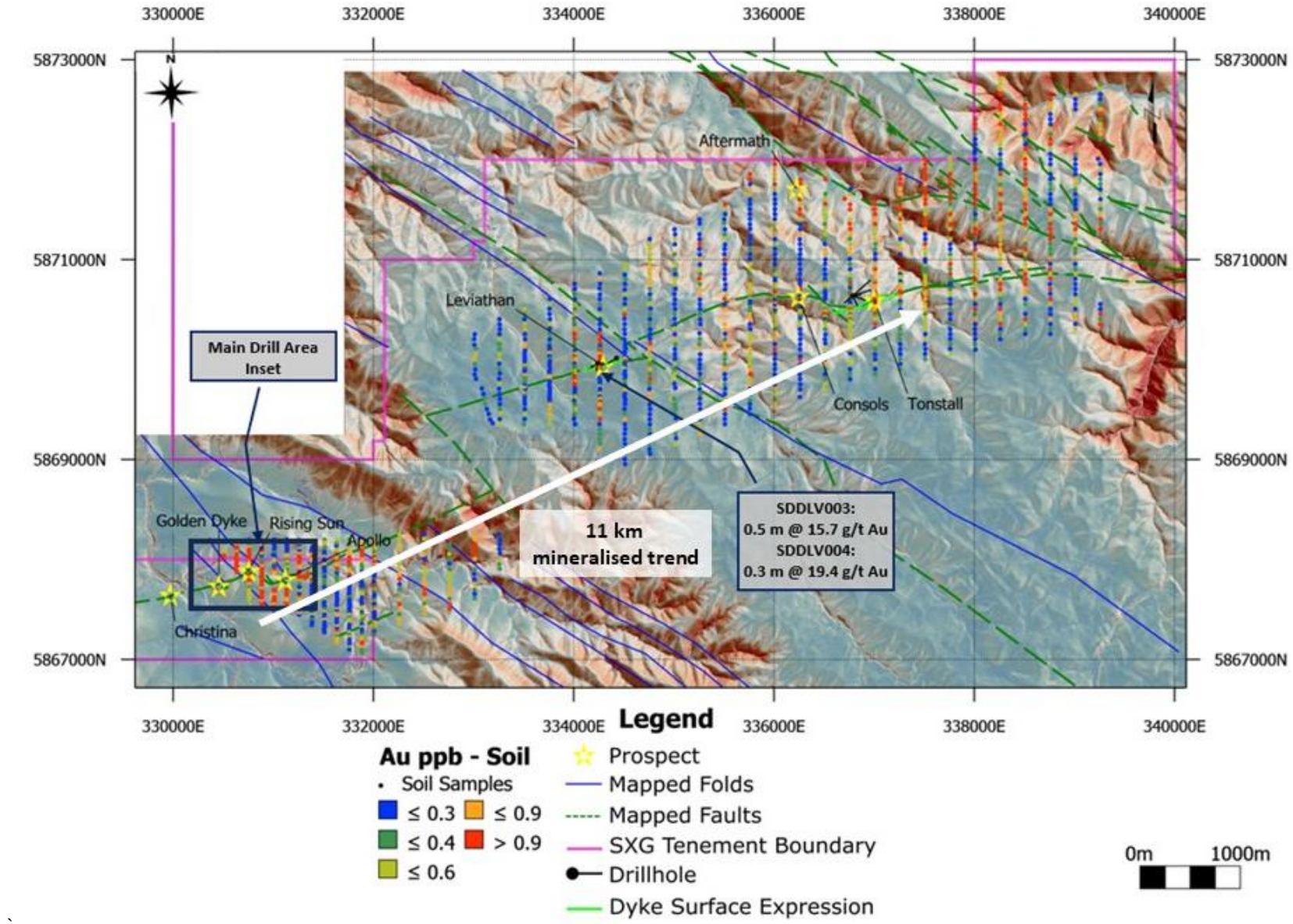

**Figure 7: Location of the Sunday Creek project, along with SXG's other Victoria projects and simplified geology.**

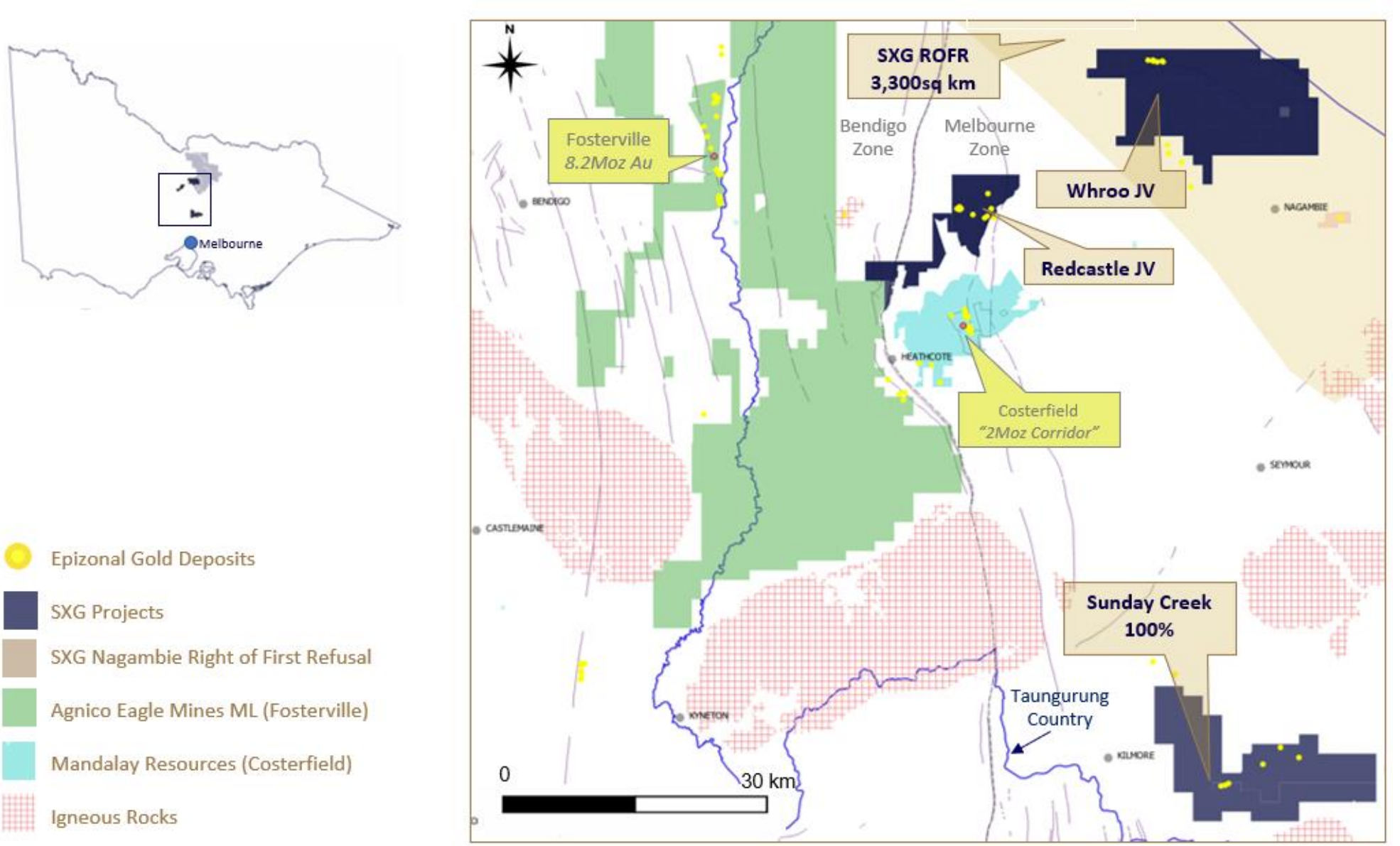

**Table 1: Drill collar summary table for recent drill holes in progress.**

| Hole_ID | Depth (m) | Prospect | East GDA94_Z55 | North GDA94_Z55 | Elevation | Azimuth | Plunge |
|---|---|---|---|---|---|---|---|
| SDDSC092 | 803.8 | Rising Sun | 330537 | 5867882 | 295.5 | 79.0 | -60 |
| SDDSC093 | 610.9 | Rising Sun | 331291 | 5867823 | 316.8 | 271 | -47.5 |
| SDDSC094 | 23.3 | Rising Sun | 330639 | 5867846 | 306.2 | 68.5 | -56 |
| SDDSC094A | 359.6 | Rising Sun | 330639 | 5867846 | 306.1 | 68.5 | -56 |
| SDDSC095 | 368.3 | Apollo | 331291 | 5867823 | 316.8 | 271 | -53 |
| SDDSC096 | 347.9 | Rising Sun | 330639 | 5867846 | 306.1 | 68 | -63.5 |
| SDDSC097 | 62.3 | Apollo | 331291 | 5867823 | 316.8 | 276 | -50.5 |
| SDDSC097A | 575 | Apollo | 331291 | 5867823 | 316.8 | 277 | -50 |
| SDDSC098 | 278.5 | Rising Sun | 330639 | 5867846 | 306.1 | 72 | -48.5 |
| SDDSC099 | 284.7 | Rising Sun | 330639 | 5867846 | 306.1 | 71.5 | -58.5 |
| SDDSC100 | 1042 | Rising Sun | 330482 | 5867891 | 289.5 | 74.5 | -64 |
| SDDSC101 | 181.5 | Rising Sun | 330639 | 5867846 | 306.1 | 63 | -37 |
| SDDSC102 | 596.8 | Rising Sun | 330537 | 5867883 | 295.5 | 75 | -59 |
| SDDSC103 | 260.6 | Rising Sun | 330639 | 5867847 | 306.1 | 53 | -53 |
| SDDSC104 | 595.2 | Rising Sun | 330639 | 5867847 | 306.1 | 64.5 | -65.7 |
| SDDSC105 | 353.6 | Apollo | 331291 | 5867823 | 316.8 | 275.3 | -55.2 |
| SDDSC106 | 653.5 | Apolo | 331291 | 5867823 | 316.8 | 279.5 | -53 |
| SDDSC107 | 815.9 | Rising Sun | 330537 | 5867883 | 295.5 | 77.5 | -62 |
| SDDSC108A | 855.9 | Apollo | 331464 | 5867865 | 333 | 272.5 | -50 |
| SDDSC109 | 520.9 | Apollo | 331291 | 5867823 | 316.8 | 273.5 | -44.5 |
| SDDSC110 | 856.7 | Rising Sun | 330482 | 5867892 | 289.5 | 78 | -66 |
| SDDSC111 | 496.7 | Apollo | 331291 | 5867823 | 316.8 | 270 | -38 |
| SDDSC112 | 490.9 | Apollo | 331464 | 5867865 | 333 | 267 | -42 |
| SDDSC112W1 | 766.4 | Apollo | 331329 | 5867859 | 200 | 267 | -42 |
| SDDSC113 | 905.5 | Rising Sun | 330511 | 5867853 | 296.6 | 67.5 | -63.5 |
| SDDSC114 | 878.6 | Rising Sun | 330464 | 5867914 | 286.6 | 82 | -58 |
| SDDSC115 | 17.6 | Rising Sun | 330464 | 5867912 | 286.6 | 83 | -58.5 |
| SDDSC115A | 923.6 | Rising Sun | 330464 | 5867912 | 286.7 | 83 | -59 |
| SDDSC116 | 682.6 | Rising Sun | 331465 | 5867865 | 333.3 | 272.5 | -41.5 |
| SDDSC117 | 1101 | Rising Sun | 330510 | 5867852 | 296.5 | 70.5 | -64.5 |
| SDDSC118 | In progress plan 1200 m | Rising Sun | 330464 | 5867912 | 286.6 | 80 | -64.5 |
| SDDSC119 | In progress plan 840 m | Apollo | 331498 | 5867858 | 336.7 | 272.5 | -45.2 |
| SDDSC120 | In progress plan 1200 m | Rising Sun | 331110 | 5867976 | 319.5 | 266.5 | -55 |
| SDDSC121 | In progress plan 1000 m | Rising Sun | 330510 | 5867852 | 296.6 | 72 | -63 |

**Table 2:** Tables of mineralised drill hole intersections reported from SDDSC110, 113 and 114 using two cut-off criteria.

1.0 g/t Au lower cutoff over a maximum of 2 m

| Hole-ID | From (m) | To (m) | Length (m) | Au g/t | Sb% | AuEq g/t |
|---|---|---|---|---|---|---|
| SDDSC110 | 401.20 | 401.90 | 0.7 | 9.4 | 1.0 | 11.2 |
| SDDSC110 | 534.91 | 536.21 | 1.3 | 0.8 | 0.5 | 1.8 |
| SDDSC110 | 556.20 | 557.30 | 1.1 | 1.8 | 0.6 | 2.8 |
| SDDSC110 | 694.85 | 695.26 | 0.4 | 0.4 | 0.6 | 1.5 |
| SDDSC110 | 731.30 | 731.75 | 0.5 | 0.6 | 0.8 | 2.0 |
| SDDSC110 | 759.68 | 762.75 | 3.1 | 0.6 | 0.1 | 0.8 |
| SDDSC110 | 789.00 | 790.00 | 1.0 | 1.6 | 0.0 | 1.6 |
| SDDSC110 | 822.00 | 823.00 | 1.0 | 1.1 | 0.0 | 1.1 |
| SDDSC110 | 825.45 | 826.28 | 0.8 | 1.7 | 0.0 | 1.8 |
| SDDSC110 | 829.91 | 830.60 | 0.7 | 1.1 | 0.0 | 1.1 |
| SDDSC113 | 322.63 | 322.78 | 0.1 | 0.5 | 0.4 | 1.3 |
| SDDSC113 | 337.00 | 339.00 | 2.0 | 3.1 | 0.4 | 3.8 |
| SDDSC113 | 345.37 | 345.68 | 0.3 | 4.2 | 0.7 | 5.6 |
| SDDSC113 | 358.06 | 361.05 | 3.0 | 0.7 | 0.2 | 1.1 |
| SDDSC113 | 406.30 | 412.20 | 5.9 | 2.3 | 0.7 | 3.7 |
| SDDSC113 | 419.00 | 422.00 | 3.0 | 0.6 | 0.1 | 0.7 |
| SDDSC113 | 425.00 | 425.52 | 0.5 | 2.0 | 0.5 | 2.9 |
| SDDSC113 | 431.65 | 431.88 | 0.2 | 1.3 | 0.1 | 1.4 |
| SDDSC113 | 458.29 | 458.80 | 0.5 | 1.5 | 0.6 | 2.5 |
| SDDSC113 | 461.12 | 461.54 | 0.4 | 4.3 | 0.0 | 4.4 |
| SDDSC113 | 464.67 | 465.72 | 1.1 | 2.1 | 0.6 | 3.3 |
| SDDSC113 | 468.10 | 468.98 | 0.9 | 156.0 | 0.4 | 156.8 |
| SDDSC113 | 477.00 | 477.38 | 0.4 | 1.8 | 0.0 | 1.8 |
| SDDSC113 | 482.00 | 482.24 | 0.2 | 1.9 | 0.0 | 1.9 |
| SDDSC113 | 493.86 | 494.38 | 0.5 | 1.3 | 0.0 | 1.3 |
| SDDSC113 | 518.51 | 518.90 | 0.4 | 14.8 | 0.8 | 16.3 |
| SDDSC113 | 522.73 | 522.98 | 0.3 | 6.1 | 0.1 | 6.3 |
| SDDSC113 | 536.75 | 543.00 | 6.3 | 1.4 | 0.3 | 2.0 |
| SDDSC113 | 545.36 | 547.08 | 1.7 | 1.2 | 0.0 | 1.2 |
| SDDSC113 | 552.00 | 555.00 | 3.0 | 1.5 | 0.4 | 2.3 |
| SDDSC113 | 558.00 | 573.50 | 15.5 | 3.4 | 0.9 | 5.0 |
| SDDSC113 | 575.55 | 580.87 | 5.3 | 10.5 | 1.7 | 13.7 |
| SDDSC113 | 590.80 | 591.00 | 0.2 | 0.7 | 0.3 | 1.2 |
| SDDSC113 | 595.00 | 595.68 | 0.7 | 0.6 | 0.4 | 1.4 |
| SDDSC113 | 624.77 | 625.10 | 0.3 | 1.7 | 0.0 | 1.7 |
| SDDSC113 | 644.36 | 644.48 | 0.1 | 0.7 | 0.2 | 1.1 |
| SDDSC113 | 702.40 | 703.25 | 0.9 | 327.7 | 2.8 | 332.9 |
| SDDSC113 | 717.60 | 717.85 | 0.3 | 1.0 | 0.2 | 1.5 |

| | | | | | | |
|---|---|---|---|---|---|---|
| SDDSC113 | 721.40 | 723.55 | 2.1 | 1.0 | 0.2 | 1.4 |
| SDDSC113 | 730.30 | 731.23 | 0.9 | 9.7 | 0.4 | 10.4 |
| SDDSC113 | 736.00 | 737.20 | 1.2 | 16.9 | 0.3 | 17.4 |
| SDDSC113 | 750.96 | 755.10 | 4.1 | 22.6 | 0.4 | 23.4 |
| SDDSC113 | 770.00 | 771.00 | 1.0 | 1.6 | 0.1 | 1.7 |
| SDDSC113 | 788.66 | 788.87 | 0.2 | 6.7 | 0.0 | 6.7 |
| SDDSC113 | 791.41 | 791.68 | 0.3 | 10.9 | 0.0 | 10.9 |
| SDDSC113 | 796.10 | 796.60 | 0.5 | 1.2 | 0.0 | 1.2 |
| SDDSC113 | 807.74 | 809.11 | 1.4 | 3.6 | 0.0 | 3.6 |
| SDDSC113 | 816.59 | 819.43 | 2.8 | 0.9 | 0.0 | 0.9 |
| SDDSC114 | 485.12 | 485.97 | 0.9 | 1.2 | 0.8 | 2.7 |
| SDDSC114 | 510.52 | 512.55 | 2.0 | 2.1 | 0.3 | 2.6 |
| SDDSC114 | 520.59 | 521.00 | 0.4 | 1.3 | 0.0 | 1.3 |
| SDDSC114 | 526.05 | 526.34 | 0.3 | 2.8 | 0.3 | 3.4 |
| SDDSC114 | 564.58 | 564.74 | 0.2 | 2.1 | 4.5 | 10.5 |
| SDDSC114 | 628.50 | 631.20 | 2.7 | 14.5 | 1.9 | 18.1 |
| SDDSC114 | 724.45 | 724.78 | 0.3 | 6.6 | 0.3 | 7.2 |
| SDDSC114 | 766.45 | 769.12 | 2.7 | 19.2 | 0.3 | 19.7 |
| SDDSC114 | 776.20 | 776.60 | 0.4 | 3.6 | 0.0 | 3.6 |
| SDDSC114 | 787.39 | 788.11 | 0.7 | 1.2 | 0.0 | 1.2 |
| SDDSC114 | 794.53 | 795.02 | 0.5 | 1.6 | 0.0 | 1.6 |
| SDDSC114 | 813.54 | 813.98 | 0.4 | 2.2 | 0.0 | 2.2 |
| SDDSC114 | 825.35 | 825.58 | 0.2 | 69.9 | 0.0 | 69.9 |
| SDDSC114 | 844.71 | 845.33 | 0.6 | 10.5 | 0.0 | 10.5 |

5.0 g/t Au cutoff over a maximum of 1 m.

| Hole-ID | From (m) | To (m) | Length (m) | Au g/t | Sb% | AuEq g/t |
|---|---|---|---|---|---|---|
| SDDSC110 | 401.20 | 401.90 | 0.7 | 9.4 | 1.0 | 11.2 |
| SDDSC113 | 337.00 | 337.20 | 0.2 | 0.8 | 3.6 | 7.6 |
| SDDSC113 | 338.26 | 339.00 | 0.7 | 7.0 | 0.0 | 7.0 |
| SDDSC113 | 345.37 | 345.68 | 0.3 | 4.2 | 0.7 | 5.6 |
| SDDSC113 | 360.82 | 361.05 | 0.2 | 1.5 | 2.5 | 6.3 |
| SDDSC113 | 408.65 | 410.70 | 2.1 | 2.4 | 1.8 | 5.9 |
| SDDSC113 | 465.46 | 465.72 | 0.3 | 8.0 | 1.1 | 10.0 |
| SDDSC113 | 468.10 | 468.98 | 0.9 | 156.0 | 0.4 | 156.8 |
| SDDSC113 | 518.51 | 518.90 | 0.4 | 14.8 | 0.8 | 16.3 |
| SDDSC113 | 522.73 | 522.98 | 0.3 | 6.1 | 0.1 | 6.3 |
| SDDSC113 | 538.69 | 538.87 | 0.2 | 26.7 | 7.6 | 41.0 |
| SDDSC113 | 546.85 | 547.08 | 0.2 | 6.9 | 0.1 | 7.1 |
| SDDSC113 | 559.47 | 560.70 | 1.2 | 4.8 | 1.0 | 6.7 |
| SDDSC113 | 562.87 | 564.53 | 1.7 | 8.5 | 1.1 | 10.6 |
| SDDSC113 | 566.90 | 567.09 | 0.2 | 61.1 | 10.6 | 81.0 |

| | | | | | | |
|---|---|---|---|---|---|---|
| SDDSC113 | 572.26 | 572.83 | 0.6 | 27.7 | 4.9 | 37.0 |
| SDDSC113 | 579.81 | 580.87 | 1.1 | 51.5 | 8.1 | 66.7 |
| SDDSC113 | 702.40 | 702.87 | 0.5 | 589.8 | 4.8 | 598.9 |
| SDDSC113 | 730.30 | 731.23 | 0.9 | 9.7 | 0.4 | 10.4 |
| SDDSC113 | 737.05 | 737.20 | 0.2 | 125.0 | 1.8 | 128.4 |
| SDDSC113 | 750.96 | 752.32 | 1.4 | 66.9 | 0.0 | 67.0 |
| SDDSC113 | 753.50 | 754.00 | 0.5 | 4.5 | 2.9 | 9.9 |
| SDDSC113 | 788.66 | 788.87 | 0.2 | 6.7 | 0.0 | 6.7 |
| SDDSC113 | 791.41 | 791.68 | 0.3 | 10.9 | 0.0 | 10.9 |
| SDDSC114 | 526.20 | 526.34 | 0.1 | 4.9 | 0.3 | 5.3 |
| SDDSC114 | 564.58 | 564.74 | 0.2 | 2.1 | 4.5 | 10.5 |
| SDDSC114 | 628.50 | 631.20 | 2.7 | 14.5 | 1.9 | 18.1 |
| SDDSC114 | 724.45 | 724.78 | 0.3 | 6.6 | 0.3 | 7.2 |
| SDDSC114 | 767.45 | 768.45 | 1.0 | 48.0 | 0.4 | 48.7 |
| SDDSC114 | 825.35 | 825.58 | 0.2 | 69.9 | 0.0 | 69.9 |
| SDDSC114 | 844.71 | 845.33 | 0.6 | 10.5 | 0.0 | 10.5 |

**Table 3:** All individual assays reported from SDDSC1110, 113 and 114 reported here >0.1g/t AuEq.

| Hole-ID | From (m) | To (m) | Length (m) | Au g/t | Sb% | AuEq g/t |
|---|---|---|---|---|---|---|
| SDDSC110 | 362.26 | 362.64 | 0.4 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 369.00 | 370.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 370.00 | 370.95 | 1.0 | 0.8 | 0.0 | 0.8 |
| SDDSC110 | 375.29 | 375.60 | 0.3 | 0.2 | 0.1 | 0.3 |
| SDDSC110 | 394.64 | 395.00 | 0.4 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 395.00 | 396.10 | 1.1 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 397.40 | 397.90 | 0.5 | 0.9 | 0.0 | 0.9 |
| SDDSC110 | 397.90 | 398.45 | 0.6 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 398.45 | 399.40 | 1.0 | 0.4 | 0.0 | 0.4 |
| SDDSC110 | 400.55 | 401.20 | 0.7 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 401.20 | 401.90 | 0.7 | 9.4 | 1.0 | 11.2 |
| SDDSC110 | 402.50 | 403.25 | 0.8 | 0.7 | 0.1 | 0.8 |
| SDDSC110 | 403.25 | 404.00 | 0.8 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 404.00 | 404.70 | 0.7 | 0.1 | 0.0 | 0.2 |
| SDDSC110 | 409.50 | 410.58 | 1.1 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 410.58 | 411.68 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 414.00 | 415.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 448.06 | 448.53 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 469.80 | 470.82 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 471.70 | 472.80 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 474.00 | 475.18 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 475.18 | 476.05 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 478.00 | 479.15 | 1.2 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 481.50 | 482.60 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 482.60 | 483.80 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 483.80 | 485.00 | 1.2 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 494.00 | 495.09 | 1.1 | 0.1 | 0.0 | 0.2 |
| SDDSC110 | 517.20 | 518.06 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 519.00 | 520.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 534.91 | 535.23 | 0.3 | 1.4 | 0.3 | 2.0 |
| SDDSC110 | 535.23 | 536.21 | 1.0 | 0.6 | 0.6 | 1.7 |
| SDDSC110 | 551.00 | 551.98 | 1.0 | 0.3 | 0.1 | 0.4 |
| SDDSC110 | 551.98 | 553.15 | 1.2 | 0.4 | 0.1 | 0.5 |
| SDDSC110 | 553.15 | 554.00 | 0.9 | 0.3 | 0.0 | 0.4 |
| SDDSC110 | 554.00 | 555.22 | 1.2 | 0.1 | 0.0 | 0.2 |
| SDDSC110 | 555.22 | 556.20 | 1.0 | 0.4 | 0.1 | 0.5 |
| SDDSC110 | 556.20 | 557.30 | 1.1 | 1.8 | 0.6 | 2.8 |
| SDDSC110 | 557.30 | 557.98 | 0.7 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 567.00 | 568.03 | 1.0 | 0.4 | 0.2 | 0.8 |
| SDDSC110 | 578.80 | 580.00 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 583.55 | 584.80 | 1.3 | 0.1 | 0.0 | 0.1 |

| | | | | | | |
|---|---|---|---|---|---|---|
| SDDSC110 | 589.00 | 590.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 593.00 | 594.00 | 1.0 | 0.1 | 0.1 | 0.2 |
| SDDSC110 | 603.00 | 604.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 608.00 | 609.00 | 1.0 | 0.1 | 0.0 | 0.2 |
| SDDSC110 | 609.00 | 610.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 628.56 | 629.02 | 0.5 | 0.0 | 0.1 | 0.1 |
| SDDSC110 | 630.18 | 631.25 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 631.25 | 631.85 | 0.6 | 0.2 | 0.2 | 0.5 |
| SDDSC110 | 631.85 | 632.94 | 1.1 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 632.94 | 634.00 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 692.09 | 692.43 | 0.3 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 692.43 | 693.66 | 1.2 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 693.66 | 694.85 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 694.85 | 695.26 | 0.4 | 0.4 | 0.6 | 1.5 |
| SDDSC110 | 695.26 | 695.96 | 0.7 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 695.96 | 696.34 | 0.4 | 0.3 | 0.3 | 0.9 |
| SDDSC110 | 697.15 | 698.00 | 0.9 | 0.1 | 0.1 | 0.3 |
| SDDSC110 | 698.00 | 699.00 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 699.00 | 700.00 | 1.0 | 0.1 | 0.0 | 0.2 |
| SDDSC110 | 700.00 | 701.04 | 1.0 | 0.2 | 0.3 | 0.7 |
| SDDSC110 | 701.04 | 702.24 | 1.2 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 702.24 | 703.50 | 1.3 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 705.51 | 706.60 | 1.1 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 706.60 | 707.79 | 1.2 | 0.2 | 0.1 | 0.3 |
| SDDSC110 | 707.79 | 709.03 | 1.2 | 0.1 | 0.0 | 0.2 |
| SDDSC110 | 711.00 | 712.00 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 712.00 | 713.05 | 1.1 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 713.05 | 714.05 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 715.00 | 716.00 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 716.00 | 716.71 | 0.7 | 0.1 | 0.0 | 0.2 |
| SDDSC110 | 716.71 | 717.90 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 717.90 | 719.00 | 1.1 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 725.00 | 726.00 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 727.00 | 728.00 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 728.00 | 729.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 729.00 | 730.00 | 1.0 | 0.0 | 0.1 | 0.2 |
| SDDSC110 | 730.00 | 731.30 | 1.3 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 731.30 | 731.75 | 0.5 | 0.6 | 0.8 | 2.0 |
| SDDSC110 | 731.75 | 732.94 | 1.2 | 0.1 | 0.2 | 0.5 |
| SDDSC110 | 738.00 | 739.11 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 742.00 | 743.15 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 743.15 | 744.28 | 1.1 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 744.28 | 745.35 | 1.1 | 0.2 | 0.1 | 0.3 |

| | | | | | | |
|---|---|---|---|---|---|---|
| SDDSC110 | 745.35 | 746.39 | 1.0 | 0.6 | 0.0 | 0.6 |
| SDDSC110 | 746.39 | 747.50 | 1.1 | 0.1 | 0.0 | 0.2 |
| SDDSC110 | 747.50 | 748.62 | 1.1 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 749.71 | 750.77 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 750.77 | 751.82 | 1.1 | 0.4 | 0.0 | 0.5 |
| SDDSC110 | 751.82 | 752.37 | 0.6 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 757.52 | 758.70 | 1.2 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 758.70 | 759.68 | 1.0 | 0.9 | 0.0 | 0.9 |
| SDDSC110 | 759.68 | 760.50 | 0.8 | 1.3 | 0.0 | 1.3 |
| SDDSC110 | 760.50 | 761.50 | 1.0 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 761.50 | 762.15 | 0.7 | 0.0 | 0.0 | 0.1 |
| SDDSC110 | 762.15 | 762.75 | 0.6 | 0.9 | 0.4 | 1.6 |
| SDDSC110 | 765.35 | 766.32 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 766.32 | 767.40 | 1.1 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 767.40 | 768.41 | 1.0 | 0.3 | 0.2 | 0.6 |
| SDDSC110 | 768.41 | 769.65 | 1.2 | 0.1 | 0.1 | 0.2 |
| SDDSC110 | 769.65 | 770.30 | 0.7 | 0.2 | 0.0 | 0.3 |
| SDDSC110 | 770.30 | 771.00 | 0.7 | 0.4 | 0.1 | 0.7 |
| SDDSC110 | 771.00 | 772.18 | 1.2 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 772.18 | 773.30 | 1.1 | 0.4 | 0.0 | 0.5 |
| SDDSC110 | 773.30 | 773.50 | 0.2 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 773.50 | 774.55 | 1.1 | 0.6 | 0.0 | 0.6 |
| SDDSC110 | 774.55 | 775.70 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 776.90 | 777.82 | 0.9 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 778.30 | 779.20 | 0.9 | 0.6 | 0.0 | 0.6 |
| SDDSC110 | 779.20 | 779.53 | 0.3 | 0.6 | 0.1 | 0.7 |
| SDDSC110 | 779.53 | 780.50 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 780.50 | 781.50 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 781.50 | 782.68 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 783.56 | 784.15 | 0.6 | 0.1 | 0.0 | 0.2 |
| SDDSC110 | 784.15 | 785.05 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 785.05 | 786.26 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 786.26 | 787.26 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 787.99 | 789.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 789.00 | 790.00 | 1.0 | 1.6 | 0.0 | 1.6 |
| SDDSC110 | 791.00 | 792.14 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 793.38 | 794.54 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 794.54 | 795.70 | 1.2 | 0.4 | 0.0 | 0.4 |
| SDDSC110 | 795.70 | 796.87 | 1.2 | 0.3 | 0.1 | 0.4 |
| SDDSC110 | 796.87 | 798.00 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 798.00 | 799.18 | 1.2 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 799.18 | 800.00 | 0.8 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 800.00 | 801.00 | 1.0 | 0.2 | 0.0 | 0.2 |

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|---|---|---|---|---|---|---|
| SDDSC110 | 802.00 | 803.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 803.00 | 804.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 804.00 | 804.78 | 0.8 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 804.78 | 805.21 | 0.4 | 0.5 | 0.0 | 0.5 |
| SDDSC110 | 805.21 | 805.75 | 0.5 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 805.75 | 807.00 | 1.3 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 807.00 | 808.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 808.00 | 809.00 | 1.0 | 0.6 | 0.0 | 0.7 |
| SDDSC110 | 809.00 | 810.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 810.00 | 811.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 811.00 | 811.99 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 813.05 | 813.77 | 0.7 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 813.77 | 814.14 | 0.4 | 0.1 | 0.0 | 0.1 |
| SDDSC110 | 816.60 | 816.93 | 0.3 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 817.37 | 818.35 | 1.0 | 0.3 | 0.0 | 0.4 |
| SDDSC110 | 818.93 | 819.40 | 0.5 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 821.00 | 822.00 | 1.0 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 822.00 | 823.00 | 1.0 | 1.1 | 0.0 | 1.1 |
| SDDSC110 | 823.00 | 824.07 | 1.1 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 824.07 | 824.63 | 0.6 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 824.63 | 825.45 | 0.8 | 0.6 | 0.0 | 0.7 |
| SDDSC110 | 825.45 | 826.28 | 0.8 | 1.7 | 0.0 | 1.8 |
| SDDSC110 | 826.28 | 827.32 | 1.0 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 827.32 | 827.86 | 0.5 | 0.5 | 0.0 | 0.5 |
| SDDSC110 | 827.86 | 828.37 | 0.5 | 0.2 | 0.0 | 0.2 |
| SDDSC110 | 828.37 | 829.06 | 0.7 | 0.6 | 0.0 | 0.6 |
| SDDSC110 | 829.06 | 829.91 | 0.9 | 0.3 | 0.0 | 0.3 |
| SDDSC110 | 829.91 | 830.60 | 0.7 | 1.1 | 0.0 | 1.1 |
| SDDSC113 | 310.36 | 310.90 | 0.5 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 310.90 | 311.35 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 311.35 | 312.20 | 0.9 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 315.00 | 316.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 316.00 | 316.93 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 318.24 | 319.06 | 0.8 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 319.06 | 319.75 | 0.7 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 319.75 | 320.75 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 320.75 | 321.90 | 1.2 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 321.90 | 322.63 | 0.7 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 322.63 | 322.78 | 0.2 | 0.5 | 0.4 | 1.3 |
| SDDSC113 | 322.78 | 323.54 | 0.8 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 323.54 | 324.00 | 0.5 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 328.00 | 329.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 330.20 | 330.40 | 0.2 | 0.3 | 0.0 | 0.3 |

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|---|---|---|---|---|---|---|
| SDDSC113 | 330.40 | 331.00 | 0.6 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 331.00 | 332.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 332.00 | 333.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 333.00 | 334.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 335.00 | 336.00 | 1.0 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 337.00 | 337.20 | 0.2 | 0.8 | 3.6 | 7.6 |
| SDDSC113 | 337.20 | 338.06 | 0.9 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 338.06 | 338.26 | 0.2 | 2.5 | 0.0 | 2.6 |
| SDDSC113 | 338.26 | 339.00 | 0.7 | 7.0 | 0.0 | 7.0 |
| SDDSC113 | 339.00 | 339.81 | 0.8 | 0.4 | 0.0 | 0.4 |
| SDDSC113 | 339.81 | 340.49 | 0.7 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 340.49 | 340.70 | 0.2 | 0.3 | 0.1 | 0.4 |
| SDDSC113 | 340.70 | 341.39 | 0.7 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 341.39 | 341.94 | 0.6 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 341.94 | 342.45 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 342.45 | 342.91 | 0.5 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 342.91 | 343.53 | 0.6 | 0.4 | 0.0 | 0.4 |
| SDDSC113 | 343.53 | 344.18 | 0.7 | 0.7 | 0.0 | 0.7 |
| SDDSC113 | 344.18 | 345.37 | 1.2 | 0.7 | 0.0 | 0.7 |
| SDDSC113 | 345.37 | 345.68 | 0.3 | 4.2 | 0.7 | 5.6 |
| SDDSC113 | 345.68 | 346.07 | 0.4 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 346.07 | 346.67 | 0.6 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 346.67 | 347.79 | 1.1 | 1.0 | 0.0 | 1.0 |
| SDDSC113 | 347.79 | 348.48 | 0.7 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 352.90 | 353.50 | 0.6 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 355.78 | 356.71 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 357.48 | 358.06 | 0.6 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 358.06 | 359.00 | 0.9 | 1.4 | 0.0 | 1.4 |
| SDDSC113 | 359.00 | 360.00 | 1.0 | 0.4 | 0.0 | 0.4 |
| SDDSC113 | 360.82 | 361.05 | 0.2 | 1.5 | 2.5 | 6.3 |
| SDDSC113 | 362.65 | 363.55 | 0.9 | 0.4 | 0.0 | 0.4 |
| SDDSC113 | 363.55 | 364.85 | 1.3 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 365.55 | 366.20 | 0.7 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 379.70 | 380.80 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 384.60 | 385.30 | 0.7 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 405.65 | 405.98 | 0.3 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 405.98 | 406.30 | 0.3 | 0.6 | 0.0 | 0.6 |
| SDDSC113 | 406.30 | 406.60 | 0.3 | 1.9 | 0.0 | 1.9 |
| SDDSC113 | 406.60 | 407.30 | 0.7 | 2.1 | 0.0 | 2.2 |
| SDDSC113 | 407.30 | 407.65 | 0.4 | 3.7 | 0.0 | 3.7 |
| SDDSC113 | 407.65 | 408.10 | 0.5 | 4.8 | 0.0 | 4.8 |
| SDDSC113 | 408.10 | 408.65 | 0.6 | 4.3 | 0.1 | 4.4 |
| SDDSC113 | 408.65 | 409.00 | 0.4 | 5.0 | 0.1 | 5.1 |

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|---|---|---|---|---|---|---|
| SDDSC113 | 409.00 | 409.60 | 0.6 | 1.8 | 0.3 | 2.3 |
| SDDSC113 | 409.60 | 410.10 | 0.5 | 0.9 | 3.5 | 7.6 |
| SDDSC113 | 410.10 | 410.35 | 0.3 | 0.6 | 0.3 | 1.2 |
| SDDSC113 | 410.35 | 410.70 | 0.4 | 4.5 | 4.8 | 13.5 |
| SDDSC113 | 410.70 | 411.05 | 0.4 | 1.5 | 0.1 | 1.6 |
| SDDSC113 | 411.05 | 411.55 | 0.5 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 411.55 | 411.85 | 0.3 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 411.85 | 412.20 | 0.4 | 1.1 | 0.9 | 2.8 |
| SDDSC113 | 412.20 | 412.50 | 0.3 | 0.6 | 0.1 | 0.8 |
| SDDSC113 | 412.50 | 412.95 | 0.5 | 0.0 | 0.3 | 0.6 |
| SDDSC113 | 412.95 | 413.73 | 0.8 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 414.90 | 415.50 | 0.6 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 415.85 | 416.85 | 1.0 | 0.2 | 0.1 | 0.3 |
| SDDSC113 | 416.85 | 417.20 | 0.4 | 0.5 | 0.0 | 0.6 |
| SDDSC113 | 417.20 | 418.00 | 0.8 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 418.00 | 419.00 | 1.0 | 0.6 | 0.1 | 0.8 |
| SDDSC113 | 419.00 | 419.50 | 0.5 | 0.7 | 0.2 | 1.1 |
| SDDSC113 | 419.50 | 420.03 | 0.5 | 0.4 | 0.0 | 0.5 |
| SDDSC113 | 420.03 | 420.45 | 0.4 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 420.45 | 420.67 | 0.2 | 1.3 | 0.0 | 1.4 |
| SDDSC113 | 420.67 | 421.82 | 1.2 | 0.5 | 0.0 | 0.6 |
| SDDSC113 | 421.82 | 422.00 | 0.2 | 1.8 | 0.2 | 2.2 |
| SDDSC113 | 422.00 | 422.46 | 0.5 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 423.00 | 424.00 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 424.00 | 425.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 425.00 | 425.52 | 0.5 | 2.0 | 0.5 | 2.9 |
| SDDSC113 | 425.52 | 426.22 | 0.7 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 426.22 | 427.00 | 0.8 | 0.6 | 0.0 | 0.7 |
| SDDSC113 | 427.00 | 427.40 | 0.4 | 0.4 | 0.0 | 0.5 |
| SDDSC113 | 431.65 | 431.88 | 0.2 | 1.3 | 0.1 | 1.4 |
| SDDSC113 | 435.00 | 436.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 438.97 | 439.28 | 0.3 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 447.58 | 448.50 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 450.00 | 451.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 453.00 | 453.75 | 0.8 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 458.29 | 458.54 | 0.3 | 1.3 | 0.5 | 2.1 |
| SDDSC113 | 458.54 | 458.80 | 0.3 | 1.7 | 0.7 | 2.9 |
| SDDSC113 | 458.80 | 459.06 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 459.06 | 459.65 | 0.6 | 0.2 | 0.2 | 0.6 |
| SDDSC113 | 459.65 | 460.27 | 0.6 | 0.2 | 0.1 | 0.3 |
| SDDSC113 | 460.27 | 461.12 | 0.9 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 461.12 | 461.54 | 0.4 | 4.3 | 0.0 | 4.4 |
| SDDSC113 | 461.54 | 461.82 | 0.3 | 0.4 | 0.1 | 0.5 |

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|---|---|---|---|---|---|---|
| SDDSC113 | 463.72 | 464.67 | 1.0 | 0.1 | 0.1 | 0.2 |
| SDDSC113 | 464.67 | 464.98 | 0.3 | 0.2 | 0.9 | 2.0 |
| SDDSC113 | 464.98 | 465.46 | 0.5 | 0.0 | 0.2 | 0.4 |
| SDDSC113 | 465.46 | 465.72 | 0.3 | 8.0 | 1.1 | 10.0 |
| SDDSC113 | 465.72 | 466.70 | 1.0 | 0.0 | 0.1 | 0.2 |
| SDDSC113 | 466.70 | 467.25 | 0.6 | 0.2 | 0.2 | 0.6 |
| SDDSC113 | 467.25 | 468.10 | 0.9 | 0.2 | 0.1 | 0.3 |
| SDDSC113 | 468.10 | 468.34 | 0.2 | 366.0 | 0.2 | 366.4 |
| SDDSC113 | 468.34 | 468.74 | 0.4 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 468.74 | 468.98 | 0.2 | 206.0 | 1.3 | 208.4 |
| SDDSC113 | 471.96 | 472.70 | 0.7 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 472.70 | 473.28 | 0.6 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 473.28 | 474.00 | 0.7 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 474.88 | 475.11 | 0.2 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 476.00 | 477.00 | 1.0 | 0.4 | 0.0 | 0.4 |
| SDDSC113 | 477.00 | 477.38 | 0.4 | 1.8 | 0.0 | 1.8 |
| SDDSC113 | 477.38 | 477.58 | 0.2 | 0.7 | 0.0 | 0.7 |
| SDDSC113 | 480.10 | 481.06 | 1.0 | 0.1 | 0.3 | 0.6 |
| SDDSC113 | 481.06 | 481.37 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 482.00 | 482.24 | 0.2 | 1.9 | 0.0 | 1.9 |
| SDDSC113 | 487.00 | 488.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 490.88 | 491.10 | 0.2 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 492.00 | 492.30 | 0.3 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 493.30 | 493.86 | 0.6 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 493.86 | 494.38 | 0.5 | 1.3 | 0.0 | 1.3 |
| SDDSC113 | 494.38 | 495.00 | 0.6 | 0.4 | 0.0 | 0.4 |
| SDDSC113 | 498.76 | 499.06 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 502.00 | 502.80 | 0.8 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 502.80 | 503.46 | 0.7 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 505.00 | 506.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 506.00 | 506.61 | 0.6 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 508.78 | 509.31 | 0.5 | 0.5 | 0.0 | 0.5 |
| SDDSC113 | 509.88 | 510.23 | 0.4 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 511.00 | 512.00 | 1.0 | 0.4 | 0.0 | 0.4 |
| SDDSC113 | 512.00 | 513.00 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 513.00 | 513.90 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 513.90 | 514.60 | 0.7 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 514.60 | 515.00 | 0.4 | 0.3 | 0.1 | 0.4 |
| SDDSC113 | 515.00 | 515.70 | 0.7 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 515.70 | 516.27 | 0.6 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 517.89 | 518.20 | 0.3 | 0.1 | 0.2 | 0.5 |
| SDDSC113 | 518.20 | 518.51 | 0.3 | 0.5 | 0.3 | 0.9 |
| SDDSC113 | 518.51 | 518.90 | 0.4 | 14.8 | 0.8 | 16.3 |

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|---|---|---|---|---|---|---|
| SDDSC113 | 519.30 | 520.15 | 0.9 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 520.15 | 521.10 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 521.10 | 522.00 | 0.9 | 0.1 | 0.0 | 0.2 |
| SDDSC113 | 522.73 | 522.98 | 0.3 | 6.1 | 0.1 | 6.3 |
| SDDSC113 | 524.00 | 524.32 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 524.32 | 524.92 | 0.6 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 524.92 | 525.80 | 0.9 | 0.1 | 0.0 | 0.2 |
| SDDSC113 | 526.52 | 527.08 | 0.6 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 529.19 | 529.76 | 0.6 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 531.50 | 531.70 | 0.2 | 0.2 | 0.1 | 0.4 |
| SDDSC113 | 531.70 | 532.17 | 0.5 | 0.2 | 0.0 | 0.3 |
| SDDSC113 | 535.95 | 536.20 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 536.20 | 536.75 | 0.6 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 536.75 | 537.14 | 0.4 | 1.4 | 0.0 | 1.4 |
| SDDSC113 | 537.14 | 537.45 | 0.3 | 0.7 | 0.0 | 0.7 |
| SDDSC113 | 537.45 | 537.75 | 0.3 | 1.3 | 0.0 | 1.3 |
| SDDSC113 | 537.75 | 538.69 | 0.9 | 0.0 | 0.1 | 0.1 |
| SDDSC113 | 538.69 | 538.87 | 0.2 | 26.7 | 7.6 | 41.0 |
| SDDSC113 | 538.87 | 539.71 | 0.8 | 0.0 | 0.1 | 0.2 |
| SDDSC113 | 539.71 | 540.09 | 0.4 | 1.7 | 0.2 | 2.1 |
| SDDSC113 | 540.09 | 541.09 | 1.0 | 0.6 | 0.1 | 0.7 |
| SDDSC113 | 541.09 | 541.52 | 0.4 | 0.1 | 0.1 | 0.3 |
| SDDSC113 | 541.92 | 542.17 | 0.3 | 2.3 | 0.5 | 3.1 |
| SDDSC113 | 542.17 | 542.71 | 0.5 | 1.0 | 0.1 | 1.2 |
| SDDSC113 | 542.71 | 543.00 | 0.3 | 1.4 | 0.0 | 1.4 |
| SDDSC113 | 543.70 | 544.53 | 0.8 | 0.2 | 0.0 | 0.3 |
| SDDSC113 | 544.53 | 545.36 | 0.8 | 0.2 | 0.0 | 0.3 |
| SDDSC113 | 545.36 | 545.63 | 0.3 | 1.7 | 0.1 | 1.8 |
| SDDSC113 | 546.85 | 547.08 | 0.2 | 6.9 | 0.1 | 7.1 |
| SDDSC113 | 549.00 | 550.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 550.00 | 551.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 552.00 | 553.00 | 1.0 | 2.0 | 1.0 | 4.0 |
| SDDSC113 | 553.00 | 554.00 | 1.0 | 0.0 | 0.2 | 0.3 |
| SDDSC113 | 554.00 | 555.00 | 1.0 | 2.4 | 0.1 | 2.6 |
| SDDSC113 | 555.00 | 556.00 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 558.00 | 558.87 | 0.9 | 0.9 | 0.2 | 1.2 |
| SDDSC113 | 558.87 | 559.47 | 0.6 | 1.0 | 1.8 | 4.3 |
| SDDSC113 | 559.47 | 559.62 | 0.2 | 7.5 | 0.7 | 8.8 |
| SDDSC113 | 559.62 | 559.80 | 0.2 | 14.9 | 3.0 | 20.4 |
| SDDSC113 | 559.80 | 560.33 | 0.5 | 0.7 | 0.2 | 1.0 |
| SDDSC113 | 560.33 | 560.70 | 0.4 | 4.7 | 1.4 | 7.3 |
| SDDSC113 | 560.70 | 560.99 | 0.3 | 0.9 | 2.1 | 4.7 |
| SDDSC113 | 560.99 | 561.30 | 0.3 | 0.9 | 1.4 | 3.5 |

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|---|---|---|---|---|---|---|
| SDDSC113 | 561.30 | 561.83 | 0.5 | 0.1 | 0.1 | 0.2 |
| SDDSC113 | 561.83 | 562.07 | 0.2 | 1.5 | 0.5 | 2.5 |
| SDDSC113 | 562.07 | 562.64 | 0.6 | 0.2 | 0.4 | 1.0 |
| SDDSC113 | 562.64 | 562.87 | 0.2 | 0.1 | 0.2 | 0.5 |
| SDDSC113 | 562.87 | 563.44 | 0.6 | 19.9 | 1.0 | 21.8 |
| SDDSC113 | 563.44 | 563.72 | 0.3 | 0.3 | 1.5 | 3.1 |
| SDDSC113 | 563.72 | 564.37 | 0.7 | 0.2 | 0.3 | 0.7 |
| SDDSC113 | 564.37 | 564.53 | 0.2 | 15.9 | 4.5 | 24.4 |
| SDDSC113 | 564.53 | 565.05 | 0.5 | 0.0 | 0.2 | 0.4 |
| SDDSC113 | 565.05 | 565.27 | 0.2 | 0.3 | 1.9 | 3.9 |
| SDDSC113 | 565.27 | 565.52 | 0.3 | 0.5 | 0.4 | 1.1 |
| SDDSC113 | 565.52 | 565.79 | 0.3 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 565.79 | 566.39 | 0.6 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 566.39 | 566.90 | 0.5 | 0.1 | 0.0 | 0.2 |
| SDDSC113 | 566.90 | 567.09 | 0.2 | 61.1 | 10.6 | 81.0 |
| SDDSC113 | 567.09 | 567.35 | 0.3 | 0.1 | 0.0 | 0.2 |
| SDDSC113 | 567.35 | 568.00 | 0.7 | 1.5 | 1.2 | 3.6 |
| SDDSC113 | 568.00 | 569.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 569.00 | 570.00 | 1.0 | 0.4 | 0.0 | 0.4 |
| SDDSC113 | 570.00 | 571.00 | 1.0 | 0.3 | 1.3 | 2.7 |
| SDDSC113 | 572.00 | 572.26 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 572.26 | 572.54 | 0.3 | 6.3 | 7.8 | 20.9 |
| SDDSC113 | 572.54 | 572.83 | 0.3 | 48.4 | 2.2 | 52.5 |
| SDDSC113 | 572.83 | 573.31 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 573.31 | 573.50 | 0.2 | 0.1 | 0.9 | 1.8 |
| SDDSC113 | 573.50 | 574.24 | 0.7 | 0.0 | 0.1 | 0.1 |
| SDDSC113 | 574.76 | 575.55 | 0.8 | 0.1 | 0.0 | 0.2 |
| SDDSC113 | 575.55 | 575.68 | 0.1 | 0.4 | 0.5 | 1.4 |
| SDDSC113 | 575.68 | 576.11 | 0.4 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 576.11 | 576.49 | 0.4 | 1.4 | 0.4 | 2.1 |
| SDDSC113 | 578.34 | 578.71 | 0.4 | 1.4 | 0.8 | 3.0 |
| SDDSC113 | 578.71 | 579.25 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 579.25 | 579.81 | 0.6 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 579.81 | 580.02 | 0.2 | 5.2 | 7.2 | 18.8 |
| SDDSC113 | 580.02 | 580.23 | 0.2 | 0.7 | 0.4 | 1.5 |
| SDDSC113 | 580.23 | 580.57 | 0.3 | 136.0 | 18.4 | 170.6 |
| SDDSC113 | 580.57 | 580.87 | 0.3 | 23.6 | 2.4 | 28.1 |
| SDDSC113 | 580.87 | 581.15 | 0.3 | 0.5 | 0.1 | 0.7 |
| SDDSC113 | 581.15 | 582.00 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 582.00 | 583.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 583.00 | 584.00 | 1.0 | 0.1 | 0.0 | 0.2 |
| SDDSC113 | 584.93 | 585.42 | 0.5 | 0.4 | 0.3 | 0.9 |
| SDDSC113 | 585.42 | 585.63 | 0.2 | 0.3 | 0.1 | 0.4 |

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|---|---|---|---|---|---|---|
| SDDSC113 | 585.63 | 586.00 | 0.4 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 586.00 | 587.00 | 1.0 | 0.2 | 0.0 | 0.3 |
| SDDSC113 | 587.00 | 588.00 | 1.0 | 0.3 | 0.1 | 0.5 |
| SDDSC113 | 588.00 | 589.00 | 1.0 | 0.2 | 0.1 | 0.4 |
| SDDSC113 | 589.00 | 590.00 | 1.0 | 0.4 | 0.1 | 0.7 |
| SDDSC113 | 590.00 | 590.80 | 0.8 | 0.3 | 0.3 | 0.9 |
| SDDSC113 | 590.80 | 591.00 | 0.2 | 0.7 | 0.3 | 1.2 |
| SDDSC113 | 592.00 | 593.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 593.00 | 594.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 594.00 | 594.51 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 594.51 | 595.00 | 0.5 | 0.1 | 0.1 | 0.2 |
| SDDSC113 | 595.00 | 595.12 | 0.1 | 0.4 | 0.5 | 1.2 |
| SDDSC113 | 595.12 | 595.68 | 0.6 | 0.6 | 0.4 | 1.4 |
| SDDSC113 | 595.68 | 596.59 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 596.59 | 597.19 | 0.6 | 0.1 | 0.1 | 0.2 |
| SDDSC113 | 597.19 | 597.68 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 601.65 | 602.73 | 1.1 | 0.1 | 0.1 | 0.2 |
| SDDSC113 | 604.55 | 605.05 | 0.5 | 0.0 | 0.1 | 0.3 |
| SDDSC113 | 610.00 | 611.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 611.00 | 612.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 612.00 | 613.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 624.77 | 625.10 | 0.3 | 1.7 | 0.0 | 1.7 |
| SDDSC113 | 625.10 | 626.00 | 0.9 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 639.10 | 639.28 | 0.2 | 0.8 | 0.0 | 0.8 |
| SDDSC113 | 644.36 | 644.48 | 0.1 | 0.7 | 0.2 | 1.1 |
| SDDSC113 | 647.51 | 648.37 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 648.37 | 649.00 | 0.6 | 0.2 | 0.0 | 0.3 |
| SDDSC113 | 649.00 | 650.06 | 1.1 | 0.2 | 0.1 | 0.3 |
| SDDSC113 | 653.78 | 653.89 | 0.1 | 0.6 | 0.1 | 0.7 |
| SDDSC113 | 674.72 | 674.85 | 0.1 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 675.18 | 675.50 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 690.00 | 691.00 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 701.76 | 702.40 | 0.6 | 0.2 | 0.0 | 0.3 |
| SDDSC113 | 702.40 | 702.67 | 0.3 | 520.0 | 0.7 | 521.2 |
| SDDSC113 | 702.67 | 702.87 | 0.2 | 684.0 | 10.5 | 703.7 |
| SDDSC113 | 702.87 | 703.25 | 0.4 | 3.5 | 0.2 | 3.9 |
| SDDSC113 | 703.25 | 703.60 | 0.4 | 0.6 | 0.1 | 0.7 |
| SDDSC113 | 703.60 | 704.06 | 0.5 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 704.06 | 704.87 | 0.8 | 0.3 | 0.0 | 0.4 |
| SDDSC113 | 705.76 | 705.98 | 0.2 | 0.3 | 0.2 | 0.6 |
| SDDSC113 | 708.00 | 709.30 | 1.3 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 709.30 | 709.85 | 0.6 | 0.8 | 0.0 | 0.8 |
| SDDSC113 | 709.85 | 710.75 | 0.9 | 0.1 | 0.0 | 0.1 |

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|---|---|---|---|---|---|---|
| SDDSC113 | 710.75 | 711.60 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 715.00 | 715.85 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 717.60 | 717.85 | 0.3 | 1.0 | 0.2 | 1.5 |
| SDDSC113 | 717.85 | 719.00 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 719.00 | 719.50 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 719.50 | 720.40 | 0.9 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 720.40 | 721.40 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 721.40 | 722.00 | 0.6 | 1.3 | 0.3 | 1.8 |
| SDDSC113 | 722.00 | 722.90 | 0.9 | 0.6 | 0.0 | 0.6 |
| SDDSC113 | 722.90 | 723.25 | 0.4 | 2.1 | 0.2 | 2.5 |
| SDDSC113 | 723.25 | 723.55 | 0.3 | 0.7 | 0.4 | 1.5 |
| SDDSC113 | 723.55 | 723.85 | 0.3 | 0.9 | 0.1 | 1.0 |
| SDDSC113 | 723.85 | 724.80 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 724.80 | 725.75 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 725.75 | 727.00 | 1.3 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 728.40 | 729.47 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 729.47 | 730.30 | 0.8 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 730.30 | 731.23 | 0.9 | 9.7 | 0.4 | 10.4 |
| SDDSC113 | 733.00 | 734.00 | 1.0 | 0.1 | 0.1 | 0.3 |
| SDDSC113 | 734.00 | 735.00 | 1.0 | 0.1 | 0.1 | 0.2 |
| SDDSC113 | 735.00 | 736.00 | 1.0 | 0.3 | 0.2 | 0.7 |
| SDDSC113 | 736.00 | 737.05 | 1.1 | 1.5 | 0.0 | 1.6 |
| SDDSC113 | 737.05 | 737.20 | 0.2 | 125.0 | 1.8 | 128.4 |
| SDDSC113 | 737.20 | 738.00 | 0.8 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 738.00 | 739.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 744.00 | 745.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 745.00 | 746.00 | 1.0 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 749.00 | 750.00 | 1.0 | 0.3 | 0.0 | 0.4 |
| SDDSC113 | 750.00 | 750.96 | 1.0 | 0.2 | 0.1 | 0.3 |
| SDDSC113 | 750.96 | 751.17 | 0.2 | 38.8 | 0.0 | 38.9 |
| SDDSC113 | 751.17 | 751.51 | 0.3 | 6.0 | 0.0 | 6.1 |
| SDDSC113 | 751.51 | 752.32 | 0.8 | 99.8 | 0.1 | 99.9 |
| SDDSC113 | 752.32 | 752.90 | 0.6 | 0.3 | 0.1 | 0.5 |
| SDDSC113 | 752.90 | 753.50 | 0.6 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 753.50 | 754.00 | 0.5 | 4.5 | 2.9 | 9.9 |
| SDDSC113 | 754.90 | 755.10 | 0.2 | 0.3 | 1.4 | 2.9 |
| SDDSC113 | 755.10 | 756.00 | 0.9 | 0.0 | 0.0 | 0.1 |
| SDDSC113 | 757.00 | 758.00 | 1.0 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 758.00 | 759.00 | 1.0 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 759.00 | 760.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 762.00 | 763.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 766.00 | 767.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 767.00 | 768.00 | 1.0 | 0.1 | 0.0 | 0.1 |

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|---|---|---|---|---|---|---|
| SDDSC113 | 770.00 | 771.00 | 1.0 | 1.6 | 0.1 | 1.7 |
| SDDSC113 | 771.00 | 772.00 | 1.0 | 0.1 | 0.1 | 0.2 |
| SDDSC113 | 773.00 | 774.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 777.00 | 778.00 | 1.0 | 0.9 | 0.1 | 1.0 |
| SDDSC113 | 778.67 | 779.03 | 0.4 | 0.4 | 0.0 | 0.5 |
| SDDSC113 | 787.60 | 788.66 | 1.1 | 0.5 | 0.0 | 0.5 |
| SDDSC113 | 788.66 | 788.87 | 0.2 | 6.7 | 0.0 | 6.7 |
| SDDSC113 | 791.41 | 791.68 | 0.3 | 10.9 | 0.0 | 10.9 |
| SDDSC113 | 796.10 | 796.60 | 0.5 | 1.2 | 0.0 | 1.2 |
| SDDSC113 | 797.94 | 798.56 | 0.6 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 806.76 | 807.25 | 0.5 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 807.25 | 807.74 | 0.5 | 0.5 | 0.0 | 0.6 |
| SDDSC113 | 807.74 | 808.86 | 1.1 | 4.1 | 0.0 | 4.1 |
| SDDSC113 | 808.86 | 809.11 | 0.3 | 1.7 | 0.0 | 1.7 |
| SDDSC113 | 809.11 | 810.18 | 1.1 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 812.11 | 812.56 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 814.58 | 815.64 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 816.59 | 816.91 | 0.3 | 1.3 | 0.0 | 1.3 |
| SDDSC113 | 816.91 | 817.37 | 0.5 | 1.5 | 0.0 | 1.5 |
| SDDSC113 | 819.00 | 819.43 | 0.4 | 3.1 | 0.0 | 3.1 |
| SDDSC113 | 820.43 | 821.00 | 0.6 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 821.00 | 822.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 829.26 | 830.30 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 831.35 | 832.13 | 0.8 | 0.2 | 0.0 | 0.2 |
| SDDSC113 | 834.05 | 835.19 | 1.1 | 0.3 | 0.0 | 0.3 |
| SDDSC113 | 838.00 | 838.44 | 0.4 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 839.85 | 840.08 | 0.2 | 0.1 | 0.0 | 0.1 |
| SDDSC113 | 840.98 | 841.42 | 0.4 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 485.12 | 485.97 | 0.9 | 1.2 | 0.8 | 2.7 |
| SDDSC114 | 485.97 | 486.40 | 0.4 | 0.4 | 0.0 | 0.5 |
| SDDSC114 | 506.70 | 506.93 | 0.2 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 506.93 | 507.23 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 510.00 | 510.52 | 0.5 | 0.2 | 0.0 | 0.3 |
| SDDSC114 | 510.52 | 510.70 | 0.2 | 1.2 | 0.3 | 1.7 |
| SDDSC114 | 510.70 | 510.83 | 0.1 | 1.3 | 0.4 | 2.1 |
| SDDSC114 | 510.83 | 511.17 | 0.3 | 3.2 | 0.3 | 3.8 |
| SDDSC114 | 511.17 | 511.51 | 0.3 | 0.6 | 0.9 | 2.2 |
| SDDSC114 | 511.51 | 512.01 | 0.5 | 3.2 | 0.0 | 3.3 |
| SDDSC114 | 512.01 | 512.55 | 0.5 | 1.8 | 0.0 | 1.8 |
| SDDSC114 | 512.55 | 513.00 | 0.5 | 0.4 | 0.0 | 0.4 |
| SDDSC114 | 518.00 | 519.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 519.00 | 520.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 520.00 | 520.59 | 0.6 | 0.1 | 0.0 | 0.1 |

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|---|---|---|---|---|---|---|
| SDDSC114 | 520.59 | 521.00 | 0.4 | 1.3 | 0.0 | 1.3 |
| SDDSC114 | 525.00 | 526.05 | 1.1 | 0.5 | 0.0 | 0.6 |
| SDDSC114 | 526.05 | 526.20 | 0.2 | 0.9 | 0.4 | 1.6 |
| SDDSC114 | 526.20 | 526.34 | 0.1 | 4.9 | 0.3 | 5.3 |
| SDDSC114 | 526.34 | 526.80 | 0.5 | 0.4 | 0.2 | 0.8 |
| SDDSC114 | 526.80 | 528.00 | 1.2 | 0.3 | 0.0 | 0.4 |
| SDDSC114 | 531.00 | 532.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 532.00 | 533.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC114 | 564.58 | 564.74 | 0.2 | 2.1 | 4.5 | 10.5 |
| SDDSC114 | 564.74 | 565.00 | 0.3 | 0.0 | 0.0 | 0.1 |
| SDDSC114 | 569.46 | 570.40 | 0.9 | 0.2 | 0.0 | 0.3 |
| SDDSC114 | 573.40 | 573.66 | 0.3 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 580.14 | 580.35 | 0.2 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 585.00 | 586.00 | 1.0 | 0.2 | 0.0 | 0.2 |
| SDDSC114 | 589.11 | 589.29 | 0.2 | 0.9 | 0.0 | 0.9 |
| SDDSC114 | 622.06 | 622.48 | 0.4 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 622.48 | 623.00 | 0.5 | 0.5 | 0.0 | 0.6 |
| SDDSC114 | 623.62 | 623.85 | 0.2 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 623.85 | 624.62 | 0.8 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 625.42 | 626.45 | 1.0 | 0.1 | 0.0 | 0.2 |
| SDDSC114 | 626.45 | 627.13 | 0.7 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 627.13 | 627.30 | 0.2 | 0.4 | 0.0 | 0.4 |
| SDDSC114 | 628.17 | 628.50 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 628.50 | 628.74 | 0.2 | 122.0 | 3.8 | 129.1 |
| SDDSC114 | 628.74 | 629.00 | 0.3 | 0.5 | 0.1 | 0.6 |
| SDDSC114 | 629.00 | 629.17 | 0.2 | 16.3 | 4.1 | 24.1 |
| SDDSC114 | 629.17 | 629.57 | 0.4 | 0.0 | 0.0 | 0.1 |
| SDDSC114 | 629.57 | 630.43 | 0.9 | 2.1 | 1.6 | 5.1 |
| SDDSC114 | 630.43 | 630.96 | 0.5 | 0.1 | 0.0 | 0.2 |
| SDDSC114 | 630.96 | 631.20 | 0.2 | 21.3 | 8.8 | 37.8 |
| SDDSC114 | 637.27 | 637.73 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 639.00 | 639.21 | 0.2 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 699.77 | 700.25 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 718.00 | 719.00 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 723.29 | 723.72 | 0.4 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 723.72 | 724.45 | 0.7 | 0.8 | 0.1 | 1.0 |
| SDDSC114 | 724.45 | 724.78 | 0.3 | 6.6 | 0.3 | 7.2 |
| SDDSC114 | 744.60 | 745.45 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 759.02 | 759.45 | 0.4 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 766.45 | 766.90 | 0.5 | 2.1 | 0.2 | 2.5 |
| SDDSC114 | 766.90 | 767.45 | 0.6 | 0.5 | 0.3 | 0.9 |
| SDDSC114 | 767.45 | 768.05 | 0.6 | 56.0 | 0.6 | 57.1 |
| SDDSC114 | 768.05 | 768.45 | 0.4 | 36.1 | 0.1 | 36.3 |

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|---|---|---|---|---|---|---|
| SDDSC114 | 768.45 | 768.82 | 0.4 | 4.6 | 0.2 | 4.9 |
| SDDSC114 | 768.82 | 769.12 | 0.3 | 1.5 | 0.1 | 1.7 |
| SDDSC114 | 769.12 | 769.65 | 0.5 | 0.2 | 0.1 | 0.4 |
| SDDSC114 | 769.65 | 770.25 | 0.6 | 0.0 | 0.0 | 0.1 |
| SDDSC114 | 771.05 | 772.05 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 773.00 | 773.30 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 773.30 | 773.65 | 0.4 | 0.0 | 0.1 | 0.2 |
| SDDSC114 | 773.65 | 774.50 | 0.9 | 0.2 | 0.0 | 0.2 |
| SDDSC114 | 774.50 | 775.05 | 0.6 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 775.05 | 775.50 | 0.5 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 775.50 | 775.90 | 0.4 | 0.2 | 0.0 | 0.2 |
| SDDSC114 | 775.90 | 776.20 | 0.3 | 0.4 | 0.0 | 0.4 |
| SDDSC114 | 776.20 | 776.60 | 0.4 | 3.6 | 0.0 | 3.6 |
| SDDSC114 | 776.60 | 776.90 | 0.3 | 0.7 | 0.0 | 0.7 |
| SDDSC114 | 777.65 | 778.15 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 785.49 | 786.42 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 786.90 | 787.20 | 0.3 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 787.20 | 787.39 | 0.2 | 0.6 | 0.0 | 0.6 |
| SDDSC114 | 787.39 | 788.11 | 0.7 | 1.2 | 0.0 | 1.2 |
| SDDSC114 | 788.11 | 788.52 | 0.4 | 0.6 | 0.1 | 0.7 |
| SDDSC114 | 788.52 | 789.75 | 1.2 | 0.3 | 0.0 | 0.4 |
| SDDSC114 | 789.75 | 790.70 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 794.53 | 795.02 | 0.5 | 1.6 | 0.0 | 1.6 |
| SDDSC114 | 795.02 | 795.68 | 0.7 | 0.5 | 0.0 | 0.5 |
| SDDSC114 | 795.68 | 796.66 | 1.0 | 0.2 | 0.0 | 0.3 |
| SDDSC114 | 800.71 | 801.00 | 0.3 | 0.2 | 0.0 | 0.2 |
| SDDSC114 | 801.00 | 802.19 | 1.2 | 0.2 | 0.0 | 0.2 |
| SDDSC114 | 802.19 | 803.34 | 1.2 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 803.34 | 804.46 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 813.54 | 813.98 | 0.4 | 2.2 | 0.0 | 2.2 |
| SDDSC114 | 813.98 | 814.27 | 0.3 | 0.6 | 0.0 | 0.6 |
| SDDSC114 | 814.27 | 815.50 | 1.2 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 823.55 | 824.60 | 1.1 | 0.2 | 0.1 | 0.3 |
| SDDSC114 | 824.60 | 825.12 | 0.5 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 825.12 | 825.35 | 0.2 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 825.35 | 825.58 | 0.2 | 69.9 | 0.0 | 69.9 |
| SDDSC114 | 825.83 | 826.82 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 830.67 | 831.63 | 1.0 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 834.14 | 835.06 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 835.06 | 835.46 | 0.4 | 0.7 | 0.0 | 0.7 |
| SDDSC114 | 835.46 | 836.00 | 0.5 | 0.8 | 0.0 | 0.8 |
| SDDSC114 | 836.00 | 837.00 | 1.0 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 837.00 | 838.12 | 1.1 | 0.2 | 0.0 | 0.2 |

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|---|---|---|---|---|---|---|
| SDDSC114 | 838.12 | 839.00 | 0.9 | 0.7 | 0.0 | 0.7 |
| SDDSC114 | 839.00 | 839.28 | 0.3 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 839.28 | 840.03 | 0.8 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 840.61 | 841.53 | 0.9 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 841.53 | 842.17 | 0.6 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 842.17 | 842.33 | 0.2 | 0.2 | 0.0 | 0.2 |
| SDDSC114 | 842.69 | 843.28 | 0.6 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 843.28 | 843.77 | 0.5 | 0.8 | 0.0 | 0.8 |
| SDDSC114 | 843.77 | 844.25 | 0.5 | 0.2 | 0.0 | 0.2 |
| SDDSC114 | 844.25 | 844.71 | 0.5 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 844.71 | 845.33 | 0.6 | 10.5 | 0.0 | 10.5 |
| SDDSC114 | 848.08 | 849.20 | 1.1 | 0.1 | 0.0 | 0.1 |
| SDDSC114 | 849.20 | 849.46 | 0.3 | 0.3 | 0.0 | 0.3 |
| SDDSC114 | 851.83 | 853.00 | 1.2 | 0.1 | 0.0 | 0.1 |

## JORC Table 1

## Section 1 Sampling Techniques and Data

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| ***Sampling techniques*** | • *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*<br>• *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.*<br>• *Aspects of the determination of mineralisation that are Material to the Public Report.*<br>• *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.* | • Sampling has been conducted on drill core (half core for >90% and quarter core for check samples), grab samples (field samples of in-situ bedrock and boulders; including duplicate samples), trench samples (rock chips, including duplicates) and soil samples (including duplicate samples).<br>Locations of field samples were obtained by using a GPS, generally to an accuracy of within 5 metres. Drill hole and trench locations have been confirmed to <1 metre using a differential GPS.<br>Samples locations have also been verified by plotting locations on the high-resolution Lidar maps<br>• Drill core is marked for cutting and cut using an automated diamond saw used by Company staff in Kilmore.<br>Samples are bagged at the core saw and transported to the Bendigo OnSite Laboratory for assay.<br>At OnSite samples are crushed using a jaw crusher combined with a rotary splitter and a 1 kg split is separated for pulverizing (LM5) and assay.<br>• Standard fire assay techniques are used for gold assay on a 30 g charge by experienced staff (used to dealing with high sulphide and stibnite-rich charges). OnSite gold method by fire assay code PE01S.<br>• Screen fire assay is used to understand gold grain-size distribution where coarse gold is evident.<br>• ICP-OES is used to analyse the aqua regia digested pulp for an additional 12 elements (method BM011) and over-range antimony is measured using flame AAS (method known as B050).<br>• Soil samples were sieved in the field and an 80 mesh sample bagged and transported to ALS Global laboratories in Brisbane for super-low level gold analysis on a 50 g samples by method ST44 (using aqua regia and ICP-MS).<br>• Grab and rock chip samples are generally submitted to OnSite Laboratories for standard fire assay and 12 element ICP-OES as described above. |
| ***Drilling techniques*** | • *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diametre, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).* | • HQ diametre diamond drill core, oriented using Boart Longyear TruCore orientation tool with the orientation line marked on the base of the drill core by the driller/offsider.<br>A standard 3 metre core barrel has been found to be most effective in both the hard and soft rocks in the project. |
| ***Drill sample recovery*** | • *Method of recording and assessing core and chip sample recoveries and results assessed.* | • Core recoveries were maximised using HQ diamond drill core with careful control over water pressure to maintain soft-rock integrity and prevent loss of fines from soft drill core. Recoveries are determined on a metre-by-metre |

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| | • *Measures taken to maximise sample recovery and ensure representative nature of the samples.*<br>• *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.* | basis in the core shed using a tape measure against marked up drill core checking against driller's core blocks.<br>• Plots of grade versus recovery and RQD (described below) show no trends relating to loss of drill core, or fines. |
| ***Logging*** | • *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*<br>• *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.*<br>• *The total length and percentage of the relevant intersections logged.* | • Geotechnical logging of the drill core takes place on racks in the the company core shed.<br>Core orientations marked at the drill rig are checked for consistency, and base of core orientation lines are marked on core where two or more orientations match within 10 degrees.<br>Core recoveries are measured for each metre<br>RQD measurements (cumulative quantity of core sticks > 10 cm in a metre) are made on a metre by metre basis.<br>• Each tray of drill core is photographed (wet and dry) after it is fully marked up for sampling and cutting.<br>• The ½ core cutting line is placed approximately 10 degrees above the orientation line so the orientation line is retained in the core tray for future work.<br>• Geological logging of drill core includes the following parametres:<br>Rock types, lithology<br>Alteration<br>Structural information (orientations of veins, bedding, fractures using standard alpha-beta measurements from orientation line; or, in the case of un-oriented parts of the core, the alpha angles are measured)<br>Veining (quartz, carbonate, stibnite)<br>Key minerals (visible under hand lens, e.g. gold, stibnite)<br>• 100% of drill core is logged for all components described above into the company MX logging database.<br>• Logging is fully quantitative, although the description of lithology and alteration relies on visible observations by trained geologists.<br>• Each tray of drill core is photographed (wet and dry) after it is fully marked up for sampling and cutting.<br>• Logging is considered to be at an appropriate quantitative standard to use in future studies. |
| ***Sub-sampling techniques and sample preparation*** | • *If core, whether cut or sawn and whether quarter, half or all core taken.*<br>• *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.*<br>• *For all sample types, the nature, quality and appropriateness of the sample preparation technique.*<br>• *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* | • Drill core is typically sampled using half of the HD diametre. The drill core orientation line is retained.<br>• Quarter core is used when taking sampling duplicates (termed FDUP in the database).<br>• Sampling representivity is maximised by always taking the same side of the drill core (whenever oriented), and consistently drawing a cut line on the core where orientation is not possible. The field technician draws these lines. |

| Criteria | JORC Code explanation | Commentary |
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| | • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.*<br>• *Whether sample sizes are appropriate to the grain size of the material being sampled.* | • Sample sizes are maximised for coarse gold by using half core, and using quarter core and half core splits (laboratory duplicates) allows an estimation of nugget effect.<br>• In mineralised rock the company uses approximately 10% of ¼ core duplicates, certified reference materials (suitable OREAS materials), laboratory sample duplicates and instrument repeats.<br>• In the soil sampling program duplicates were obtained every 20$^{th}$ sample and the laboratory inserted low-level gold standards regularly into the sample flow. |
| ***Quality of assay data and laboratory tests*** | • *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*<br>• *For geophysical tools, spectrometres, handheld XRF instruments, etc, the parametres used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*<br>• *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.* | • The fire assay technique for gold used by OnSite is a globally recognised method, and over-range follow-ups including gravimetric finish and screen fire assay are standard. Of significance at the OnSite laboratory is the presence of fire assay personnel who are experienced in dealing with high sulphide charges (especially those with high stibnite contents) – this substantially reduces the risk of in accurate reporting in complex sulphide-gold charges.<br>• The ICP-OES technique is a standard analytical technique for assessing elemental concentrations. The digest used (aqua regia) is excellent for the dissolution of sulphides (in this case generally stibnite, pyrite and trace arsenopyrite), but other silicate-hosted elements, in particular vanadium (V), may only be partially dissolved. These silicate-hosted elements are not important in the determination of the quantity of gold, antimony, arsenic or sulphur.<br>• A portable XRF has been used in a qualitative manner on drill core to ensure appropriate core samples have been taken (no pXRF data are reported or included in the MX database).<br>• Acceptable levels of accuracy and precision have been established using the following methods<br>*¼ duplicates* – half core is split into quarters and given separate sample numbers (commonly in mineralised core) – low to medium gold grades indicate strong correlation, dropping as the gold grade increases over 40 g/t Au.<br>*Blanks* – blanks are inserted after visible gold and in strongly mineralised rocks to confirm that the crushing and pulping are not affected by gold smearing onto the crusher and LM5 swing mill surfaces. Results are excellent, generally below detection limit and a single sample at 0.03 g/t Au.<br>*Certified Reference Materials* – OREAS CRMs have been used throughout the project including blanks, low (<1 g/t Au), medium (up to 5 g/t Au) and high-grade gold samples (> 5 g/t Au). Results are automatically checked on data import into the MX database to fall within 2 standard deviations of the expected value.<br>*Laboratory splits* – OnSite conducts splits of both coarse crush and pulp |

| Criteria | JORC Code explanation | Commentary |
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| | | duplicates as quality control and reports all data. In particular, high Au samples have the most repeats.<br>*Laboratory CRMs* – OnSite regularly inserts their own CRM materials into the process flow and reports all data<br>*Laboratory precision* – duplicate measurements of solutions (both Au from fire assay and other elements from the aqua regia digests) are made regularly by the laboratory and reported.<br>• *Accuracy and precision* have been determined carefully by using the sampling and measurement techniques described above during the sampling (accuracy) and laboratory (accuracy and precision) stages of the analysis.<br>• *Soil sample* company duplicates and laboratory certified reference materials all fall within expected ranges. |
| ***Verification of sampling and assaying*** | • *The verification of significant intersections by either independent or alternative company personnel.*<br>• *The use of twinned holes.*<br>• *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.*<br>• *Discuss any adjustment to assay data.* | • The Independent Geologist has visited Sunday Creek drill sites and inspected drill core held at the Kilmore core shed.<br>• Visual inspection of drill intersections matches the both the geological descriptions in the database and the expected assay data (for example, gold and stibnite visible in drill core is matched by high Au and Sb results in assays).<br>• In addition, on receipt of results Company geologists assess the gold, antimony and arsenic results to verify that the intersections returned expected data.<br>• The electronic data storage in the MX database is of a high standard. Primary logging data are entered directly by the geologists and field technicians and the assay data are electronically matched against sample number on return from the laboratory.<br>• Certified reference materials, ¼ core field duplicates (FDUP), laboratory splits and duplicates and instrument repeats are all recorded in the database.<br>• Exports of data include all primary data, from hole SDDSC077B onwards after discussion with SRK Consulting. Prior to this gold was averaged across primary, field and lab duplicates.<br>• Adjustments to assay data are recorded by MX, and none are present (or required).<br>• Twinned drill holes are not available at this stage of the project. |
| ***Location of data points*** | • *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*<br>• *Specification of the grid system used.*<br>• *Quality and adequacy of topographic control.* | • Differential GPS used to locate drill collars, trenches and some workings<br>• Standard GPS for some field locations (grab and soils samples), verified against Lidar data.<br>• The grid system used throughout is Geocentric datum of Australia 1994; Map Grid Zone 55 (GDA94_Z55), also referred to as ELSG 28355.<br>• Topographic control is excellent owing to sub 10 cm accuracy from Lidar data. |

| Criteria | JORC Code explanation | Commentary |
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| ***Data spacing and distribution*** | • *Data spacing for reporting of Exploration Results.*<br>• *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.*<br>• *Whether sample compositing has been applied.* | • The data spacing is suitable for reporting of exploration results – evidence for this is based on the improving predictability of high grade gold-antimony intersections.<br>• At this time the data spacing and distribution are not sufficient for the reporting of Mineral Resource Estimates. This however may change as knowledge of grade controls increase with future drill programs.<br>• Sample compositing has not been applied to the reporting of any drill results. |
| ***Orientation of data in relation to geological structure*** | • *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*<br>• *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.* | • The true thickness of the mineralised intervals reported are interpreted to be approximately 50-60% of the sampled thickness.<br>• Drilling is oriented in an optimum direction when considering the combination of host rock orientation and apparent vein control on gold and antimony grade.<br>The steep nature of some of the veins may give increases in apparent thickness of some intersections, but more drilling is required to quantify.<br>• A sampling bias is not evident from the data collected to date (drill holes cut across mineralised structures at a moderate angle). |
| ***Sample security*** | • *The measures taken to ensure sample security.* | • Drill core is delivered to the Kilmore core logging shed by either the drill contractor or company field staff. Samples are marked up and cut by company staff at the Kilmore core shed, in an automated diamond saw and bagged before loaded onto strapped secured pallets and trucked by commercial transport to Bendigo for submission to the laboratory. There is no evidence in any stage of the process, or in the data for any sample security issues. |
| ***Audits or reviews*** | • *The results of any audits or reviews of sampling techniques and data.* | • Continuous monitoring of CRM results, blanks and duplicates is undertaken by geologists and the company data geologist. Mr Michael Hudson for SXG has the orientation, logging and assay data. |

## Section 2 Reporting of Exploration Results

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| ***Mineral tenement and land tenure status*** | • *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*<br>• *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.* | • The Sunday Creek Goldfield, containing the Clonbinane Project, is covered by the Retention Licence RL 6040 and is surrounded by Exploration Licence EL6163 and Exploration Licence EL7232. All the licences are 100% held by Clonbinane Goldfield Pty Ltd, a wholly owned subsidiary company of Southern Cross Gold Ltd. |
| ***Exploration done by other parties*** | • *Acknowledgment and appraisal of exploration by other parties.* | • The main historical prospect within the Sunday Creek project is the Clonbinane prospect, a high level orogenic (or epizonal) Fosterville-style deposit. Small scale mining has been undertaken in the project area since the 1880s continuing through to the early 1900s. Historical production occurred with multiple small shafts and alluvial workings across the Clonbinane Goldfield permits. Production of note occurred at the Clonbinane area with total production being reported as 41,000 oz gold at a grade of 33 g/t gold (Leggo and Holdsworth, 2013)<br>• Work in and nearby to the Sunday Creek Project area by previous explorers typically focused on finding bulk, shallow deposits. Beadell Resources were the first to drill deeper targets and Southern Cross have continued their work in the Sunday Creek Project area.<br>• EL54 - Eastern Prospectors Pty Ltd<br>Rock chip sampling around Christina, Apollo and Golden Dyke mines. Rock chip sampling down the Christina mine shaft. Resistivity survey over the Golden Dyke. Five diamond drill holes around Christina, two of which have assays.<br>• ELs 872 & 975 - CRA Exploration Pty Ltd<br>Exploration focused on finding low grade, high tonnage deposits. The tenements were relinquished after the area was found to be prospective but not economic.<br>Stream sediment samples around the Golden Dyke and Reedy Creek areas. Results were better around the Golden Dyke. 45 dump samples around Golden Dyke old workings showed good correlation between gold, arsenic and antimony.<br>Soil samples over the Golden Dyke to define boundaries of dyke and mineralization. Two costeans parallel to the Golden Dyke targeting soil anomalies. Costeans since rehabilitated by SXG.<br>• ELs 827 & 1520 - BHP Minerals Ltd<br>Exploration targeting open cut gold mineralization peripheral to SXG tenements.<br>• ELs 1534, 1603 & 3129 - Ausminde Holdings Pty Ltd |

| Criteria | JORC Code explanation | Commentary |
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| | | Targeting shallow, low grade gold. Trenching around the Golden Dyke prospect and results interpreted along with CRAs costeans. 29 RC/Aircore holes totalling 959 m sunk into the Apollo, Rising Sun and Golden Dyke target areas.<br>ELs 4460 & 4987 - Beadell Resources Ltd<br>• ELs 4460 & 4987 - Beadell Resources Ltd<br>ELs 4460 and 4497 were granted to Beadell Resources in November 2007. Beadell successfully drilled 30 RC holes, including second diamond tail holes in the Golden Dyke/Apollo target areas.<br>• Both tenements were 100% acquired by Auminco Goldfields Pty Ltd in late 2012 and combined into one tenement EL4987.<br>• Nagambie Resources Ltd purchased Auminco Goldfields in July 2014. EL4987 expired late 2015, during which time Nagambie Resources applied for a retention licence (RL6040) covering three square kilometres over the Sunday Creek Goldfield. RL6040 was granted July 2017.<br>• Clonbinane Gold Field Pty Ltd was purchased by Mawson Gold Ltd in February 2020.<br>Mawson drilled 30 holes for 6,928 m and made the first discoveries to depth. |
| ***Geology*** | • *Deposit type, geological setting and style of*<br>• *mineralisation.* | • Refer to the description in the main body of the release. |
| ***Drillhole Information*** | • *A summary of all information material to the understanding of the exploration results including a tabulation of the following*<br>• *information for all Material drill holes:*<br>○ *easting and northing of the drill hole collar*<br>○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar*<br>○ *dip and azimuth of the hole*<br>○ *down hole length and interception depth*<br>○ *hole length.*<br>• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.* | • Refer to appendices |
| ***Data aggregation methods*** | • *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg. cutting of high grades) and cut-off grades are usually Material and should be stated.*<br>• *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for* | • See “Further Information” and “Metal Equivalent Calculation” in main text of press release. |

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td>such aggregation should be stated and some typical examples of such aggregations should be shown in detail.<br>• The assumptions used for any reporting of metal equivalent values should be clearly stated.</td><td></td></tr>
<tr><td>Relationship between mineralisation widths and intercept lengths</td><td>• These relationships are particularly important in the reporting of Exploration Results.<br>• If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.<br>• If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg. ‘down hole<br>• length, true width not known’).</td><td>• See reporting of true widths in the body of the press release.</td></tr>
<tr><td>Diagrams</td><td>• Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</td><td>• The results of the diamond drilling are displayed in the figures in the announcement.</td></tr>
<tr><td>Balanced reporting</td><td>• Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</td><td>• All results above 0.1g/t Au have been tabulated in this announcement. The results are considered representative with no intended bias.<br>• Core loss, where material, is disclosed in tabulated drill intersections.</td></tr>
<tr><td>Other substantive exploration data</td><td>• Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</td><td>• Previously reported diamond drill drill results are displayed in plans, cross sections and long sections and discussed in the text and in the Competent Person’s statement.<br>• Preliminary testing (AMML Report 1801-1) has demonstrated the viability of recovering gold and antimony values to high value products by industry standard processing methods.<br>• The program was completed by AMML, an established mineral and metallurgical testing laboratory specialising in flotation, hydrometallurgy, gravity and comminution testwork at their testing facilities in Gosford, NSW. The program was supervised by Craig Brown of Resources Engineering & Management, who was engaged to develop plans for initial sighter flotation testing of samples from drilling of the Sunday Creek deposit.<br>• Two quarter core intercepts were selected for metallurgical test work (Table 1). A split of each was subjected to assay analysis The table below shows samples selected for metallurgical test work:
<table>
<tr><th>Sample Location</th><th>Sample Name</th><th>Weight (kg)</th><th>Drill hole</th><th>from (m)</th><th>to (m)</th></tr>
<tr><td>Rising Sun</td><td>RS01</td><td>22.8</td><td>MDDSC025</td><td>275.9</td><td>289.3</td></tr>
<tr><td>Apollo</td><td>AP01</td><td>16.6</td><td>SDDSC031</td><td>220.4</td><td>229.9</td></tr>
</table></td></tr>
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| Criteria | JORC Code explanation | Commentary |
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| | | The metallurgical characterisation test work included:<br>• Diagnostic LeachWELL testing.<br>• Gravity recovery by Knelson concentrator and hand panning.<br>• Timed flotation of combined gravity tails.<br>• Rougher-Cleaner flotation (without gravity separation), with sizing of products, to produce samples for mineralogical investigation.<br>• Mineral elemental concentrations and gold deportment was investigated using Laser Ablation examination by University of Tasmania.<br>• QXRD Mineralogical assessment were used to estimate mineral contents for the test products, and, from this, to assess performance in terms of minerals as well as elements, including contributions to gold deportment. For both test samples, observations and calculations indicated a high proportion of native ('free') gold: 84.0% in RS01 and 82.1% in AP01.<br>• Samples of size fractions of the three sulphide and gold containing flotation products from the Rougher-Cleaner test series were sent to MODA Microscopy for optical mineralogical assessment. Key observations were:<br>  ○ The highest gold grade samples from each test series found multiple grains of visible gold which were generally liberated, with minor association with stibnite (antimony sulphide).<br>  ○ Stibnite was highly liberated and was very 'clean' – 71.7% Sb, 28.3% S.<br>  ○ Arsenopyrite was also highly liberated indicating potential for separation.<br>  ○ Pyrite was largely free but exhibited some association with gangue minerals. |
| **Further work** | • *The nature and scale of planned further work (eg. tests for lateral extensions or depth extensions or large-scale step-out drilling).*<br>• *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.* | • The Company drilled 30,000 m in 2023 and plans to continue drilling with 4 diamond drill rigs. The Company has stated it will drill 19,000 m of drilling from September 2023 to April 2024. The company remains in an exploration stage to expand the mineralisation along strike and to depth.<br>• See diagrams in presentation which highlight current and future drill plans. |