

Feasibility Study Demonstrates Compelling Value Proposition for In-situ Resource Development at Century

New Century Resources Limited (Company or New Century) (ASX:NCZ) is pleased to provide the results of the In-situ Feasibility Study (Study), with defined in-situ resource deposits at Silver King and East Fault Block building on the existing tailings reprocessing operations.

Highlights:

- Strongly value accretive proposition for development of in-situ operations (initially Silver King and East Fault Block) alongside current tailings operations at Century
- Attractive in-situ operation economics (incremental to tailings):
 - At base case: Pre-tax NPV₈ A\$212M, IRR 102%, payback 2.2 years¹
 - At current spot: Pre-tax NPV₈ A\$234M, IRR 111%, payback 2.0 years²
- Increased zinc output and production of a new lead product with silver credits:
 - Average lead metal (in-concentrate) production output of 33,000tpa, containing 972,000oz pa silver
 - Average additional zinc metal (in-concentrate) production output 22,000tpa
- Premium lead concentrate product, grading 65-70% lead and 500-600g/t silver, providing attractive offtake finance options
- In-situ operation reduces Century wide C1 costs by US\$0.21/lb payable zinc, through the benefit of additional lead, zinc and silver metal output spread over Century's existing significant sunk capital base (in-situ operation C1 -US\$0.49/lb payable zinc)
- Estimated pre-production capital of A\$66.7M, with cost spread over the first ~15 months from initiation of project development
- Final Investment Decision (FID) to follow amendment to existing environmental approvals and completion of financing and joint venture assessment process
- Next steps:
 - Completion of Board approved Front End Engineering Design (FEED) works, operational readiness and long lead item procurement
 - Targeting FID in Q1 CY2022 and first production in Q1 CY2023

¹ Base case metal prices: Zn: US\$2,535/t, Pb: US\$2,205/t, Ag: US\$25/oz, 0.70 AUD:USD, see Table 1 (Page 3) and Table 2 (Page 4)

² Current spot metal prices: Zn: US\$3,030/t, Pb: US\$2,290/t, Ag: US\$23.9/oz, 0.736 AUD:USD

New Century Resources Ltd

Office Level 4, 360 Collins Street, Melbourne VIC 3000
 Phone +61 (3) 9070 3300
 Email info@newcenturyresources.com
 Website www.newcenturyresources.com

- **Upgraded Mineral Resource for Silver King and East Fault Block: 4.4Mt @ 4.8% Pb (209kt), 5.4% Zn (234kt), 47g/t Ag (6.6Moz) - (Meas/Ind/Inf)³**
- **Maiden Ore Reserve for Silver King and East Fault Block: 2.5Mt @ 5.3% Pb (133kt), 5.6% Zn (140kt), 68g/t Ag (5.4Moz) - (Probable)³**
- **Further resource upside potential via expanded exploration drilling of targets identified at Silver King (~5,000m drilling) and Watson's Lode (~4,000m drilling)**
- **Century Ore Reserves extend mine life to 2027**
- **Clear pathway to mine life extension to 2030 and beyond via conversion of Mineral Resources at Watson's Lode, South Block and further Silver King extensions⁴**

Cautionary Statements

As the Study utilises a portion of Inferred Resources, the ASX Listing Rules require a cautionary statement is included in this announcement. The Study referred to in this announcement is a study of the potential of combining the Company's in-situ resources with the Company's current tailings mining at the Century Mine.

The Study includes a proportion (14%) of Inferred Resources. There is a lower level of geological confidence associated with Inferred Resources and there is no certainty that further exploration work will result in the determination of Indicated Resources or that the production target will be realised. The Company has concluded however, that it has reasonable grounds for disclosing a mining and production target which includes 14% of Inferred Mineral Resources as the Inferred Resources used in the Study are not critical to the economic viability of the combined operations. Further evaluation work and appropriate studies are required before the Company will be in a position to estimate additional Ore Reserves to support a longer mine life.

New Century believes that the production target, forecast financial information derived from that target, and other forward-looking statements included in this announcement are based on reasonable grounds. However, neither the Company nor any other person makes or gives any representation, assurance or guarantee that the production target or expected outcomes reflected in this announcement in relation to the production target will ultimately be achieved.

Investors should note that the Company believes the commodity prices, AUD:USD exchange rate and other variables that have been assumed to estimate the potential revenues, cash flows and other financial information are based on reasonable grounds as at the date of this announcement. However, actual commodity prices, exchange rates and other variables may differ materially over the contemplated mine life and, accordingly, the potential revenue, cash flow figures and other financial information provided in this announcement should be considered as an estimate only that may differ materially from actual results. Accordingly, the Company cautions investors from relying on the forecast information in this announcement and investors should not make any investment decisions based solely on the results.

Several key steps need to be completed to achieve the expansion of production at the Century Mine. Many of those steps are referred to in this announcement. Investors should note that if there are any delays associated with completing those steps, or completion of the steps does not yield the expected results, the actual revenue and cash flow figures may differ materially from the Study results presented in this announcement.

To achieve the range of outcomes indicated in this announcement, funding, including working capital, in the order of A\$83.5 million will likely be required. The Company is generating cashflow from operations, has existing cash reserves, and has a financing facility through Vårde Partners. Any start-up working capital requirement is anticipated to be covered by the cash flow generation of the existing operations or alternatively financing facilities, however investors should note there is no certainty that cashflow available from existing operations will be sufficient, or that the Company will be able to raise any additional funding if needed. It is also possible that funding may only be available on terms that may be dilutive to or otherwise affect the value of the Company's existing shares.

³ See pages 8 and 9 for further details on the upgraded Silver King Mineral Resource and maiden Ore Reserve for the Silver King and East Fault Block deposits.

⁴ See ASX Announcement dated 02 September 2021 for further details on the maiden Inferred Mineral Resource for Watson's Lode.

Table 1: In-situ Feasibility Study Life of Mine Summary - Physicals

Item	Units	Silver King Underground	Silver King Open Pit	East Fault Block Open Pit	Total
Mining					
Ore Mined	Mt	2.0	0.3	0.6	2.9
Waste Mined	Mt	1.4	2.1	7.7	11.2
Open Pit Strip Ratio ¹	-	-	6.8	13.4	-
Processing					
Feed Grade²					
Zinc	%	4.3%	2.3%	8.5%	4.9%
Lead	%	7.1%	4.4%	0.9%	5.6%
Silver	g/t	78	28	36	65
Recovery³					
Zinc (into Zinc Concentrate)	%	70%	70%	70%	70%
Lead (into Lead Concentrate)	%	84%	84%	60%	79%
Silver (into Zinc Concentrate)	%	10%	10%	35%	15%
Silver (into Lead Concentrate)	%	70%	70%	35%	63%
Production					
Recovered Metal					
Zinc	kt	57.2	6.4	34.2	97.8
Lead	kt	113.3	12.3	3.3	128.9
Silver	kOz	3,744	276	473	4,494
Payable Metal⁴					
Zinc (Zinc Concentrate)	kt	47.7	5.3	28.5	81.5
Lead (Lead Concentrate)	kt	107.7	11.7	3.1	122.4
Silver (Zinc and Lead Cons)	kOz	3,141	209	249	3,599
Products⁵					
Zn Concentrate (dry basis)	kt	119.2	13.2	71.3	203.8
Lead Concentrate (dry basis)	kt	164.2	17.8	4.7	186.8

1. Strip ratio for Silver King open pit and East Fault Block open pit
2. Average metal grades based on life of mine material reporting to the processing plant
3. Average recoveries based on steady state operations post ramp up
4. Please see 'Zinc and Lead Concentrate Marketing' section on Page 17 for further details on metal payability
5. In-situ and tailings initially processed via separate existing zinc rougher and scavenger circuits, followed by combined feed for Zinc Cleaner 2 circuit, see Figure 6

Table 2: In-situ Feasibility Study Life of Mine Summary - Financials

Item	Units	Total In-situ (Base Case)	Total In-situ (Current Spot)
Economic Assumptions¹			
Zinc Price	US\$/t	2,535	3,030
Lead Price	US\$/t	2,205	2,290
Silver Price	US\$/oz	25	23.9
Exchange Rate	US\$:A\$	0.70	0.736
Project Cash Flow			
Net Smelter Revenue	A\$m	709.3	738.5
EBITDA	A\$m	384.4	412.0
Maximum Cash Draw (including working capital) ²	A\$m	83.5	83.4
Sustaining Costs & Rehabilitation	A\$m	14.3	14.3
Net Project Cash Flow (pre-tax)	A\$m	286.7	314.3
Financial Metrics			
Pre-tax NPV ₈	A\$m	212.0	233.9
Pre-tax IRR	%	102%	111%
Pre-tax Payback Period	Yrs	2.2	2.0
NPV/Capex	-	3.8	4.1

1. Commodity price and metal exchange rate assumed to be flat over life of mine for Base Case
2. Represents all capital requirements including appropriate contingency and working capital allowances for in-situ development. Costs for plant, site services, etc are distributed between the three deposits based on life of mine throughput and working capital is expected to be recovered at end of in-situ operations.

Table 3: In-situ Feasibility Study Life of Mine Summary - In-situ Operating Cost¹

Item	US\$/lb Zn ²
Mining	0.55
Processing	0.31
Site G&A	0.14
Transport	0.12
Treatment Charges ³	0.37
C1 Cost (excl Lead & Silver Credits)⁴	1.49
Lead Credit	-1.50
Silver Credit	-0.48
C1 Cost (incl. Lead & Silver Credits)⁴	-0.49
Royalties	0.19
Corporate Costs	0.01
Sustaining Capex	0.05
All-in Sustaining Cost (AISC)	-0.24

1. In-situ mined ore only, excludes tailings
2. Payable metal basis, in-situ metal production only
3. Zinc concentrate and lead concentrate treatment charges
4. C1 is defined as direct cash operating costs produced, net of by-product credits, divided by the amount of payable zinc produced. Direct cash operating costs include all mining, processing, transport, treatment costs and smelter recovery deductions through to refined metal.

Operations Overview

Mine Location and History

The Century Zinc Mine (**Century Mine or Operation**) is located in north-west Queensland approximately 250km from Mt Isa. Production at Century began in 2000 and was one of the largest zinc mines in the world, producing 475,000tpa zinc and 50,000tpa lead concentrates using conventional open-pit mining, grinding and flotation at the Lawn Hill mine site. Processed concentrates were transferred along a 304km underground slurry pipeline to Century's port facility at Karumba, on the Gulf of Carpentaria. Concentrates were then dewatered before being transported on the M.V. Wunma transshipment vessel to export ships anchored offshore and then sold to smelters globally. The Mine was placed on care in maintenance in 2016 by the previous owners and acquired by New Century in 2017.



Figure 1: Century Mine and regional infrastructure overview

Since acquiring the Century Mine, the Company restarted operations through the reprocessing of the large tailings Ore Reserve on the mine site. Tailings operations commenced in August 2018. Since that time, Century has produced over 650,000t of zinc concentrate and is currently one of the top 15 largest zinc operations globally.

Study Aims and Scope

The Study investigated the incorporation of Silver King and East Fault Block in-situ deposits into the existing mine plan (in addition to the current tailings reprocessing) to produce zinc concentrate and a new lead concentrate (**Project**). Metal production and economics for in-situ ore processing reported here exclude tailings (i.e. are incremental to tailings). The Study aimed to:

- increase metal production at a lower average C1 cost while maintaining the current tailings mining rate; and
- increase the overall cashflow generated by the Project.

Mineral Resources and Ore Reserves

The current tailings Ore Reserve (49.3Mt at 3.0% Zn and 14g/t Ag, as at 30 June 2021) provides base production, with in-situ resources under the Study providing additional production. The two in-situ deposits on the mining lease (Silver King and East Fault Block) are located less than 2km from the processing plant and have been used as the feed source for the current Study, with two additional deposits on the Company's leases (South Block and Watson's Lode) to be assessed for potential mine life extension in due course.

The following is an overview of the defined deposits for the Project:

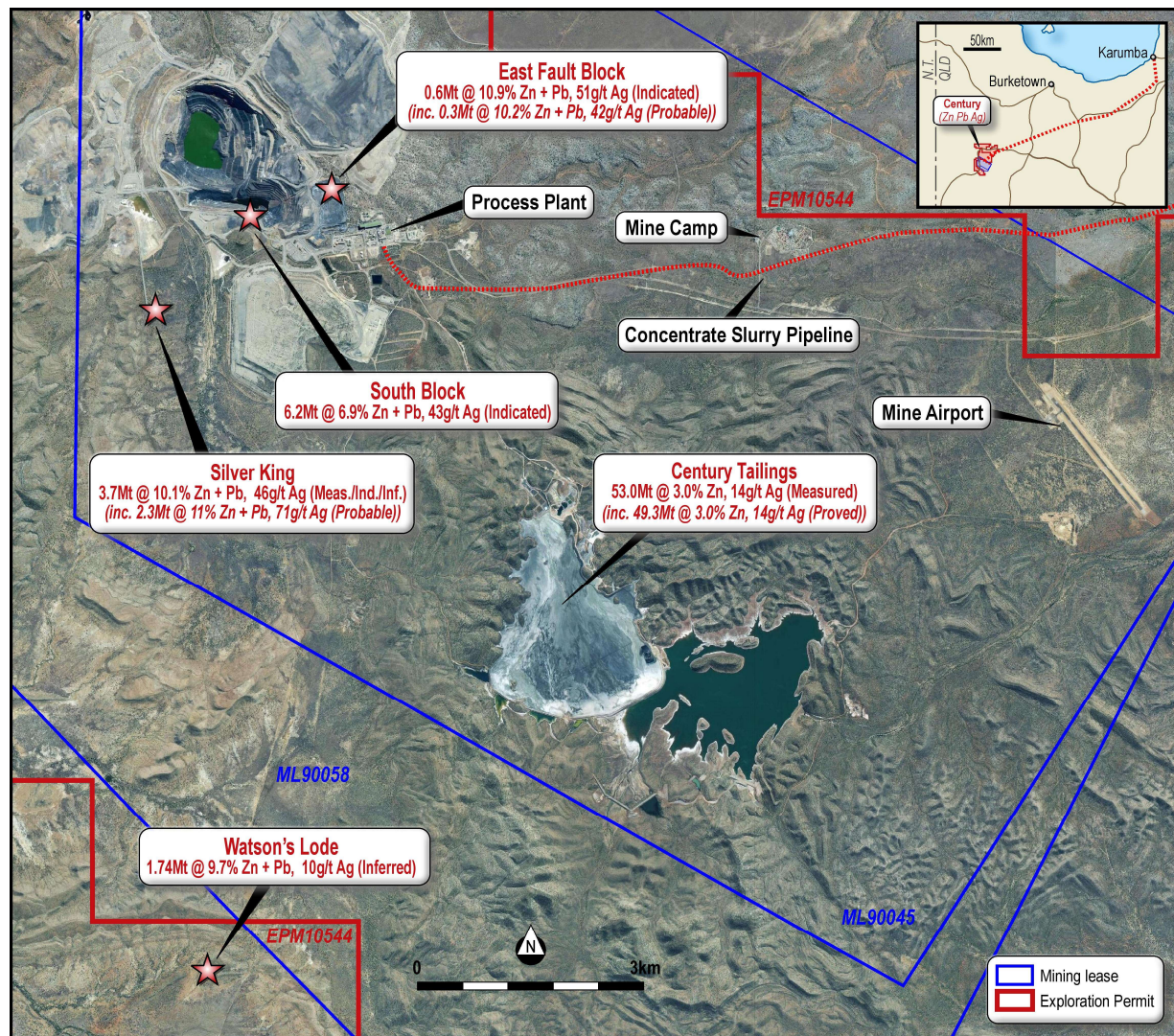


Figure 2: Century Deposit Overview

Mineral Resources

- The **Silver King deposit** is a high-grade vein style deposit located to the south-west of the original open pit and extends along strike. Recent exploration work has highlighted the extension potential for Silver King, with an identified prospective Silver King vein repeat (to the south) and a splay off the main vein (to the north-west)⁵
- The **East Fault Block deposit** is a pod of the original Century ore deposit and is located on the north-west corner of the previous run of mine (**ROM**) pad.

Whilst not included in the Study mine plan, there are two additional identified Mineral Resources at Century which will form the basis of potential future mine life extension:

- The **South Block deposit** was the final cutback of the original “Big Zinc” deposit and was never mined by the previous owners due to a site of cultural significance, known as Magazine Hill, located adjacent to the deposit. In May 2018, the Queensland Government registered a Cultural Heritage Agreement between the Company and the Native Title holders to allow for the potential impact on Magazine Hill through the mining of South Block. Notwithstanding this access agreement being in place, the Company is focused on mining methods for South Block development which won’t require the removal of Magazine Hill.
- The **Watson’s Lode deposit**⁶ is located on EPM 10544 surrounding the Century mining leases and is approximately 10km from the existing Century processing plant. Watson’s Lode is a vein-style system, consisting of predominately epithermal quartz carbonate breccias with varying contents of sphalerite, galena, chalcopyrite, pyrite and siderite.

The current total in-situ Mineral Resources at the Century Mine (inclusive of Ore Reserves) are:

Table 4: In-situ Mineral Resources (Measured, Indicated and Inferred)^{2,3,4}

Project	Measured				Indicated				Inferred				Total						
	Mt	Zn (%)	Pb (%)	Ag (g/t)	Mt	Zn (%)	Pb (%)	Ag (g/t)	Mt	Zn (%)	Pb (%)	Ag (g/t)	Mt	Zn (%)	Pb (%)	Ag (g/t)	Zn (kt)	Pb (kt)	Ag (MOz)
Silver King ¹	1.0	5.1	5.7	58	2.1	5	5.2	44	0.6	2.5	6	32	3.7	4.5	5.5	44	170	202	5.4
East Fault Block	-	-	-	-	0.6	9.8	1.1	51	-	-	-	-	0.6	9.8	1.1	51	63	7	1.1
South Block	-	-	-	-	6.2	5.4	1.5	43	-	-	-	-	6.2	5.4	1.5	43	335	93	8.6
Watson’s Lode	-	-	-	-	-	-	-	-	1.7	7.7	2	10	1.7	7.7	2	10	134	35	0.6
In-situ Total	1.0	5.1	5.7	58	8.8	5.5	2.4	44	2.3	6.4	3	16	12.2	5.7	2.8	39	702	334	15.8
Tailings	53.0	3	-	14	-	-	-	-	-	-	-	-	53	3	-	14	1,604	-	24.0

1. Total including underground and open pit
2. See the Appendix of this announcement for further details
3. Tonnes and grades are rounded
4. Mineral Resources as of 30 June 2021

Further details on Mineral Resources can be found in Appendix 2 and Appendix 3.

Ore Reserves

In conjunction with the Study, New Century is pleased to announce a maiden Ore Reserve for the Silver King and East Fault Block deposits.

⁵ See ASX Announcement dated 07 June 2021 for further details on Silver King drilling and resource definition program

⁶ See ASX Announcement dated 02 September 2021 for further details on the maiden Inferred Mineral Resource for Watson’s Lode

The Study has been used as the basis to estimate Ore Reserves for the Project reported in accordance with the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (**JORC Code**). The Ore Reserve was estimated from the Mineral Resource after consideration of the level of confidence in the Mineral Resource and considering material and relevant modifying factors. Details of the material assumptions underpinning the Ore Reserve are set out in the sections below and Appendix 2 (JORC Table 1) of this announcement.

Table 5: Century In-situ Ore Reserve Statement^{1,2,3,4}

Project	Type	Cut-off NSR ⁴ (AUD/t)	Proved				Probable				Total						
			Mt	Zn (%)	Pb (%)	Ag (g/t)	Mt	Zn (%)	Pb (%)	Ag (g/t)	Mt	Zn (%)	Pb (%)	Ag (g/t)	Zn (kt)	Pb (kt)	Ag (MOz)
Silver King	Underground	53	-	-	-	-	1.7	4.7	6.9	83	1.7	4.7	6.9	83	78	114	4.5
Silver King	Open Pit	38	-	-	-	-	0.6	8.5	0.9	36	0.6	8.5	0.9	36	49	5	0.7
East Fault Block	Open Pit	38	-	-	-	-	0.3	5.1	5.1	42	0.3	5.1	5.1	42	13	13	0.4
In-situ Total			-	-	-	-	2.5	5.6	5.3	68	2.5	5.6	5.3	68	140	133	5.4
Tailings		29	49.3	3.1	3	13.8	-	-	-	-	49.3	3.1	-	13.8	1,473	-	22.0

1. Ore Reserves are a subset of Mineral Resources
2. Ore Reserves are estimated using a zinc price of US\$2,450/tonne, a lead price of US\$1,750/tonne and silver price of US\$22/oz and exchange rate of 0.74 USD:AUD
3. The above data has been rounded to the nearest 100,000 tonnes, 0.1% lead grade and 10,000 lead tonnes, 1g/t silver grade and 1,000,000 silver ounces. Errors of summation may occur due to rounding.
4. Revenue is calculated using a Net Smelter Return (NSR) formula applied to mining shapes due to the multiple revenue streams available from contributing metals (zinc, lead, silver). The NSR calculation estimates the value of the ore by subtracting estimated shipping costs, treatment charges, royalties and selling costs from the gross value of the recovered metal in ore.

The Ore Reserve estimate is based on the operating methodology, modifying factors and unit cost estimates for the base case reported in the Study.

Measured and Indicated Mineral Resources for Silver King and East Fault Block have been converted to Probable Ore Reserves subject to mine design physicals and an economic evaluation. Any Inferred material contained within the mine plan has been treated as waste. The Ore Reserves have been defined at delivery to the processing plant ROM pad.

The Ore Reserve mining cost estimation has been prepared using the Study financial model populated with Ore Reserve physicals. The Ore Reserve capital cost estimate has adopted the detail developed for the Study base case. These parameters are detailed in the 'Capital Cost' section below.

The Ore Reserve processing costs and recoveries have assumed the same factors/rates developed for the base case for the Study. These parameters are detailed in Table 1 in Appendix 2.

The Ore Reserve schedule mining sequence and mine productivities are consistent with those adopted for the Study and differs only in its treatment of Inferred Mineral Resource material contained within the ore delivery to the ROM. A detailed financial assessment indicated positive economic outcomes for the Ore Reserve schedule, without inclusion of Inferred Mineral Resources.

For Silver King, lead is the dominant income stream accounting for approximately 55% of Project revenue, remaining value is recognised from silver and zinc. For East Fault Block, zinc is the dominant income stream accounting for approximately 85% of Project revenue, remaining value is recognised from silver and lead.

A discounted cashflow analysis (DCF) was conducted on the Ore Reserve cashflows to determine the Net Present Value (NPV), which was found to be positive across a range of $\pm 20\%$ for key variables that could be expected to influence pre-tax cashflows, value and returns. The Project is most sensitive to revenue related factors in isolation, followed by operating costs then capital costs. This is typical for a Project of this nature and scale. There is a slight bias to the upside in that positive sensitivities generally have a greater positive impact than an equal and opposite negative move.

Mining

Silver King: Underground

The underground mining methods employed in the Silver King mine design include a mixture of sub level open stoping methods, listed in order of prevalence in the mine plan; modified Avoca, transverse stoping in wide ore zones including double lift stoping where hanging wall conditions permit, uphole stoping, and floor benching with post cemented rock fill to establish sill pillars.

Access to the underground workings will be via a decline, located on the footwall side of the Silver King ore body at an average gradient of 1 in 8 down. The nominal production level interval is 20m vertically. However, this may vary locally to maximise ore extraction in line with the geology of the orebody.

Development ground support has been designed in line with the rock mass characterisation with over all stability being high. Minimal geotechnical risk is forecast within the stopes under the proposed dimensions with hanging wall stability relatively high.

The underground mine plan includes a mix of waste rock fill and cemented rock fill. Only fresh, or unoxidized material will be stockpiled and utilised for stope back fill. Weathered waste rock material sourced from the Silver King open pit, boxcut and initial decline development will be adequately segregated during waste rock dump construction.

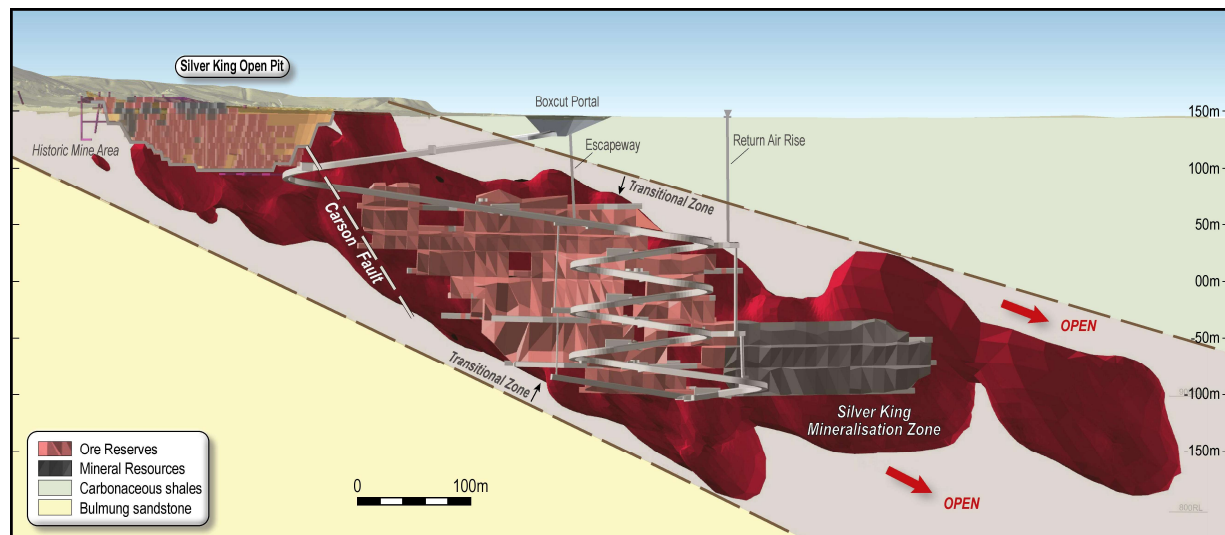


Figure 3: Silver King Life of Mine Plan, 2 (Pink) = Probable Reserve. 3 (Grey) = Inferred Mining Shapes
Dilution factors and recoveries were determined by ore category (development or stoping/production) with stoping ore separated into large, medium and small stopes. Dilution of

average 10% was applied to the development ore. Mining recoveries of 95% and 100% were applied to stoping ore and development ore respectively.

The underground mine plan consists of 2.03Mt of ore with average zinc, lead and silver grades of 4.3%, 7.1% and 78g/t respectively. This includes 1.67Mt of Probable ore. A stoping cut-off grade of NSR AUD\$105/t NSR was applied, with incremental ore recoverable down to NSR AUD\$53/t.

Open Pit Operations

The potential for the shallow Silver King and East Fault Block mineral resources to be extracted has been assessed using conventional open pit mining design and evaluation techniques. Rock will be fractured through drilling and blasting, then will be delivered to nominated locations using an excavator and truck. Mining costs have been derived from a first-principles techniques for a small-medium scale open pit mining operation.

Ore will be hauled directly to the existing ROM pad at the processing plant. Waste material will preferentially be used for underground backfill or alternately placed on in-pit waste dumps, with non-acid forming waste being taken to designated waste dumps for progressive rehabilitation capping.

An integrated process was conducted to establish the mining schedule, determining that the Silver King Underground ore would underpin the schedule, with the open pits providing incremental feed during periods when underground operations are unable to meet the full ore feed requirements.

Open pit mining at Century has an established history with open pit operations being undertaken over approximately 16 years. All mining support infrastructure remains at Century with only modest refurbishment costs to recommission. With the depletion of the original Century Ore Reserve, much of the mobile mining equipment was demobilised from site, except for a small fleet which was retained to complete rehabilitation works. This provides a low-cost opportunity to re-establish open pit operations and concurrently complete a portion of the environmental rehabilitation works required for final closure. New Century's current mining fleet on site consists of one 180t Komatsu PC1800 diesel-hydraulic excavator, one 200T Komatsu PC2000 diesel-hydraulic excavator, five 170t payload Komatsu 630E rigid dump trucks and a small fleet of the necessary ancillary equipment.

Silver King: Open Pit

The portion of the Silver King deposit assessed for open pit extraction is 400m along a north-east strike and dipping approximately 60° to the north-west. The mineralized material outcrops and extends to a maximum depth of approximately 140m. The width of the deposit varies depending on the depth and is typically between 5 to 10m, reaching 20m wide at its maximum.

Figure 3 shows the location of the pit relative to the underground mine, illustrating that the remaining ore below the pit bottom has potential for extraction by underground mining methods (not contemplated in the current study).

The mine plan consists of 303kt of ore with average zinc, lead and silver grades of 2.3%, 4.4% and 28g/t respectively. This includes 40kt inferred, 146kt indicated and 103kt measured ore, plus diluting material. The low strip ratio of 6.8 is due to the location of the ore close to surface, minimising waste stripping. An ore dilution of 9% and a mining recovery of 97% were applied. A cut-off grade of NSR AUD\$38/t was applied.

East Fault Block: Open Pit

Mineralisation starts at approximately 40m below the surface with a strike length of approximately 230m. The ore body extends to a depth of 95m and is 30m wide for the bulk of the economically recoverable blocks. A strip ratio of 13.4 was generated from the designed pit shape. The mine plan includes 577kt of indicated ore, inclusive of dilution, with average zinc, lead and silver grades of 8.5%, 0.9% and 36g/t respectively. No inferred or measured ore was included in the design. A cut-off grade of NSR \$AUD 38/t was applied.

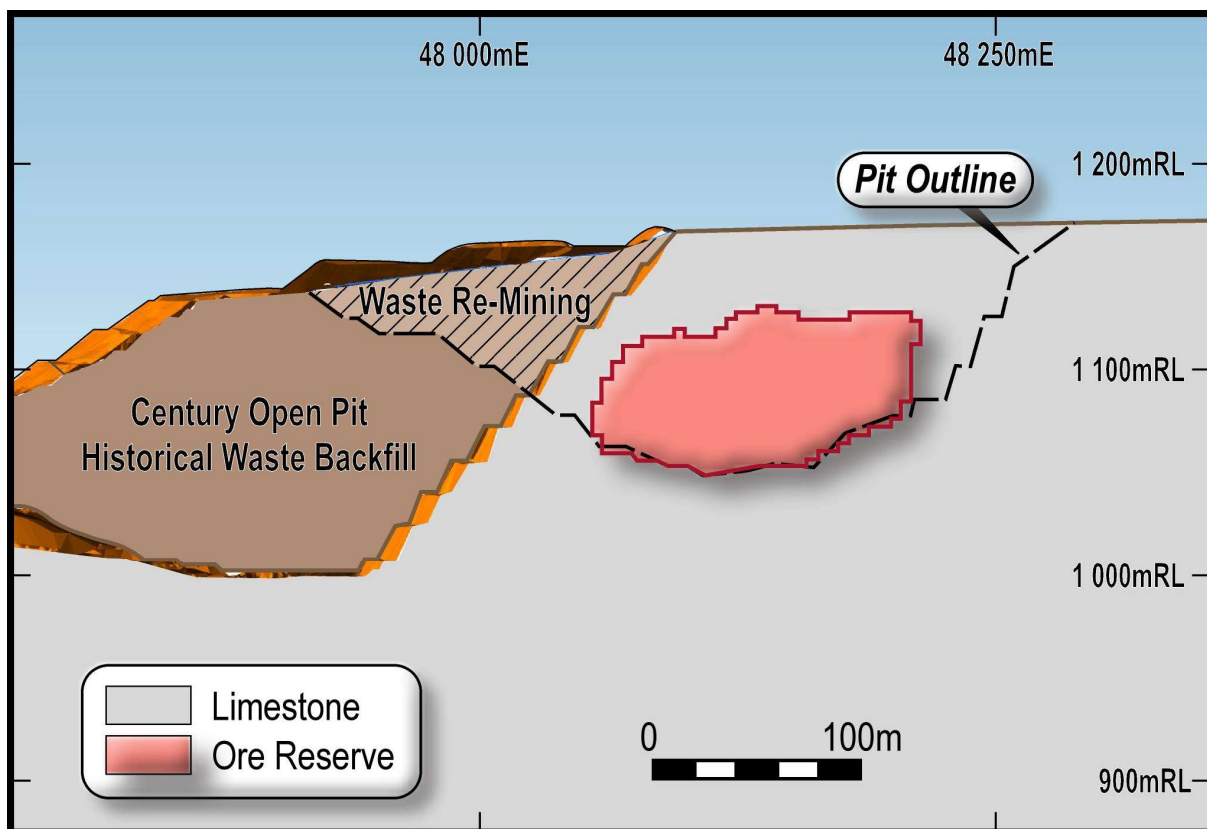


Figure 4: East Fault Block ultimate pit design

Ore Mining Profiles

The following figure shows the in-situ processing schedule by deposit and resource category (exclusive of Tailings):

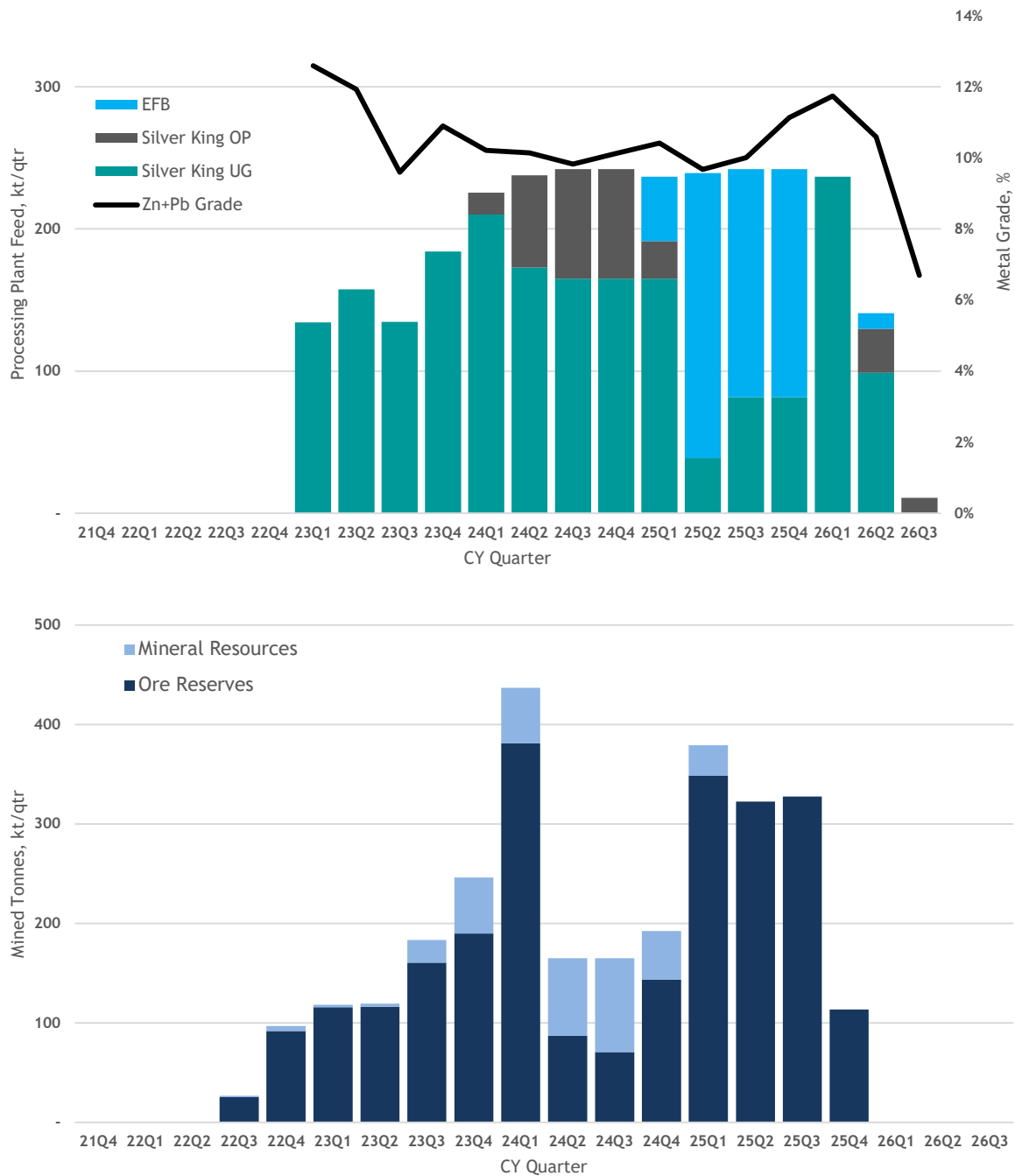


Figure 5: In-situ processed ore production profile and Zn/Pb feed grade (top) and in-situ mined production profile by resource category (bottom)

The following table provides a detailed breakdown of the mining production and grade profile for each deposit:

Table 6: Mining and metal grade profile by deposit¹

Year	Unit	LOM Total	Year 1	Year 2	Year 3	Year 4
Silver King: Underground						
Ore Throughput	Mt	2.03	0.61	0.71	0.37	0.34
Zn Head Grade	%	4.3%	4.8%	5.0%	3.0%	3.1%
Contained Zn	t	87,171	29,470	35,967	11,171	10,562
Pb Head Grade	%	7.1%	6.4%	6.1%	8.9%	8.6%
Contained Pb	t	144,578	39,198	43,628	32,752	29,000
Ag Head Grade	g/t	78	78	58	86	112
Contained Ag	koz	5,083	1,529	1,336	1,013	1,204
Silver King: Open Pit						
Ore Throughput	Mt	0.30	-	0.23	0.03	0.04
Zn Head Grade	%	2.3%	-	2.3%	2.3%	2.3%
Contained Zn	t	7,077	-	5,487	617	973
Pb Head Grade	%	4.4%	-	4.4%	4.4%	4.4%
Contained Pb	t	13,346	-	10,354	1,161	1,831
Ag Head Grade	g/t	28	-	29	28	28
Contained Ag	koz	277	-	215	24	38
East Fault Block						
Ore Throughput	Mt	0.58	-	-	0.57	0.01
Zn Head Grade	%	8.5%	-	-	8.5%	8.7%
Contained Zn	t	48,905	-	-	47,965	939
Pb Head Grade	%	0.9%	-	-	0.9%	1.0%
Contained Pb	t	5,442	-	-	5,335	107
Ag Head Grade	g/t	36	-	-	36	37
Contained Ag	koz	676	-	-	663	13

1. Throughput shown as dry metric tonnes

Processing

Metallurgical Testwork Summary

Metallurgical test work was undertaken by the previous owner of the Century Mine on the Silver King ore in conjunction with the then Century production ore in 2012. The tests showed lead and silver recovery to be proportional to their head grades, with lead concentrate grades of greater than 65% Pb and 200g/t Ag achievable with high recoveries.

Testwork carried out by the Company in 2019 (and further confirmed through the latest testwork) indicated flotation with a combination of tailings and in-situ material provided no negative impact on flotation performance. However, the Company has opted to maintain separate rougher flotation circuits for tailings and in-situ to provide greater flexibility for process optimisation of each ore type in its own circuit.

Further metallurgical testwork was carried out on Silver King and East Fault Block samples obtained from three metallurgical holes drilled during the 2021 infill drilling campaign (Silver King) and stored and refrigerated East Fault Block samples from earlier drill campaigns. The program included updated mineralogy, comminution, and flotation testwork (batch and locked cycle). Testing was carried out to determine the optimum primary grind size, reagent addition rate, requirement of pre-flotation (carbon removal) and the impact of combining in-situ flotation with tailings compared to separate processing. The testwork results were in line with historical Century operations, in both grind size, expected metal recovery and reagent consumption rate.

Testwork on the potential benefit of including ore sorting was also carried out. The outcomes of this work indicated that there was potential value available from inclusion, however it would likely be more beneficial for South Block material. It was determined not to include ore sorting in the initial flow sheet, but the contemplated design allows for inclusion at a later date if further testwork validates the business case.

Process Design

The following figure provides a high-level overview of the processing plant with the inclusion of the in-situ ore processing line:

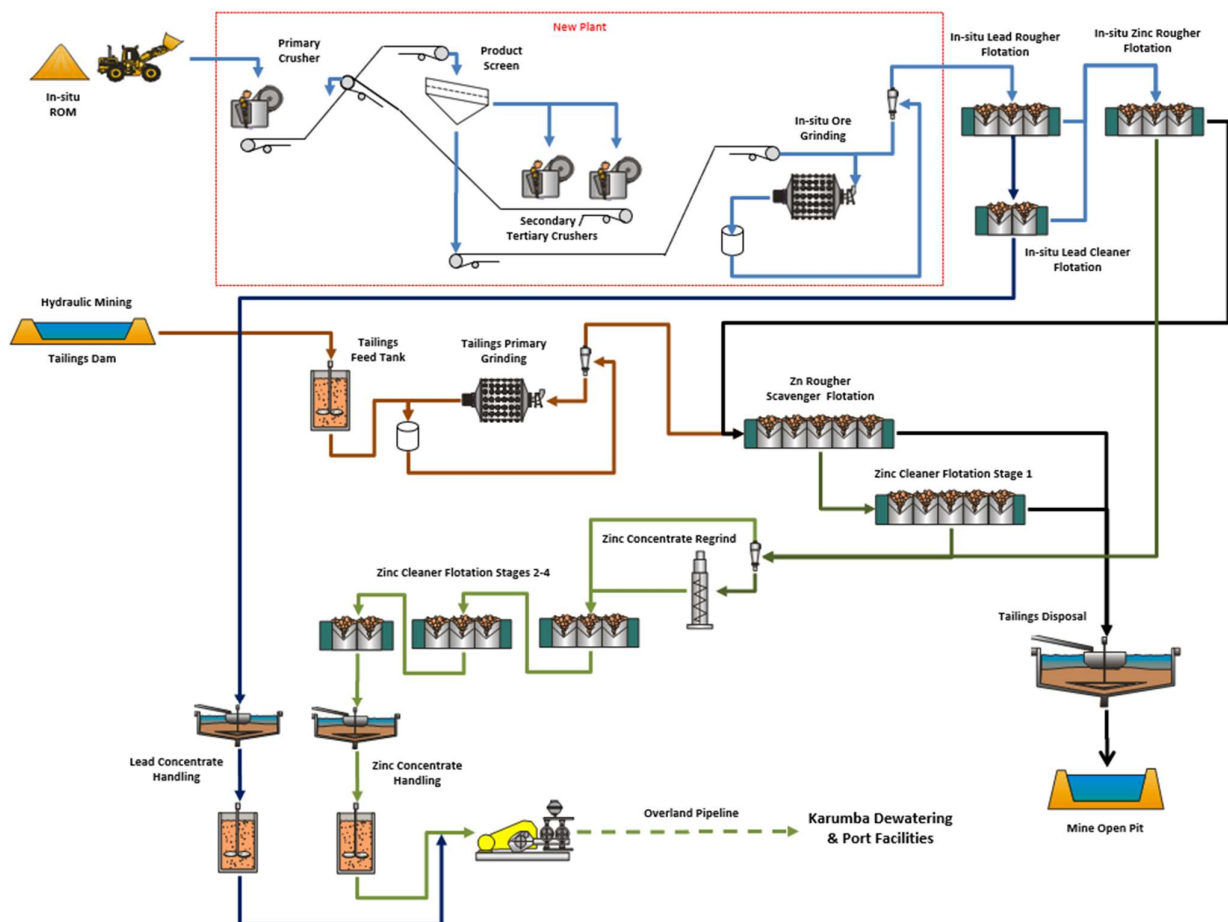


Figure 6: Processing plant flowsheet with inclusion of in-situ ore

The Company engaged GR Engineering Services Limited (**GRES**) (**ASX:GNG**) to undertake a feasibility-level design and capital cost estimate for modifications required to the existing flotation plant and processing a combination of tailings and open pit/underground ore. The aim was to optimise the flow sheet such that it could be modified to allow concurrent processing of both tailings and in-situ ore, utilising the remaining unused equipment within the processing plant (namely the lead flotation circuit and associated product handling).

The flowsheet selected has been designed to produce a saleable lead concentrate and a zinc rougher and scavenger concentrate for inclusion and further flotation upgrade in the existing zinc tailings cleaner circuit. It comprises a three stage semi mobile crushing plant (with the option for the inclusion of ore sorting), single stage ball milling, pre-carbonaceous flotation, followed by lead and zinc sequential flotation, integration of in-situ zinc Rougher/Scavenger product into the current tailings retreatment Cleaner circuit and thickening of the new high-grade lead concentrate.

Recoveries

Based on metallurgical testwork on in-situ ore, the following is a summary of the design recoveries (post ramp-up) used for the Study.

Table 7: Steady State Metal Recoveries

Item	Silver King (Underground / Open Pit)		East Fault Block	
	Study Input	Testwork	Study Input	Testwork
Zinc (into Zinc Concentrate)	70%	88-95%	70%	54-87%
Lead (into Lead Concentrate)	84%	93-94%	60%	60-88%
Silver:				
Into Zinc Concentrate	10%	5-45%	35%	45-82%
Into Lead Concentrate	70%	49-91%	35%	5-42%

A ramp-up of 18 months from first ore production to achieving name-plate production has been assumed for in-situ recoveries, resulting in a profile between the Series 1 and Series 2 McNulty curves. This selection is based on the mature level of processing, standard equipment utilised and expansion on an already operating Processing Plant (84% by Month 8, 96% by Month 12).

Metallurgical locked cycle flotation testwork has shown lead and zinc recoveries for Silver King ore up to 94.1% and 94.8% respectively. With East Fault Block showing standalone recoveries of up to 60% and 86.7% for lead and zinc respectively. However, East Fault Block ore has shown good potential for blending with Silver King feed, with blended lead recoveries achieved up to 87.7%.

Services and Infrastructure

Power

The Century Mine site is supplied electricity via the North West Power System (**NWPS**), a generation and transmission distribution network centred in the Mt Isa region of Queensland. The system services residential, industrial, and mining operations. Network supply feeds a central substation located on site, adjacent to the concentrator, from which electricity is distributed around site on a local network. In addition to the NWPS connection, Century has an existing 7MW capacity diesel

power station onsite which is used to supply power to critical functions during NWPS supply interruptions, which primarily occur during the wet season.

The inclusion of in-situ mining and processing equipment will exceed the current capacity of contracted grid power. To accommodate the increased power demand required by the site over that currently contracted, the Company will seek to source additional grid supplied power or supplement with existing on-site diesel power generation as required.

The Silver King underground mine is not planned to be connected to the site distribution grid, with local demand insufficient to warrant the capital infrastructure required to extend the site network. Local diesel generators at the Silver King mine site are planned to be installed to meet the underground mine demand.

Water

Water requirements can be adequately met with existing supply. Hydraulic mining will continue to use water sourced from the Evaporation Dam, recycled from the processing plant and the original Century pit, which is now a substantial water body.

The groundwater supply infrastructure for Century Mine comprises of the Eastern and Western Bore Fields. Water extracted from these bores has historically supplemented the process plant requirements and it is forecast that both Bore Fields and the in-pit lake have sufficient capacity to meet water demands post implementation of In-situ processing if the Evaporation Dam water is depleted.

Other Site Infrastructure

All other site infrastructure, including the airport, accommodation village, administration and project buildings, on-site laboratory, and maintenance warehouses require only minor works to meet the peak demands of in-situ mining operations. On-site manning is expected to peak at 400 personnel, with 12 additional rooms scheduled for refurbishment, taking the total available rooms to 410.

Product Logistics and Marketing

Product Pipeline, Port and Logistics

The final zinc and lead concentrates are pumped (separately in batches) to the Karumba Port facility via the 304km underground slurry pipeline. At the port, slurry is thickened and dewatered using five large filter presses. Filtered concentrate is dried and agglomerated using a rotary dryer, where it is then stacked in an 80kt undercover stockpile facility.

The concentrate is then reclaimed and sent to the transshipment vessel (**M.V. Wunma**) for transport out of the Norman River to bulk carriers in the Gulf of Carpentaria. In 2018 the Company reinstated annual dredging of the river to maintain navigability for the M.V. Wunma.

Century Mine, Pipeline and Port facilities are equipped to handle both zinc and lead concentrates (as per historical operations) and therefore do not require any modification.

Zinc and Lead Concentrate Marketing

The zinc concentrate produced by the proposed combined operations (tailings and in-situ) at Century is expected to contain on average 48% zinc and 100-160g/t silver and is proposed to be sold into existing offtake contracts.

The lead concentrate produced by the combined operations in the Study is expected to contain on average 65-70% lead and 500-600g/t silver. The Company does not yet have offtake contracts in place for a lead concentrate, however based on the projected product quality and current market demand, no issues are expected in achieving sale of 100% of production.

The payability and treatment charge (TC) terms used for the Study vary depending on the concentrate specifications and levels of by-products. The assumptions used by New Century are based on the benchmarks and actual costs from off-takers, determined by the current concentrate characteristics, and are in line with normal terms available in the market.

Zinc concentrate payability terms have been assumed as follows:

- Zinc payable: 85% or minimum deduction of 8 units
- Silver payable: deduct 3oz per tonne and pay 70% of balance

Lead concentrate payability terms have been assumed as follows:

- Lead payable: 95% or minimum deduction of 3 units
- Silver payable: deduct 1.6oz per tonne and pay 95% of balance

A US\$2/t concentrate (dry) silver refining charge has been assumed for lead concentrates, in-line with standard industry contracts.

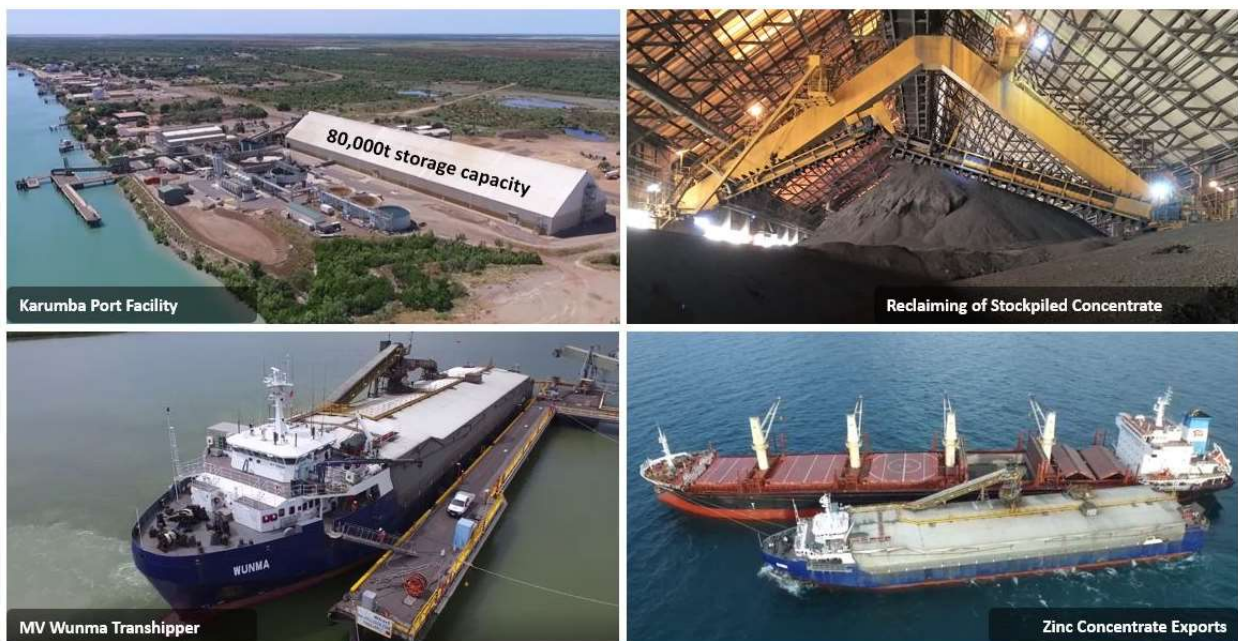


Figure 7: Existing product infrastructure at Karumba Port Facility

Project Schedule

The project schedule has been developed in conjunction with the contributing consultants for the Study, as well as the site-based owner's Projects team. The target for first ore for the in-situ operations is Q1 CY2023. The initial mine development will focus on Silver King Underground, with Silver King Open Pit and East Fault Block Open Pit commencing development in later years.

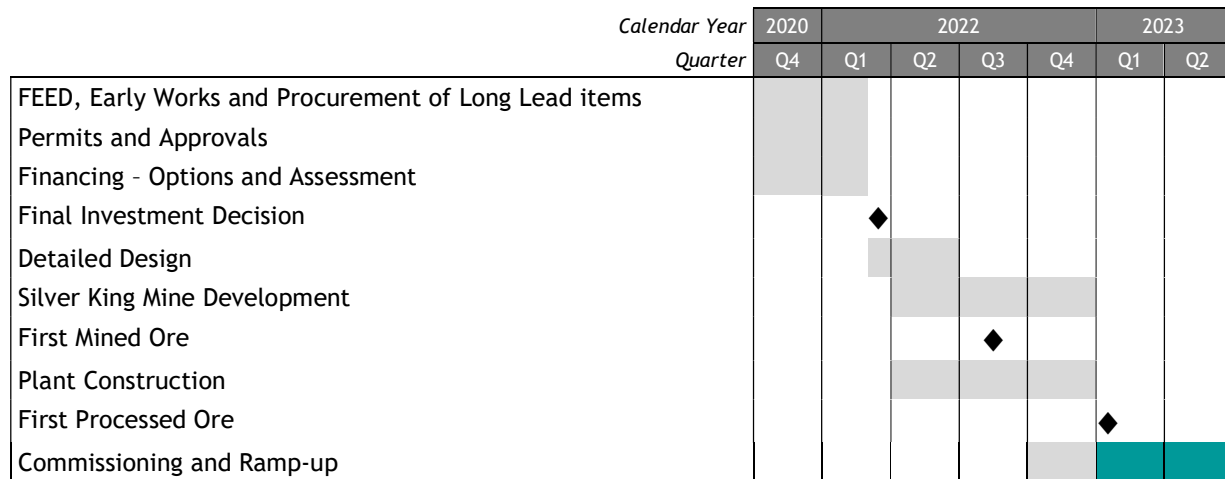


Figure 8: Proposed development schedule for in-situ ore production

The focus of the next phase will be to commence front-end engineering design (FEED) work to optimise the processing plant construction and refurbishment, mining schedules and additional operational readiness activities to allow development of an executable plan to gain a final investment decision. Several options to reduce capital will be investigated during the early works program, including the overall contracting strategy, sale and lease back (of New Century's existing mining equipment) and Build, own and operate (BOO) / Build, own, operate and transfer (BOOT) arrangements for front-end crush/grinding equipment.

Securing all required permits and approvals is estimated to take three to six months, with this process already well progressed. The critical path includes sourcing of the ball mill, with it being scheduled to be ordered by the end of CY2021. A final investment decision and updated execution schedule is expected in Q1 CY2022, allowing a progression to first processed ore in Q1 CY2023.

Production Profile

The following is a production schedule for the in-situ operations:

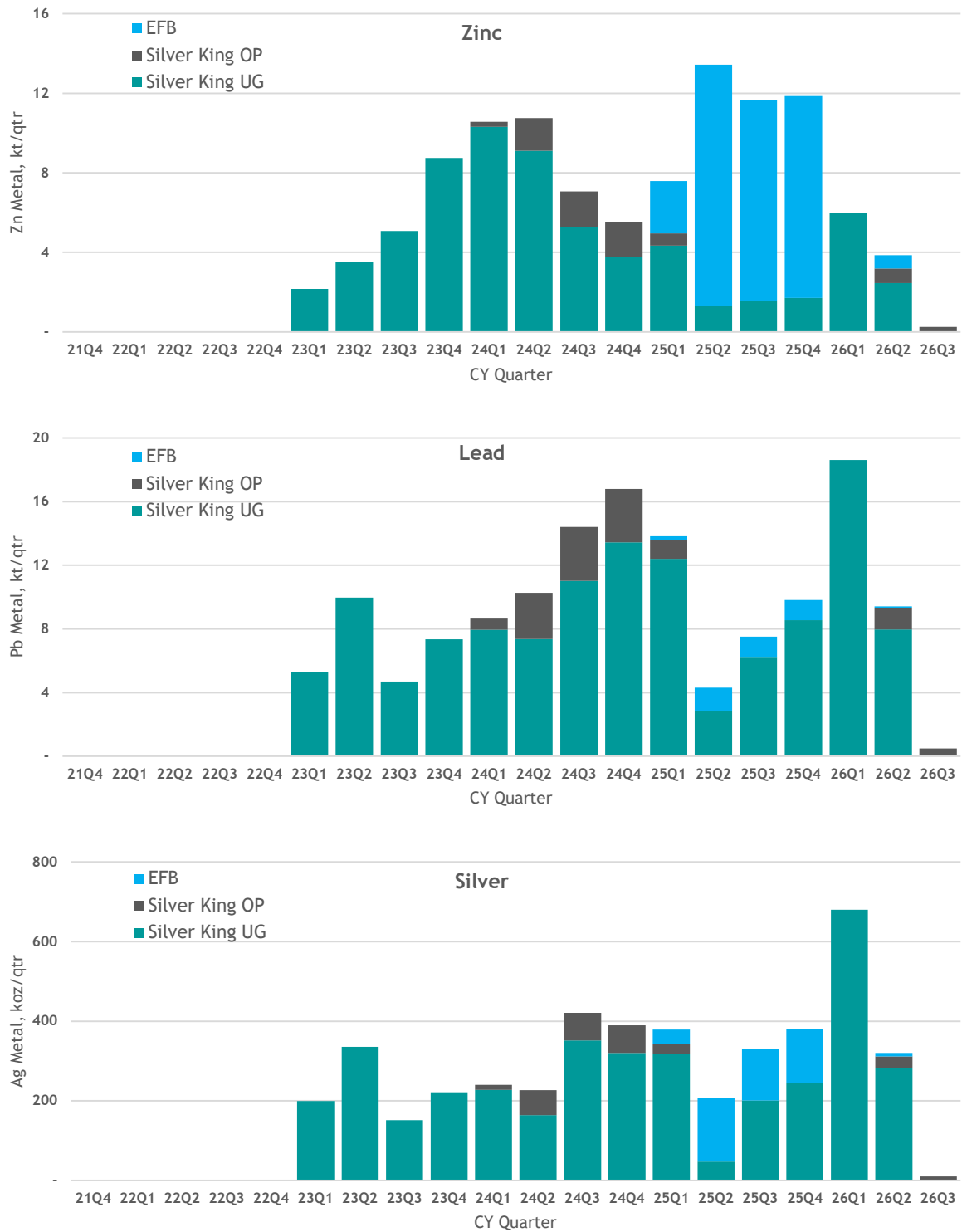


Figure 9: Estimated zinc, lead and silver quarterly production profiles

Capital Cost

Upfront Capital Costs

The following table provides the capital cost breakdown for in-situ development.

Table 8: In-situ Initial Capital Cost Estimate

Item	AUDm
Mine Establishment	13.9
Process Plant, Pipeline & Port	40.6
Site Infrastructure	3.9
Owner's Cost	5.4
Contingency	2.8
Pre-Production Capital Cost to first Mined Ore	66.7
Estimated Working Capital (to first concentrate production)	16.8
Maximum Cash Draw	83.5

Mine establishment costs are for Silver King underground, which include all capital items, development, site establishment and mobilisation. The cost base was developed from first principles by the New Century mine technical services team, using contractor estimates or quotations on most items. Benchmarking against similar Queensland operations has shown that costs align well with comparable operations and include appropriate allowances.

The pre-strip and development costs for Silver King Open Pit and East Fault Block occur later in operations and are accounted for in Operating Cost, apart for some minor establishment costs which are allowed for in Sustaining Capital.

GRES provided a Class 3 (AACE) estimate for the processing plant, which included the refurbishment of existing equipment, as well as the installation of new equipment (mainly crushers, ball mill /sizing circuit, conveyors and conditioning tanks for the lead flotation circuit). A detailed contingency analysis was completed based on the source and quality of the input costs base across all direct and indirect cost estimates. The analysis resulted in an overall contingency of 8.3% (on total of direct and indirect costs) which is included.

Site infrastructure costs, including power, water, camp and related services have been developed based on Century's current operating cost basis.

The base case overall Study estimate is to a $\pm 15\%$ level of accuracy and based on Q3 CY2021 Australian dollars. Future changes to exchange rate or escalation have been excluded.

Estimated working capital allowance includes development and production from Silver King to provide an initial ROM stockpile of 50kt of ore to have available for production. Under the base case metal price assumptions, the ROM at plant start-up would include ore with a contained metal value of A\$25 million⁷. Further mine plan work will be carried out in the next phase to optimise initial ore production in line with processing plant ramp-up to minimise working capital requirements for the Project.

⁷ 50.1kt of ore at 3.3% Zn, 10.6% Pb, 150g/t Ag, assumed payability of 85% Zn, 95% Pb and avg Ag payability of 50%, base case metal prices and exchange rate as summarised in Table 2

Sustaining Capital

Sustaining capital for ongoing underground development work (A\$11.6m), as well as site establishment and mobilisation for open pit operations (A\$2.3m) has been allowed for in the Project estimate. Estimated closure costs for Silver King of A\$0.4m have also been included.

Table 9: In-situ Total LOM Capital Cost Estimate

Item	AUDm
Pre-Production Capital	66.7
Sustaining & Closure Costs	14.3
Total In-situ LOM Capital Costs	81.0

The overburden of East Fault Block is planned to be used for rehabilitation and capping requirements for the existing waste rock dumps on site. Therefore, inclusion of East Fault Block development will reduce the overall site closure cost, and the availability of operational surface mining equipment will allow for additional rehabilitation to be carried out with spare capacity. This has not been accounted for in the Study but will have its value contribution defined in the next stage.

Operating Cost

Operating costs have been estimated based on quantities established from actual operating costs for the Project, estimates from suppliers and contractors (where applicable) and current market rates. Details of each cost centre can be found in the sections below.

Table 10: In-situ Total LOM Operating Cost Estimate

Item	Silver King Underground		Silver King Open Pit		East Fault Block		Total In-situ	
	A\$/t ore ¹	US\$/lb Zn ²	A\$/t ore ¹	US\$/lb Zn ²	A\$/t ore ¹	US\$/lb Zn ²	A\$/t ore ¹	US\$/lb Zn ²
Mining	51.5	0.70	30.4	0.55	49.7	0.32	49.0	0.55
Processing	27.9	0.38	27.1	0.49	24.5	0.16	27.1	0.31
Site G&A	12.8	0.17	10.6	0.19	10.1	0.07	12.0	0.14
Transport	11.3	0.15	8.3	0.15	10.6	0.07	10.8	0.12
Treatment Charges ³	34.2	0.46	25.0	0.45	30.7	0.20	32.5	0.37
C1 Cost (excl Pb & Ag Credits)¹	137.7	1.86	101.5	1.84	125.7	0.81	131.5	1.49
Lead Credit	-	-2.26	-	-2.21	-	-0.11	-	-1.50
Silver Credit	-	-0.71	-	-0.45	-	-0.09	-	-0.48
C1 Cost (incl. Pb & Ag Credits)⁴	-	-1.11	-	-0.81	-	0.61	-	-0.49
Royalties	19.0	0.26	11.8	0.21	10.8	0.07	16.6	0.19
Corporate Costs	0.6	0.01	0.4	0.01	0.4	0.00	0.6	0.01
Sustaining Capex	5.7	0.08	3.8	0.07	2.0	0.01	4.8	0.05
All-in Sustaining Cost (AISC)	163.0	-0.77	117.4	-0.52	138.8	0.69	153.4	-0.24

1. Excluding all metal credits

2. Based on payable zinc metal production from in-situ mined ore only, excludes tailings

3. Zinc concentrate and lead concentrate treatment charges

4. C1 is defined as direct cash operating costs produced, net of by-product credits, divided by the amount of payable zinc produced. Direct cash operating costs include all mining, processing, transport, treatment costs and smelter recovery deductions through to refined metal

Due to both the significant by-product credits and tailings covering most of the fixed cost-base, in-situ operations are forecast to have negative C1 costs at the assumed base case pricing. With in-situ operation included in the overall operation cost (i.e. tailings and in-situ), the life of mine average C1 cost and AISC (both on a payable zinc basis) are estimated drop by US\$0.21/lb US\$0.17/lb respectively.

The following is an overview of the operating cost profile for in-situ operations. As tailings operations include most of the fixed costs for the Project, processing, port and site G&A costs are greatly reduced for in-situ and are mainly the variable costs for in-situ operation.

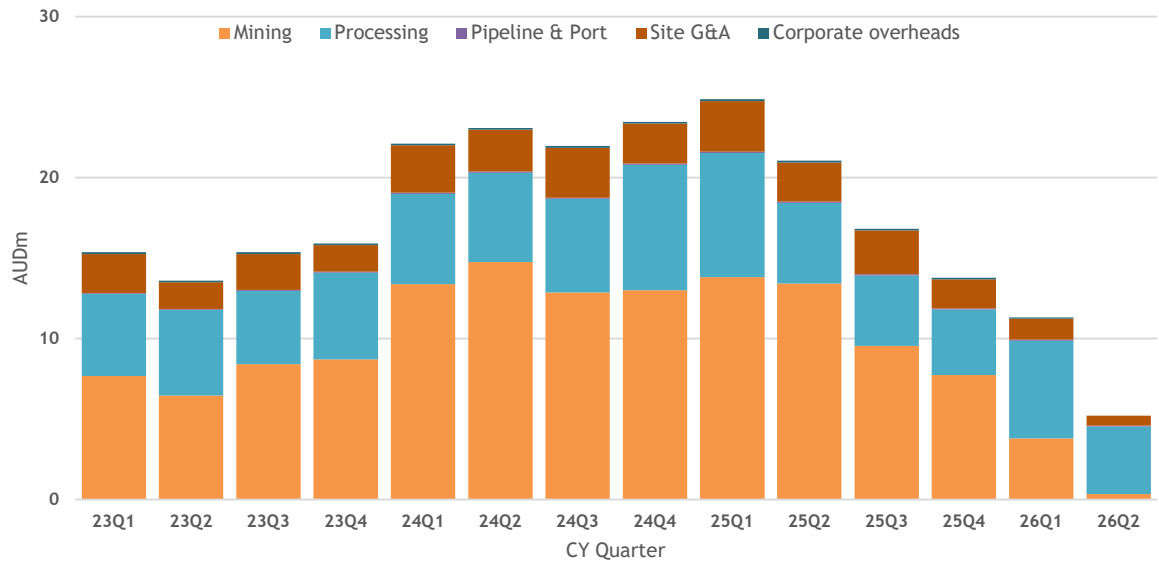


Figure 10: Quarterly site operating cost profile for In-situ (excludes tailings operating costs)

Mining Cost

Mining represents the largest cost centre for in-situ, representing on average 37%, 30% and 40% of C1 costs (excluding credits) for Silver King Underground, Silver King Open Pit and East Fault Block respectively. The life of mine breakdown of costs for each operation is found below:

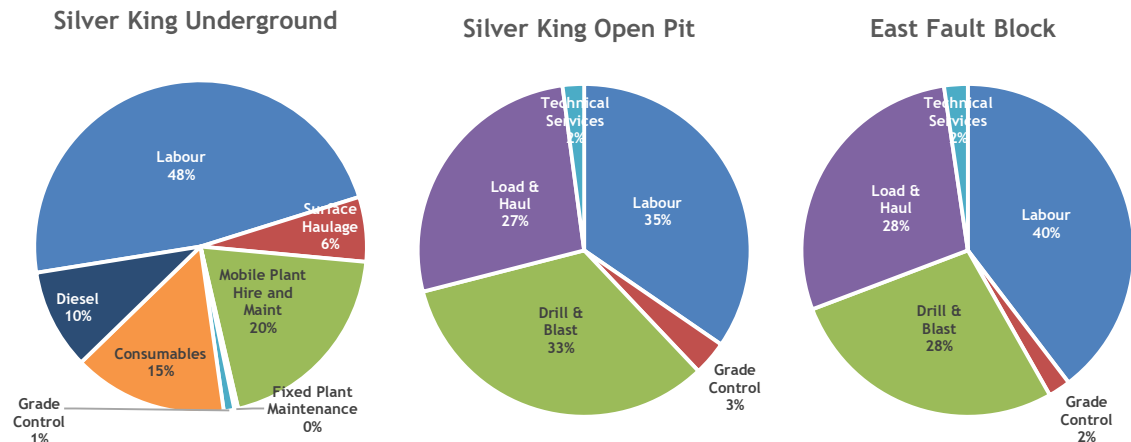


Figure 11: LOM breakdown of mining costs for each deposit

Processing Cost

Processing costs are predominantly made up of electricity, reagents and consumables, averaging a combined 64% for in-situ ore processing. The operating cost estimate above has been developed on the actual current operation costs for tailings. The costs have been separated into fixed and variable portions, with the variable portion adjusted for the production in that period.

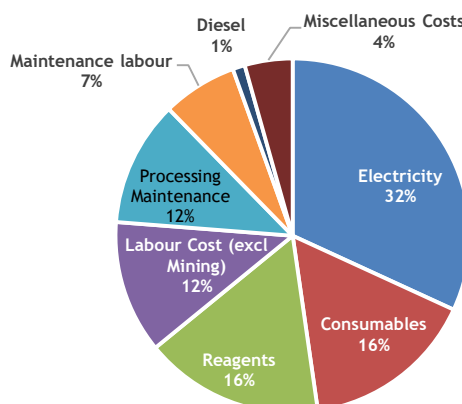


Figure 12: LOM breakdown of mining costs for in-situ operation

Product Logistics, Marketing and Sale Costs

The incorporation of lead concentrates into the existing Pipeline, Port and transshipping operation is not expected to materially change the operational strategy or cost base of the assets (approximately US\$0.01-0.02/lb Zn payable). The operations previously transported lead concentrates through the existing logistics chain, providing extensive operational data, processes, and procedures to use.

The Study incorporates the operation of the M.V. Wunma in 5,000t parcels to concentrate ships in the Gulf of Carpentaria. The life of mine average operating cost for the transshipment vessel is A\$0.60/wet metric tonne of concentrate. This includes the consumable costs only, as all labour, maintenance, consumables, and G&A costs are included in the existing tailings operation.

The life of mine average overseas shipment cost for the Study is US\$50/wmt.

Treatment Charges

The Study incorporates assumptions for life of mine treatment charges, based on recent market information, annual benchmark increases and general market sentiment. The Study has adopted a life of mine average of USD\$155/t zinc concentrate and USD\$175/t lead concentrate, both in line with historical averages.

Corporate Costs

Life of mine average corporate costs of A\$0.60/t feed have been taken into consideration and include all additional incremental corporate overheads associated with the proposed operations,

licenses, permits and mining lease payments as well as all cultural and stakeholder engagement commitments as outlined in the Gulf Communities Agreement.

Royalties

Queensland levies mineral royalties for extractive operations within the state. All royalties are based on an 'ad valorem' value of minerals. Zinc and silver royalties are determined by a variable rate between 2.50% and 5.00% of value, depending on average metal prices. The Queensland Government royalties are applied to all commodities produced and sold in accordance with published rates and guidelines. In addition to government royalties, the existing 2% NSR over the Century tenements has also been included.

In-Situ Development Funding

Following completion of the Study, New Century is now undertaking activities to obtain its required final environmental amendment and also a process of assessment of development financing or joint venture options. These activities are well underway. The Company has several options available for funding development of all or part of the in-situ operations, including utilisation of cash flow from tailings operations, project financing, joint ventures, offtake financing, contractor financing and via the equity markets.

The Company intends on developing an optimal financing or joint venture structure for in-situ development over the next 3 to 6 months, with the preferred option to be selected by Final Investment Decision, which is targeted in Q1 CY2022.

Financial Results

The economics of in-situ operations have been assessed using the discounted cash flow method, based on a monthly schedule of tonnes mined and processed from and in-situ ore.

Capital and operating costs are applied to mining, processing, product transportation and overheads.

Shipping and logistics, product payability, treatment and refining costs, state and other royalties are included to calculate the NPV for the Project.

A discount rate of 8% has been applied to real term cash flows to calculate the pre-tax NPV. No inflation has been applied.

Unless otherwise stated, all cash flows are in Australian dollars.

The following is a summary of key financial metrics for the Project:

Table 11: Expansion In-Situ Feasibility Study Life of Mine Summary - Financials (Base and Spot)

Item	Units	Total In-situ (Base Case)	Total In-situ (Current Spot)
Economic Assumptions¹			
Zinc Price	US\$/t	2,535	3,030
Lead Price	US\$/t	2,205	2,290
Silver Price	US\$/oz	25	23.9
Exchange Rate	US\$:A\$	0.70	0.736
Project Cash Flow			
Net Smelter Revenue	A\$m	709.3	738.5
EBITDA	A\$m	384.4	412.0
Maximum Cash Draw (including working capital) ²	A\$m	83.5	83.4
Sustaining Costs & Rehabilitation	A\$m	14.3	14.3
Net Project Cash Flow (pre-tax)	A\$m	286.7	314.3
Financial Metrics			
Pre-tax NPV₈	A\$m	212.0	233.9
Pre-tax IRR	%	102%	111%
Pre-tax Payback Period	Yrs	2.2	2.0
NPV/Capex	-	3.8	4.1

1. Commodity price and metal exchange rate assumed to be flat over life of mine for Base Case

2. Represents all capital requirements including appropriate contingency and working capital allowances for in-situ development. Costs for plant, site services, etc are distributed between the three deposits based on LOM throughput

The figures below outline the quarterly cash flows and the cash flow per deposit for the in-situ operations.

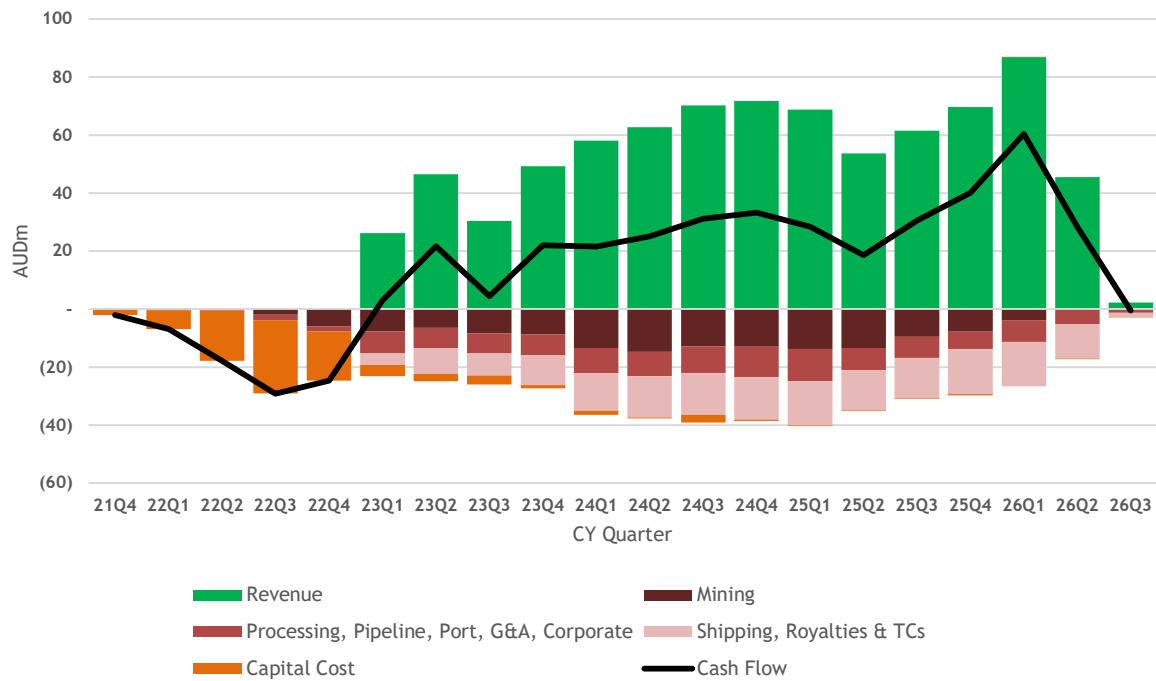


Figure 13: In-situ cash flow profile and pre-tax cash flow

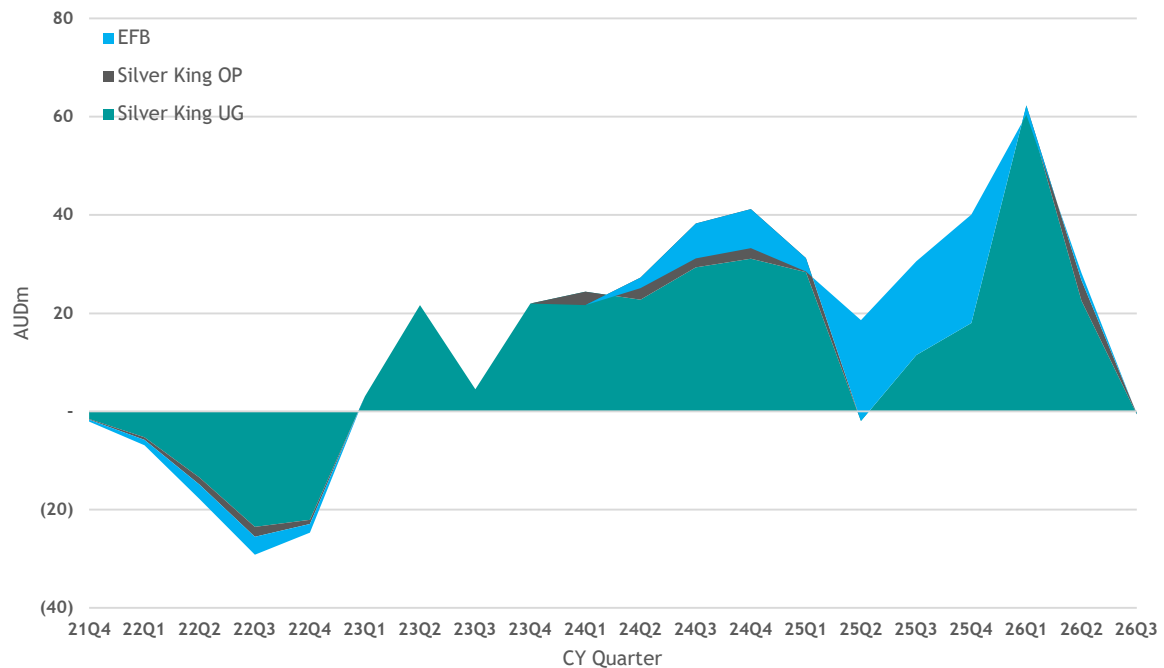


Figure 14: In-situ cash flow profile by deposit

Sensitivity Analysis

For each deposit, the sensitivity of the project NPV to key input changes is summarised in the table below. The base case NPV for each deposit is A\$174m (Silver King Underground), A\$17m (Silver King Open Pit) and A\$21m (East Fault Block).

The economics of the Silver King deposits are more sensitive to the lead price, compared to East Fault Block, which has a higher zinc grade. All deposits demonstrate positive economics in downside macro scenarios, providing a strong basis for the business in times when metal prices are depressed.

Whilst the majority of C1 costs are site-controlled, treatment charges, which typically represent 25% of the C1 cost (excluding credits), represents the largest uncontrollable cost item for the project. However, as the analysis below demonstrates, even assuming historically high treatment charges will still provide highly profitable returns.

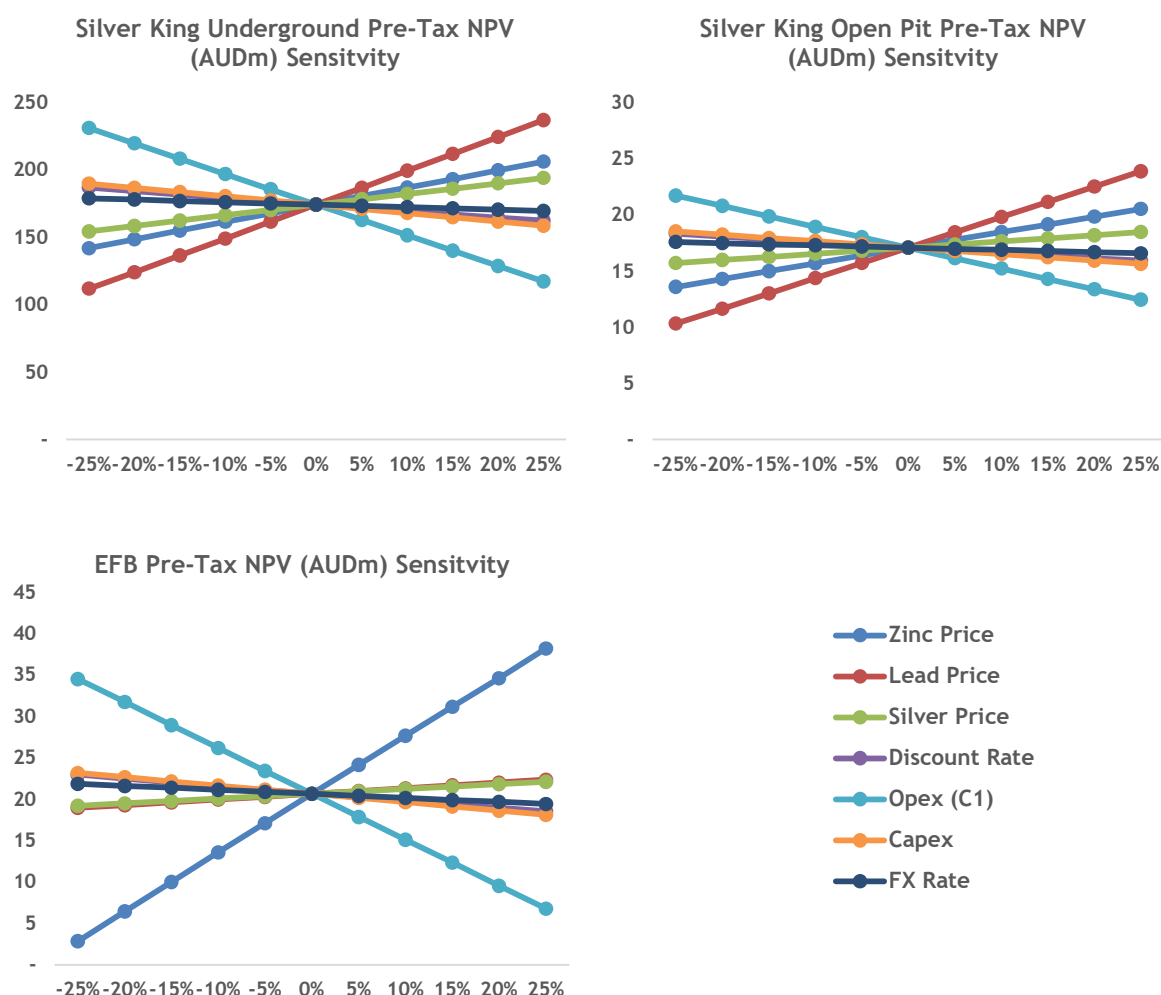


Figure 15: Sensitivity analysis for each in-situ deposit

Environment, Approvals and Stakeholders

Environment

The proposed development of East Fault Block and Silver King lie within currently disturbed areas on the existing Mining Lease and Environmental Authority at Century. Development of the deposits is expected to require an amendment to the existing Environmental Authority with pre-lodgement activities with the Department of Environment and Science underway. The amendment application is expected to be submitted in October 2021, with the process expected to take up to 6 months.

Regulatory Approvals and Licenses

Century Mining Limited (CML), which is 100% owned by New Century, holds all the relevant mining and exploration leases for the cases considered in the Study.

Native Title and Cultural Heritage

The Century Mining Leases were granted following a right to negotiate process in accordance with the *Native Title Act 1993* (Cth) (NTA). Further, any Native Title rights and interests in the Term Lease underlying the Century Mining Leases were acquired by the State of Queensland following a process in accordance with the NTA.

The consent from the relevant Native Title holders for the grant of the Century Mining Leases (and other grants) is contained in the Gulf Communities Agreement (GCA), which has no termination date other than the date upon which the Century Mining Leases are relinquished.

Any Native Title rights and interests in relation to the pipeline corridor were acquired by the State of Queensland following a process in accordance with the NTA. Further, the pipeline operational licence was granted following a process in accordance with the NTA. The consent from the relevant Native Title holders for the grant of the pipeline operational Licence (and other grants) is contained in the GCA. Any Native Title rights and interests in relation to the Karumba Port Facility were acquired by the State of Queensland following a process in accordance with the NTA.

Local Community

The impact area of the proposed operations encompasses the Lower Gulf Region of north-west Queensland, inclusive of the area immediately surrounding the Century Mine at Lawn Hill and Karumba, and the communities of Gregory, Doomadgee, Burketown, Normanton and Mornington Island. These non-contiguous areas are contained within the local government areas of Burke Shire, Carpentaria Shire, Doomadgee Aboriginal Shire, and Mornington Shire.

The reinvigoration of economic activity at the Century Mine by New Century has significantly re-energised communities through partial, and in some cases complete renewal of many of the past benefits identified through the Mine's previous operational life. New Century maintains regular engagement with the Queensland Government and with the local governments that have an interest in the Century Mine's operations, including the potential expansion activities described in this Study. Development of East Fault Block will include a partnership with the Waanyi People through their commercial Joint Venture⁸ and our operational readiness processes will include engagement with the Joint Venture to refine a service delivery profile.

⁸ See ASX Announcement dated 29 May 2018 for further details Waanyi Downer Joint Venture

Resource Upgrade and Further Exploration Drilling

The Company has recently completed⁹ four reverse circulation drill holes within historical IP targets located to the southwest of the original Silver King workings. All four holes targeted the down dip extent of mineralisation historically mined at surface.

Additionally, following a review of historical IP targets around the Silver King deposit, exploration drilling has confirmed the occurrence of prospective mineralisation within the previously untested Vein No.4, 200m north-west of the main lode.

New Century has taken the strategic decision to expand its exploration activities on its tenements surrounding the Century operations. Further exploration at Silver King and Watson's Lode will now be accelerated. The Company has secured the ongoing use of both IP equipment and an exploration drilling rig, with drilling set to begin in late September 2021.

The next programs at Silver King and Watson's Lode will involve:

- expanded 3D-IP geophysical survey over selected areas near each deposit;
- at **Silver King**, a further ~5,000m of exploration drilling to better define newly identified shallow mineralisation and potential expansion of the No.4 Vein along strike (all of which is outside the Mineral Resource completed in the Study); and
- at **Watson's Lode**, a further ~4,000m of exploration drilling program to expand the new resource along strike, in addition to testing IP chargeability anomalies near the deposit.

⁹ See ASX Announcement dated 02 September 2021 for further details on the Silver King drilling and proposed exploration program

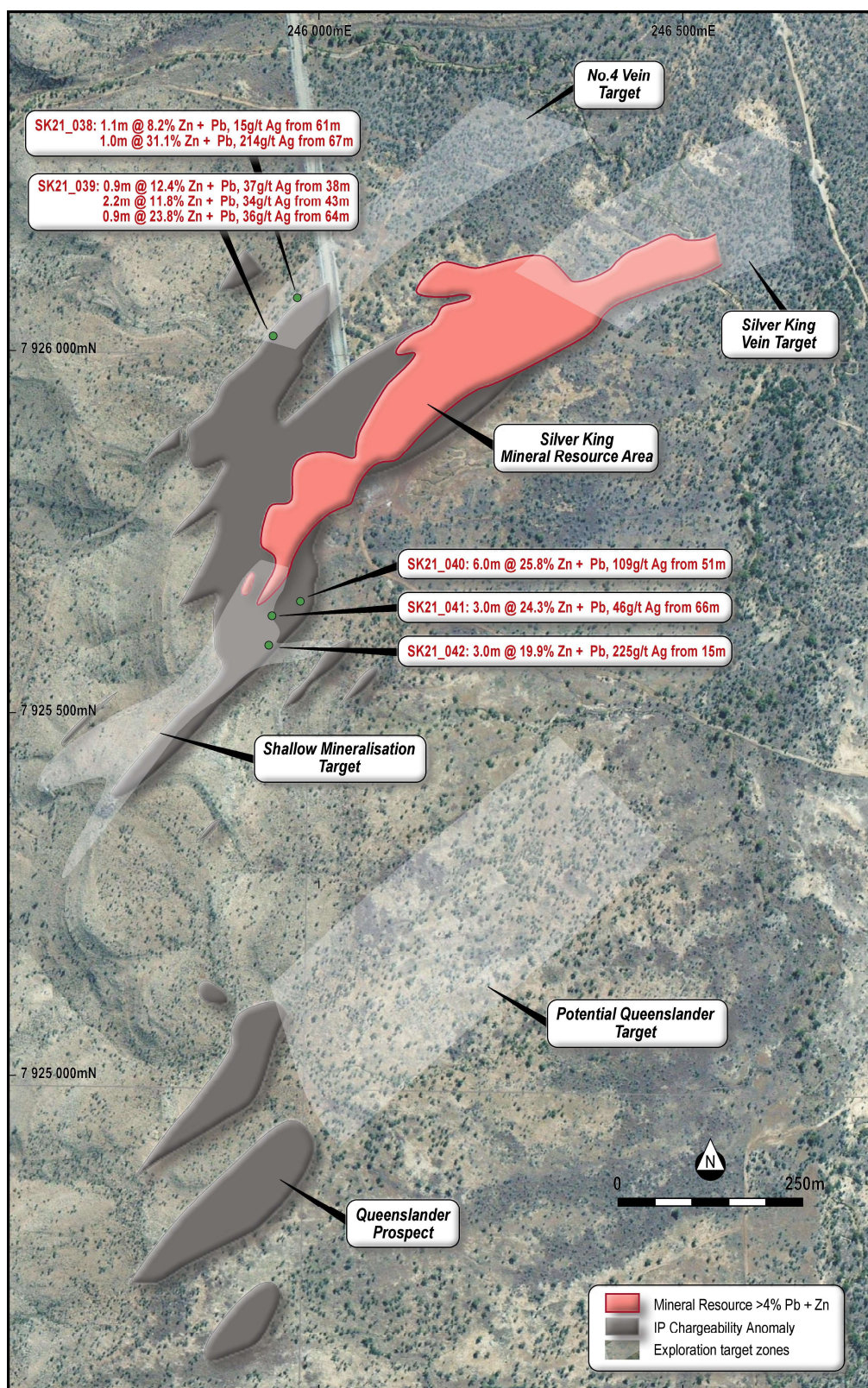


Figure 16: Location of newly identified shallow mineralisation surrounding Silver King overlaid with 10ms (10 mV/V) IP-chargeability shell for future drill targeting

Expansion Potential: South Block, Watson's Lode and Silver King

A Prefeasibility Study was carried out in 2019¹⁰ for the inclusion of South Block (as well as East Fault Block and Silver King) into the overall operations. The Study highlighted the potential to improve the economics of mining South Block through optimisation of the mining method to reduce the overall strip ratio.

A significant amount of past exploration at Watson's Lode including over 20,000m of drilling, multiple IP surveys and geochemical soil sampling has been reported. These results, in conjunction with full collation and review of historic IP data over the prospect have supported the estimation of a maiden Inferred Mineral Resource.

The combination of South Block and Watson's Lode has the potential to add 7.9Mt of Mineral Resources, containing 469kt of zinc, 128kt of lead and 9.2MOz of silver to the life of mine plan. These resources, combined with the inclusion of the remaining unconverted Silver King resource, provide the potential to extend mine life beyond the existing tailings only operations at Century.

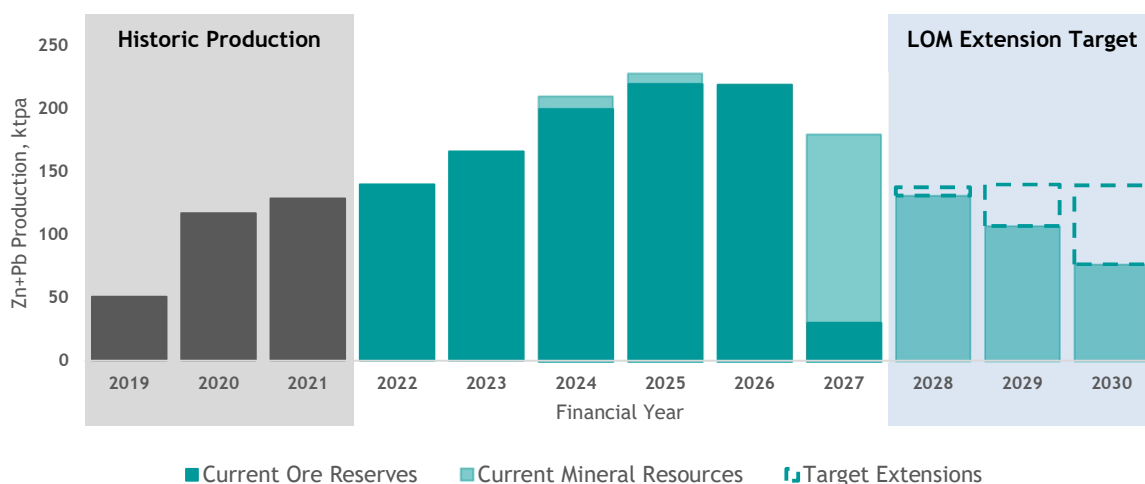


Figure 17: Mined ore production profile showing potential mine life extension with the inclusion of Silver King Resource, South Block and Watson's Lode and a target extension to current resources

A scoping level study is planned for H1 CY2022 to determine the most economic mining method of South Block for inclusion in the life of mine plan. Further resource drilling is planned for Watson's Lode to increase the confidence in the deposit and form the basis of a scoping study over that resource. These studies will provide estimates for the likely timing and method to develop these resources.

Listing Rule 5.8.1 Information

Silver King is a vein-style system, consisting of predominately epithermal quartz carbonate breccias with varying contents of sphalerite, galena, chalcopyrite, pyrite and siderite. The mineralisation is focused on a dilational jog structure within a north-eastern trending fault.

¹⁰ See ASX Announcement dated 25 June 2019 for further details on the Expansion Prefeasibility Study results

Approximately 95% of the drilled intersections and samples are diamond drill core, with the remaining samples from Reverse Circulation (RC) chips. Half core samples were taken from diamond drill core for analysis, whilst the sampling method for the RC chips is via a rotary cone splitter with an 80 / 10 / 10 split. RAB, Percussion, Geotechnical and bulk sampled Metallurgical holes were excluded from the estimation.

For the most recent drilling half core samples were crushed, pulverised and a split taken for assay. Samples were analysed for a range of elements using ME-XRF15c, ME-OG46 (inductively coupled plasma-atomic emission spectrometry techniques) for Silver with Leco for carbons and sulphurs. These are industry standard and appropriate. Certified reference materials (standards and blanks) were inserted into the sample stream.

The estimate was completed using the kriging method within 5m x 10m x 2.5m blocks. The estimate was reported to a 4% Zn+Pb cut-off grade, a level which has reasonable expectation for economic extraction.

The classification of the Mineral Resource is based on drill spacing and estimation quality (kriging efficiency), the drill spacing of approximately 10m x 10m for Measured, 20m x 20m for Indicated and 40m x 40m for Inferred. Additional drilling will be required to increase confidence in the Mineral Resource classification down plunge, however this is proposed to be conducted from underground platforms during mining operations.

Mining and metallurgical assumptions are based on the results of work conducted during the Study.

This announcement is approved for release by the Board of New Century Resources.

For further information, please contact:

New Century Resources

Patrick Walta

Managing Director

P: +61 3 9070 3300

E: info@newcenturyresources.com

Media enquiries

Shane Goodwin

Head of Corporate Affairs

P: +61 434 039 106

E: sgoodwin@newcenturyresources.com

Appendix 1: Competent Persons Statements

Competent Persons Statement - Reserves

The information relating to the Estimation and Reporting of Ore Reserves at the Century Tailings Deposit, Silver King Deposit and East Fault Block Deposit is based on information compiled by Timothy Edwards, a Competent Person who is a member of the Australasian Institute of Mining and Metallurgy. Timothy Edwards is a full-time employee of the Company. Timothy Edwards has sufficient experience which is relevant to the style of mineralization and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian code for Reporting Exploration Results, Mineral Resources and Ore Reserves' (**JORC Code**). . Timothy Edwards consents to the inclusion in this announcement of the matters based on his information in the form and context which it appears.

Competent Person's Statement - Resources

The information in this report that relates to Exploration Results and Mineral Resources is based on information compiled by Nick Spanswick, a Competent Person who is a member of the Australian Institute of Geoscientists. Nick Spanswick is a full-time employee of the Company. Nick Spanswick has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken, to qualify as a Competent Person as defined in the JORC Code. Nick Spanswick consents to the inclusion in this announcement of the matters based on his information in the form and context in which it appears.

Appendix 2: JORC Code (2012 Edition): Table 1

Silver King (Underground and Open Pit) Resource Estimation

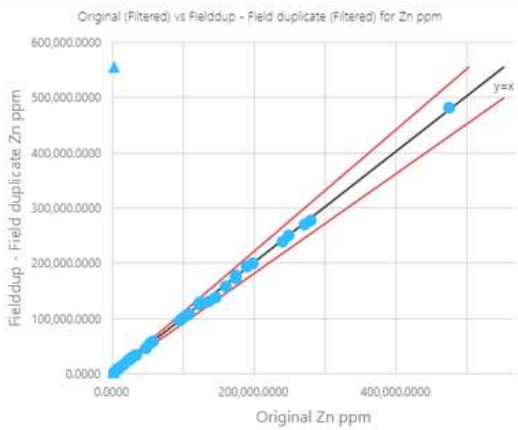
Section 1: Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information. 	<ul style="list-style-type: none"> All sampling used in the 2021 Silver King Mineral Resource estimate was carried out by drilling methods both RC and diamond drilling. Sample lengths range from 0.25m to 1.5m for diamond core samples and were a nominal 1m length for RC samples. Sampling of RC chips involved splitting using an 80/10/10 cone splitter at the rig, resulting in 10% sample recovery to the primary split. This approximated a mass of 5kg per metre sampled being submitted to the laboratory for sample preparation. The Competent Person considers the sampling to be of high quality. Measures taken to ensure sample representivity include - orientation of the drill holes as close as practical to perpendicular to the known mineralised structure, and collection, and analysis of field duplicates.
Drilling techniques	<ul style="list-style-type: none"> Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc). 	<ul style="list-style-type: none"> Reverse circulation drilling was carried out using a truck mounted UDR- 1000 drill rig equipped with automatic rod-handler. A combined, detachable cyclone and dust unit and an auxiliary compressor, was utilised. All holes were drilled using a 5 1/4 inch hammer. Diamond drilling was carried out at NQ3, HQ3, and PQ3 diameters. All drilling was carried out using triple tube barrels to maximise core recovery in poor ground. Core diameters were as follows - <ul style="list-style-type: none"> NQ3 45mm HQ3 61.1mm PQ3 83mm Core orientation was achieved using a single shot down-hole survey tool, which records - azimuth, inclination, magnetic tool face angle, gravity roll angle, magnetic field strength and temperature. From this data the bottom of hole, or BOH, is marked and an orientation line projected along the length of succeeding coherent core. This may be used for orientating geological structures during the logging process.
Drill sample recovery	<ul style="list-style-type: none"> Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the 	<ul style="list-style-type: none"> Core recovery was recorded at the drill rig by the driller's assistant, with core blocks denoting drilled metres and recovered metres in between sample runs. All values were checked at the core yard by experienced field assistants, prior to detailed logging by Geologists. The accepted length of recovered core between drilling intervals was recorded

Criteria	JORC Code explanation	Commentary
	<p>samples.</p> <ul style="list-style-type: none"> Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material. 	<p>in the detailed logging sheets. These were later loaded into the Datashed5 database.</p> <ul style="list-style-type: none"> For RC drilling, field logging sheets were used to note any small samples encountered. No significant issues were encountered with regards to sample recovery during the 17-hole RC campaign in 2013. No sample weights were recorded. RC Drilling data from 2021 was not available (or used) at time of writing. <u>Diamond Drilling:</u> <ul style="list-style-type: none"> All diamond drilling was carried out using triple tube barrels to maximise core recovery in broken ground. Diamond core that is orientated is routinely cut along a line 1cm to the right of the BOH orientation line (looking down-hole) to limit the potential for sampling bias by the sampler. Diamond core sample sizes were as follows - <ul style="list-style-type: none"> HQ Diamond drill whole core (~8kg) HQ Diamond drill half core (~4kg) NQ Diamond drill half core (~2kg) The variance in sub-sample size was not considered a risk to the overall comparability and representativeness of the samples. <u>Reverse Circulation Drilling</u> <ul style="list-style-type: none"> Reverse Circulation drilling used an 80/10/10 cone splitter, resulting in 10% sample recovery to the primary split, this approximated a mass of 5kg per metre sampled. Fines loss to air was monitored to ensure no significant loss was occurring leading to size fraction bias. Bags were not weighed and recovery / sample size was never an issue. The cone splitter was checked to be level, and in good order, to ensure effective non-bias sampling. The splitter cone was also routinely cleaned to minimize potential cross-sample contamination through material 'hang-up'. No definitive relationship has been defined between recovery and grade that have been considered in the estimation of the Mineral Resource. Targeted Geotechnical and Metallurgical holes were drilled in 2021 to improve the understanding in these areas. No issues material to the classification of the Resource have been identified. See Metallurgical Testing Report 2021.
Logging	<ul style="list-style-type: none"> Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. The total length and percentage of the relevant intersections logged. 	<ul style="list-style-type: none"> Detailed geological logging has been carried out on all Diamond drill holes, the data collected includes - Recovery, RQD, BPM, stratigraphy, lithology, structure, colour, weathering, mineral proportion estimate and sample intervals. Geological core logging was carried out in a qualitative manner by logging Geologists using standardised - colour, mineralogical, lithological, and stratigraphic codes. This would be complemented by a brief written log of the observations. Quantitative logging occurred with regards to the measurement of Rock Quality Designation (RQD). Drill core in lengths of 10 cm or more is measured, and the percentage total of which is calculated for a given length. Photos of core, in both wet and dry states, were taken for later reference once core had been measured and metre intervals marked. The length of logged intervals totals 33,639m 100% of recovered drill samples were logged
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> If core, whether cut or sawn and whether quarter, half or all core taken. If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. 	<ul style="list-style-type: none"> All drill core was cut using an Almonte automatic core saw. Half core or full core samples were taken, with a very small sub-sample of quarter core field duplicates for variability analysis. RC samples were split using an 80/10/10 cone splitter at the rig. All samples below the surface water table ~10m were essentially dry.

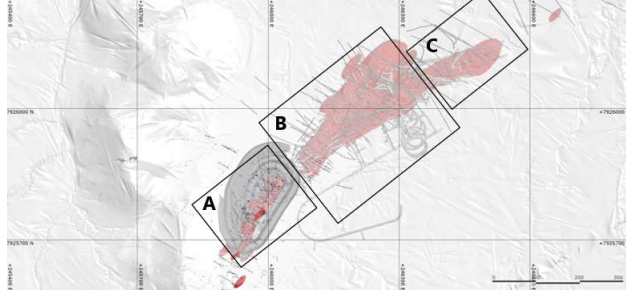
Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> For all sample types, the nature, quality and appropriateness of the sample preparation technique. Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. Whether sample sizes are appropriate to the grain size of the material being sampled. 	<ul style="list-style-type: none"> All sample preparation was in line with industry standards. Minor variations in the process exist between the Century laboratory and the external ALS laboratory. Both RC samples and Diamond drill core followed the same preparation paths. In general, samples are received and digitally logged into a Laboratory Information Management System (LIMS/CCLAS). The samples are then oven dried then crushed to a nominal 2mm or 3mm depending on the laboratory. The sample is then split with approximately 300g retained and pulverised to either 85% passing 75µm (ALS), or 85% passing 53µm (Century). No studies have been carried out with regards to the liberation particle size of the minerals, and no comparative analysis has been carried out between the laboratory pulverisation protocols to this point. These methods are considered appropriate for the style of mineralisation. <p>Century Sample Preparation</p> <pre> graph TD A[Register Samples in CCLAS] --> B[Dry samples in oven - 100°C for 12 hours] B --> C[Remove samples and sort in numerical order] C --> D{Are there any large rocks in the sample?} D -- YES --> E[Crush in 'ESSA' jaw crusher] D -- NO --> F[Pass sample through 'Boyd' crusher rotary split to 200-300g Particle size ~3mm] E --> F F --> G[Pulverise sample in LIMS 90% < 53 microns] F --> H[Reject] H --> I[Dispose Reject unless otherwise instructed] G --> J[Place 50-100g sample into labelled sample bag] J --> K[Retain pulp for Analysis] </pre>

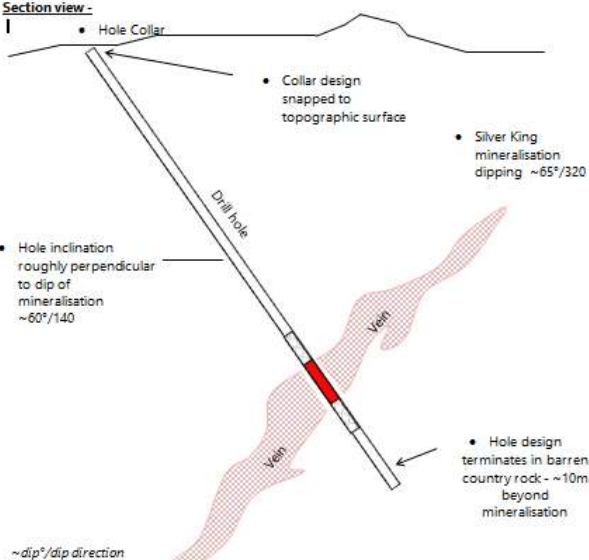
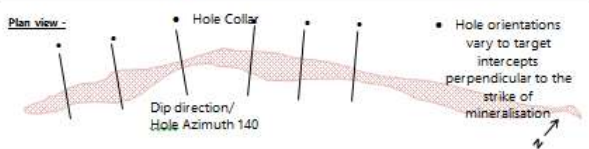
Criteria	JORC Code explanation	Commentary
		<p>ALS Sample Preparation</p> <pre> graph TD A[LOG-22 Affix Bar Code and log sample in LIMS] --> B[WEI-21 Record Received sample weight] B --> C{Is the sample dry?} C -- NO --> D[If samples are excessively wet, the sample should be dried to a maximum of 120°C. (ORY-21)] C -- YES --> D D --> E[CRU-31 Fine crushing of rock chip and drill samples to better than 70% < 2mm] E --> F[SPL-21 Split sample with riffle splitter] F --> G[PUL-31 Up to 250g sample split is pulverized to better than 85% < 75 microns Split sample with riffle splitter] F --> H[Reject] H --> I[Dispose Reject unless otherwise instructed] G --> J[Retain pulp for Analysis] </pre> <ul style="list-style-type: none"> • Duplicate samples were collected and analysed at both the coarse crush split and the pulverised split stages. • The following shows a comparison of half core 'duplicate' samples, or 'field duplicates' • The variance of the respective element is dependent on the degree of homogeneity of the sample tested, and should be roughly equal to, or below the nugget value of the deposit. <p>Original (Filtered) vs Fielddup - Field duplicate (Filtered) for Pb ppm</p> <p>The scatter plot displays the comparison between original and field duplicate samples for lead (Pb) concentration in ppm. The x-axis represents the 'Original Pb ppm' and the y-axis represents the 'Fielddup - Field duplicate Pb ppm'. A solid red line indicates the ideal 1:1 relationship (y=x). Two additional red lines parallel to the y=x line represent the 95% confidence interval. The data points, shown as blue circles, are tightly clustered around the y=x line, indicating high consistency between the original and duplicate samples. The axes range from 0.0000 to 800,000.0000.</p>

Criteria	JORC Code explanation	Commentary
		 <ul style="list-style-type: none"> Overall, despite a small sample set, the indication is that half core duplicates show good correlation. Sample sizes appear appropriate based on variability analysis of duplicates.
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> <i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i> <i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i> <i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i> 	<ul style="list-style-type: none"> Samples were analysed by the following methods - <u>Century Laboratory & ALS Laboratory 2006-2021</u> <ul style="list-style-type: none"> Pb, Zn, Fe, Mn, S, SiO₂: From the pulverised material a 0.1-0.3g sample is taken and dissolved in lithium borate flux used to form a fused disc. This disc is then analysed using a wavelength dispersive X-Ray fluorescence spectrometer. Ag: Silver (Ag) was analysed using an Aqua Regia Digest and an Atomic Absorption Spectrometry (AAS) Finish. For C: From the Pulverised sample carbon (C) was analysed via a leco Carbon Analyzer. Sediment is combusted in an oxygen atmosphere and any carbon present is converted to CO₂. The sample gas flows into a non-dispersive infrared (NDIR) detection cell. The NDIR measures the mass of CO₂ present. The mass is converted to percent carbon based on the dry sample weight. The total organic carbon content is subtracted from the total carbon content to determine the total inorganic carbon content of a given sample <u>ALS Laboratory 2012-Present</u> <ul style="list-style-type: none"> Pb, Zn, Fe, Mn, S, SiO₂: A prepared sample (0.1g) is fused with 1.0g of sodium peroxide flux in a zirconium crucible at 700°C. The resulting melt is cooled and dissolved in dilute hydrochloric acid. This solution is then analysed by inductively coupled plasma - atomic emission spectrometry (ICP-AES) and the results are corrected for spectral inter element interferences. Ag: Silver (Ag) was analysed using an Aqua Regia Digest and an Atomic Absorption Spectrometry (AAS) Finish. C: From the Pulverised sample carbon (C) was analysed via a leco Carbon Analyzer. Sediment is combusted in an oxygen atmosphere and any carbon present is converted to CO₂. The sample gas flows into a non-dispersive infrared (NDIR) detection cell. The NDIR measures the mass of CO₂ present. The mass is converted to percent carbon based on the dry sample weight. The total organic carbon content is subtracted from the total carbon content to determine the total inorganic carbon content of a given sample

Criteria	JORC Code explanation	Commentary																
		<ul style="list-style-type: none">Both the XRF and ICP-AES methods are considered total methods and are consistent with industry standards. Duplicate analysis of samples by both methods indicates no material bias is introduced between the analysis suites.The Century laboratory is accredited by NATA to the ISO/IEC 17025 standard for the analysis of the tailings samples by XRF.No geophysical tools were used for analysis of samples.<u>External Controls</u><ul style="list-style-type: none">The following external controls were used to monitor laboratory accuracy and precision of sample analysis - <table><tr><th>Control</th><th>Objective</th></tr><tr><td>Standards</td><td>To indicate the precision and accuracy of the batch being analysed. Inserted randomly throughout the sample submission.</td></tr><tr><td>Blanks</td><td>To identify potential contamination in the preparation process. Inserted between or following high grade samples to identify potential cross contamination.</td></tr><tr><td>Umpire assays</td><td>To indicate variance in both accuracy and precision between laboratories analytical equipment</td></tr></table> <table><tr><th>Control</th><th>Target Frequency</th></tr><tr><td>Duplicate</td><td>1:20</td></tr><tr><td>Blank</td><td>1:20</td></tr><tr><td>Umpire check</td><td>5%</td></tr></table> <ul style="list-style-type: none"><ul style="list-style-type: none">On receipt of analytical results, control standards are charted to ensure they fall within 2 standard deviations of the accepted mean. Samples outside of 2 standard deviations require action. Actions taken include but are not limited to -<ul style="list-style-type: none">an audit trail check for potential sample swaps or mislabellingre-analysis of sample batch with new standardcomparative analysis against laboratory control standardslaboratory audit of procedures and standardsWhere the issue cannot be resolved the assay batch is not loaded into the database for use in the Mineral Resource estimate.Blanks are plotted to ensure they fall below an accepted upper limit, based on the materiality to the data purpose, and relative to the analytical method. For Silver King a value of 0.1% was selected as the action line. For any values that plotted above this level, actions taken include but were not limited to -<ul style="list-style-type: none">an audit trail check for potential sample swaps or mislabellingre-analysis of sample batch with new blank/standardcomparative analysis against laboratory control standardslaboratory audit of procedures and standards<u>Internal Laboratory Controls</u><ul style="list-style-type: none">The laboratories carry out internal quality control which may also be used for reference when investigating data quality.The frequency, placement and type of QC used is automated in the LIM system (CCLAS EL) and will randomly	Control	Objective	Standards	To indicate the precision and accuracy of the batch being analysed. Inserted randomly throughout the sample submission.	Blanks	To identify potential contamination in the preparation process. Inserted between or following high grade samples to identify potential cross contamination.	Umpire assays	To indicate variance in both accuracy and precision between laboratories analytical equipment	Control	Target Frequency	Duplicate	1:20	Blank	1:20	Umpire check	5%
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Criteria	JORC Code explanation	Commentary
		<p>place repeats and Certified Reference Materials CRMs in sample batches.</p> <ul style="list-style-type: none"> ▪ The Laboratory is regularly audited for continued compliance with ISO/IEC 17025 by NATA. ▪ The Laboratory uses matrix-matched well-certified internal standards inserted into every batch as unknowns, performs one repeat sample every batch. ▪ Blanks are not used as they are unfeasible in fused-bead XRF analysis. ▪ As a requirement of NATA accreditation, the laboratory regularly participates in external proficiency testing.
Verification of sampling and assaying	<ul style="list-style-type: none"> • <i>The verification of significant intersections by either independent or alternative company personnel.</i> • <i>The use of twinned holes.</i> • <i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i> • <i>Discuss any adjustment to assay data.</i> 	<ul style="list-style-type: none"> • In 2013 Umpire samples were sent to ALS laboratories to check for any bias between laboratories. • Following the receipt of results from primary analysis, a random selection of samples with material grades was selected for re-analysis by another independent laboratory; this approached 10% of the total samples for the campaign. • Following analysis, sample pair statistics were investigated to identify any potential bias between laboratories. No material bias was identified in the process. • twinned holes have been drilled to confirm RC drilling results from pre 2012 were acceptable for use in the 2021 Resource Estimate. No issues were found with earlier assays, survey data or logging. • All drilling and sampling data is stored within the NCR geological database managed by Maxwell Geosciences, Datashed5. All data entry and changes are fully auditable and the following controls and measures are in place - <ul style="list-style-type: none"> ○ All logging was completed on into excel templates with drop down boxes that were then uploaded by the Database Administrator. ○ Senior Geologist reviewed all data prior to it being entered into the database. ○ If data was not valid it was sent back to the logging geologist to fix the errors. ○ Data was entered following the Century workflow template shown in the Appendix of the main report. • Melbourne Server • Century Server • No adjustments to assay data have been made. • Where data was deemed invalid or unverifiable it was excluded from the Mineral Resource estimation.
Location of data points	<ul style="list-style-type: none"> • <i>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</i> • <i>Specification of the grid system used.</i> • <i>Quality and adequacy of topographic control.</i> 	<ul style="list-style-type: none"> • <u>Drill-hole Collars</u> <ul style="list-style-type: none"> ○ The drill collars of the holes at Silver King (and access tracks) were located using a TOPCON GPS System, namely a HiPer XT with an FC2500 Field Controller. This system requires a base station to receive constant Satellite information from a fixed, known position. ○ The field work involved holding the Topcon GPS Rover over each drill collar and storing a point when the fixed Satellite position is attained. ○ The co-ordinates are stored in AMG94 • <u>Down-hole Surveys</u> <ul style="list-style-type: none"> ○ Down-hole surveys were taken at 30m intervals for all inclined drill-holes using a Champ Gyro down-hole survey tool, which records - azimuth, inclination, magnetic tool face angle, gravity roll angle, magnetic field strength and temperature. ○ The tool includes a Quality Check function with a predetermined magnetic threshold to highlight survey data that is outside the range of acceptable magnetic interference. Where magnetic interference is

Criteria	JORC Code explanation	Commentary
		<p>encountered, this is logged, and a lower confidence level is assigned to the survey data in the database.</p> <ul style="list-style-type: none"> Low confidence surveys are flagged and this data is excluded from use in the Mineral Resource. All work at Silver King was carried out in AMG94. Century Mine Grid was originally an Exploration grid based on an interpolated position from 1:100,000 map sheet 6660 Lawn Hill and a compass orientation, ie more or less a truncated AMG. All point elevations and Map grid co-ordinates collected reconcile well with the surface features and elevations on the DTM when compared to hole collar pick-ups. The digital terrain model (DTM) used for the topographic surface at Silver King is developed from a recent drone survey conducted by the NCR survey Department. The Drone Survey Report is provided, and all ground control points were collected with a Topcon RTK GPS with real time corrections operating from the Century Mine base GPS station.
Data spacing and distribution	<ul style="list-style-type: none"> Data spacing for reporting of Exploration Results. Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. Whether sample compositing has been applied. 	<ul style="list-style-type: none"> Drill spacing across the deposit is generally in the range of 10-50m along strike and 20-30m down dip.  <p>A. Historic workings - pattern drilled RC and Diamond 10 - 20m spacing.</p> <p>B. Upper zone - mixed orientations 10 - 30m spacing.</p> <p>C. Lower zone - extensional drilling requiring infill >30m.</p> <ul style="list-style-type: none"> The complex, multi-phase mineralisation, of the Silver King deposit results in high apparent variability at the current drill spacing. The potential for short range, high grade structures, is high. The current data spacing provides reasonable confidence in the ranges and continuity of potentially high-grade veins. All Reverse Circulation drill holes used for the resource estimate were sampled at 1m intervals, whilst diamond core was sampled to geological boundaries at 1m intervals with a minimal interval size of 0.25m and maximum of 1.5m. As such, samples were composited to a uniform 1m length within domain bounds for statistical evaluation. Residuals were treated with equivalent statistical weighting.
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material. 	<ul style="list-style-type: none"> The following diagram illustrates the Silver King drill-hole design criteria

Criteria	JORC Code explanation	Commentary
		<p>Section view -</p>  <p>Plan view -</p>  <ul style="list-style-type: none"> Where all design criteria are met, or approximated, no sample bias of structures should be incurred. There is no known material sampling bias within the Silver King Mineral Resource. No material bias is created by the angle of the drilling relative to the angle of the mineralisation as the intercepts are roughly perpendicular
Sample security	<ul style="list-style-type: none"> The measures taken to ensure sample security. 	<ul style="list-style-type: none"> RC samples were collected in individually numbered calico bags at the drill rig. Each number was logged against the respective sample interval by the rig geologist. An inventory of samples was taken by field assistants on collection of the samples from the drill rig to ensure all were accounted for. Samples numbers and intervals were entered into the Datashed database along with all logging data, and hole details. All samples were registered into the Laboratory Information Management System (LIMS) on arrival and reconciled to the submission list.
Audits or reviews	<ul style="list-style-type: none"> The results of any audits or reviews of sampling techniques and data. 	<ul style="list-style-type: none"> No internal or external audits or reviews of the sampling techniques have been carried out

Section 2: Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with 	<ul style="list-style-type: none"> NCR holds a mining lease (ML90045) over the Silver King mine; this has an expiry date of 18/09/2037. As part of an operating mine the Silver King is not subject to any operating restrictions. It is however subject to environmental conditions pertaining to land and water management, as well as adherence to cultural sensitivities pertaining to the local indigenous people. NCR currently holds Mining Lease ML90045 over the Silver King area. There are no known impediments to operating in the area.

Criteria	JORC Code explanation	Commentary
	<i>any known impediments to obtaining a licence to operate in the area.</i>	
<i>Exploration done by other parties</i>	<ul style="list-style-type: none"> Acknowledgment and appraisal of exploration by other parties. 	<ul style="list-style-type: none"> Exploration and Mining has been ongoing for over 100 years in the Burketown Mineral field, there is a large catalogue of historical documents, maps, scientific papers and reports pertaining to the area.
<i>Geology</i>	<ul style="list-style-type: none"> Deposit type, geological setting and style of mineralisation. 	<ul style="list-style-type: none"> Silver King is a structurally hosted Pb-Zn quartz carbonate vein breccia. Mineral relationships in the veins suggest the sphalerite zinc mineralization occurred in one of the earlier phases, with later overprinting by massive galena (Pb-sulphide). The Zinc rich fluids are more pervasive through the host rocks infilling much of the brecciated rock in the fault zone, and along the western H4r/H3 shale to sandstone lithological contact potentially due to contrasting brittle-elastic responses to stress within these rock masses. The Pb zones appear more confined to the fault structure(s) and may indicate later reactivation and infill of the fault(s). The Pb zones are also significantly higher grade than the Zn overall.
<i>Drill hole Information</i>	<ul style="list-style-type: none"> A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: <ul style="list-style-type: none"> easting and northing of the drill hole collar elevation or RL (Reduced Level - elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length. If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case. 	<ul style="list-style-type: none"> Not applicable - no exploration results have been reported; a tabulated summary of drill holes used in the 2021 Mineral Resource may be found in the Appendix 3 of this Announcement.
<i>Data aggregation methods</i>	<ul style="list-style-type: none"> In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. The assumptions used for any reporting of metal equivalent values should be clearly stated. 	<ul style="list-style-type: none"> Not applicable - no exploration results have been reported
<i>Relationship between mineralisation</i>	<ul style="list-style-type: none"> These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to 	<ul style="list-style-type: none"> Not applicable - no exploration results have been reported

Criteria	JORC Code explanation	Commentary
<i>widths and intercept lengths</i>	<p><i>the drill hole angle is known, its nature should be reported.</i></p> <ul style="list-style-type: none"> <i>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').</i> 	
<i>Diagrams</i>	<ul style="list-style-type: none"> <i>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</i> 	<ul style="list-style-type: none"> Not applicable - no exploration results have been reported
<i>Balanced reporting</i>	<ul style="list-style-type: none"> <i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</i> 	<ul style="list-style-type: none"> Not applicable - no exploration results have been reported
<i>Other substantive exploration data</i>	<ul style="list-style-type: none"> <i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i> 	<ul style="list-style-type: none"> Not applicable - no exploration results have been reported
<i>Further work</i>	<ul style="list-style-type: none"> <i>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</i> <i>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i> 	<ul style="list-style-type: none"> Not applicable - no exploration results have been reported

Section 3: Reporting of Resources

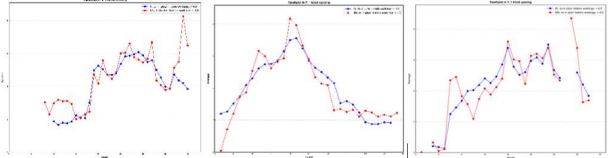
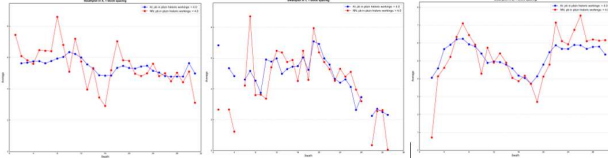
Criteria	JORC Code explanation	Commentary
<i>Database integrity</i>	<ul style="list-style-type: none"> <i>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</i> <i>Data validation procedures used.</i> 	<ul style="list-style-type: none"> NCR has a managed commercial Database. NCR geologists provide the initial review with upload checks and reports provided by Maxgeo. All data is stored within the NCR geological database. Data was exported as .csv and .mdb format files. Qualitative logging is carried out into standardised Microsoft Excel logging spreadsheets with drop down logging codes for each variable. The logging geologist then completes a commentary for the relevant section which should correspond with the logging codes for the interval. Where there is inconsistency the commentary information is prioritised. Data is loaded into Vulcan or Leapfrog mining software and visually inspected for any anomalous logs, surveys or values within the context of the surrounding drill holes. If any areas appear inconsistent with the local trend the original core photos are referred to for confirmation, or alternatively the drill-hole is removed from the estimate as a low confidence data source.

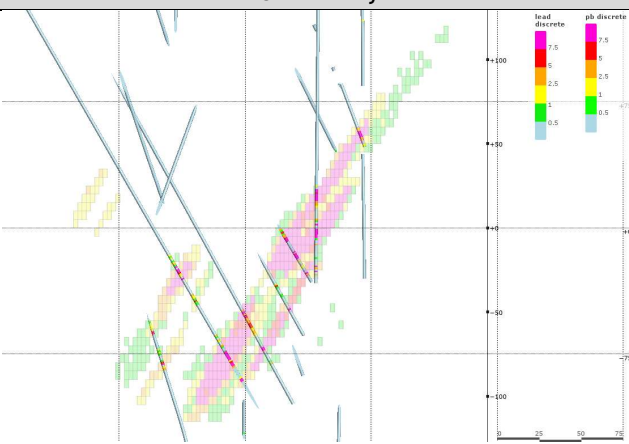
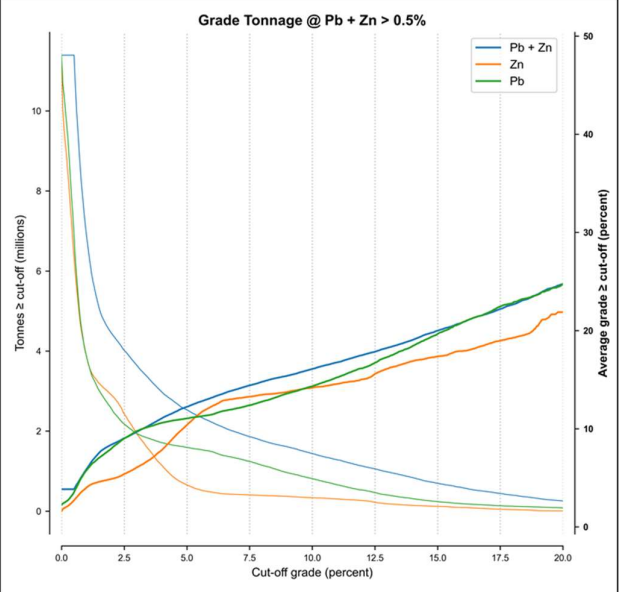
Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> • Transcription errors are unlikely with assay data due to an automated upload process of results from the nominated laboratory. • All changes and updates within the Datashed database are fully auditable and traceable. • Partial data may not be imported to the database, mandatory fields must be completed to allow import to occur. • Mandatory fields are as follows - <ul style="list-style-type: none"> ○ Project code, ○ Prospect code, ○ Hole ID, ○ Hole Type, ○ Tenement, ○ Ranking, ○ Status(Planned/Drilled), ○ Survey method, ○ Easting, ○ Northing, ○ RL, ○ Co-ordinate system, ○ Depth From, ○ Depth To, ○ Hole Diameter, ○ Logging Geologist, ○ Company, ○ Drill Company ○ Logging dates - commenced, completed ○ Survey data - depth, magnetic azimuth, dip, instrument, ranking ○ Sample data - sample ID, from, to, sample type • All results must correspond to identical sample despatch numbers to be accepted.
Site visits	<ul style="list-style-type: none"> • <i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i> • <i>If no site visits have been undertaken indicate why this is the case.</i> 	<ul style="list-style-type: none"> • The Competent Person for the Mineral Resource estimate has worked on similar projects within the district and has modelled epithermal and SEDEX base metals deposits.
Geological interpretation	<ul style="list-style-type: none"> • <i>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</i> • <i>Nature of the data used and of any assumptions made.</i> • <i>The effect, if any, of alternative interpretations on Mineral Resource estimation.</i> • <i>The use of geology in guiding and controlling Mineral Resource estimation.</i> • <i>The factors affecting continuity both of grade and geology.</i> 	<ul style="list-style-type: none"> • Silver King has been explored and mined for over one hundred years. Although many small discrepancies exist between interpretations of the deposit, the general understanding controls, and nature of mineralisation, is good. • Silver King is a structurally hosted Pb-Zn quartz carbonate vein breccia. Mineral relationships in the veins suggest the sphalerite (ZnS) mineralization occurred in several of the early mineralisation phases with later overprinting by massive galena (PbS). • The Zinc rich fluids are more pervasive through the host rocks infilling much of the brecciated rock in the fault zone, and also along the western H4r/H3 shale to sandstone lithological contact; potentially due to contrasting brittle-elastic responses to stress within these rock masses. • The Pb zones appear localised to the fault structure(s) and may indicate reactivation and infill of the fault(s) at a later date. The Pb zones are also significantly higher grade than the Zn overall. • A detailed structural model of the deposit is being generated to better understand the cross reef mineralisation, though this currently makes up a relatively small proportion of the mineralisation at Silver King. • The multi-phase fluid events at the deposit not only manifest as complex mineralogical overprinting within the breccia's and veins

Criteria	JORC Code explanation	Commentary																
		<p>but have promoted highly variable failure paths during fault reactivation due to the brittle nature of the predominant quartz-carbonate fluids once crystallised.</p> <ul style="list-style-type: none">The nature of this mineralisation style requires higher drilling density than typical base metals deposits.The following data was collected for geological logging and analytical assays - <table><tr><th>Data type</th><th>No. Holes</th><th>Total length (m)</th><th>% of total data</th></tr><tr><td>Diamond core drilling</td><td>180</td><td>29,604</td><td>95</td></tr><tr><td>Reverse Circulation drilling</td><td>17</td><td>1,264</td><td>5</td></tr><tr><td>Total</td><td>132</td><td>24,288</td><td>100</td></tr></table> <ul style="list-style-type: none">Where high grade Pb or Zn was encountered in assays, geological structures may be inferred by proxy, where no primary information is available. This assumption was used in the development of the Mineral Domains in Leapfrog.Historic plans and sections were also used as references as to the mineralisation expressions seen during underground mining to aid in the development of the geological model.No surface mapping was carried out as the majority of the Mineral Resource does not have a surface expression. For safety reasons limited work may be carried out around the historic excavations.Greater understanding of the paragenesis of mineralisation along with macro and micro scale controls will always improve geological understanding. This can only be achieved by increasing data density through reduced drill spacing.The mineralisation at Silver King is structurally hosted - as such the fault surface and lithological contacts were used to drive the search ellipses when interpolating mineral domains in Leapfrog® Geo mining software.Mineral Domain grade shells were generated for both Pb and Zn at 2%, 3%, 5%, 3%, and 2%, 3%, 6% respectively. All shells were estimated as individual domains.Visual validation was carried out to ensure grade shells honoured drill intercepts, showed continuity of structure consistent with the geological interpretation, and were without unjustifiable interpolation or extrapolation of the envelopes.Grade data was composited within the geological domains. This data was subsequently used in the generation of variograms used in the Ordinary Kriging estimation process.The continuity of both grade and geology at Silver King is primarily structurally driven through brittle failure of the local rock mass. This allowed fluids to permeate and crystallise in the Silver King system. The extent of the pathways generated, and the fluid compositions determined the grade distribution.Mineralisation events were episodic, with each event showing differing characteristics due to the chemical composition of the fluids and the prevailing conditioning of the rock-mass by earlier events.	Data type	No. Holes	Total length (m)	% of total data	Diamond core drilling	180	29,604	95	Reverse Circulation drilling	17	1,264	5	Total	132	24,288	100
Data type	No. Holes	Total length (m)	% of total data															
Diamond core drilling	180	29,604	95															
Reverse Circulation drilling	17	1,264	5															
Total	132	24,288	100															
Dimensions	<ul style="list-style-type: none">The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.	<ul style="list-style-type: none">The current defined Silver King Mineral Resource is contained within an area which measures <table><tr><td>Strike</td><td>850m</td></tr><tr><td>Across Strike</td><td>200m</td></tr><tr><td>Depth</td><td>400m</td></tr></table> <ul style="list-style-type: none">The true width (across strike) of the mineralised zone ranges from 1m to 50m laterally and is highly variable.The Resource remains open to the north, down plunge.	Strike	850m	Across Strike	200m	Depth	400m										
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Estimation and modelling techniques	<ul style="list-style-type: none">The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.The assumptions made regarding recovery of by-products.Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.Any assumptions behind modelling of selective mining units.Any assumptions about correlation between variables.Description of how the geological interpretation was used to control the resource estimates.Discussion of basis for using or not using grade cutting or capping.The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.	<p>The estimation process can be summarised as follows:</p> <ul style="list-style-type: none">Data was exported from the Datashed database (collar, assay, geology, survey) and a drill hole database was created in Leapfrog.Interpretation and construction of the geology model was carried out in Leapfrog mining softwareLithological and Fault surface wireframes were used to generate a trend surface driving variable search ellipse orientations based on proximity to the associated control.Grade shells were generated using 1m composites of the data, at cut offs for both Pb and Zn. 2%, 3%, 5%, 3%, and 2%, 3%, 6%Domains were visually checked in Leapfrog against drill data for shells of best fit. Isolated and small (<1000cubic metres) domains were removed, and areas of excessive extrapolation were trimmed to a distance consistent with the local interpretation not exceeding half the local drill spacing.Data is composited to 1m intervals within the shells. Areas were classified by location.Population statistics within the zones were assessed within Leapfrog Edge software package.Variograms were then generated within Leapfrog Edge.The Block model was then constructed in Leapfrog Edge utilising the geology model and grade shell surfaces. Coding of blocks follows Leapfrog's implicit processes. An evaluated geology model is linked to the block model and coded appropriately.Block coding was then visually validated in graphical sections against the source surfaces and shellsBlock Estimation Parameters were then set up in Leapfrog Edge for Pb, Zn, Ag. Other elements (Fe, C, Mn, Mg, S) were assessed by stratigraphic domain.Domain boundaries and composite selection <table><tr><th colspan="2">General</th><th colspan="2">Boundary Analysis</th><th colspan="2">Compositing</th></tr><tr><th>Name</th><th>Domain</th><th>Values</th><th>Boundary</th><th>Composite in</th><th>Composite length</th></tr><tr><td>ag in STRAT MODEL H3</td><td>Stratigraphy: H3</td><td>ag</td><td>hard</td><td>Within boundary</td><td>1</td></tr><tr><td>ag in STRAT MODEL H4e</td><td>Stratigraphy: H4e</td><td>ag</td><td>hard</td><td>Within boundary</td><td>1</td></tr><tr><td>ag in ag: 10.0 - 50.0</td><td>ag</td><td>10.0 - 50.0</td><td>ag</td><td>Within boundary</td><td>1</td></tr><tr><td>ag in ag: 50.0 - 100.0</td><td>ag</td><td>50.0 - 100.0</td><td>ag</td><td>Within boundary</td><td>1</td></tr><tr><td>ag in ag: < 10.0</td><td>ag</td><td>< 10.0</td><td>ag</td><td>Within boundary</td><td>1</td></tr><tr><td>ag in ag: > 100.0</td><td>ag</td><td>> 100.0</td><td>ag</td><td>Within boundary</td><td>1</td></tr><tr><td>pb in STRAT MODEL H3</td><td>Stratigraphy: H3</td><td>pb</td><td>hard</td><td>Within boundary</td><td>1</td></tr><tr><td>pb in STRAT MODEL H4e</td><td>Stratigraphy: H4e</td><td>pb</td><td>hard</td><td>Within boundary</td><td>1</td></tr><tr><td>pb in pb: 2.0 - 5.0</td><td>pb</td><td>2.0 - 5.0</td><td>pb</td><td>Within boundary</td><td>1</td></tr><tr><td>pb in pb: < 2.0</td><td>pb</td><td>< 2.0</td><td>pb</td><td>Within boundary</td><td>1</td></tr><tr><td>pb in pb: > 5.0</td><td>pb</td><td>> 5.0</td><td>pb</td><td>Within boundary</td><td>1</td></tr><tr><td>zn in STRAT MODEL H3</td><td>Stratigraphy: H3</td><td>zn</td><td>hard</td><td>Within boundary</td><td>1</td></tr><tr><td>zn in STRAT MODEL H4e</td><td>Stratigraphy: H4e</td><td>zn</td><td>hard</td><td>Within boundary</td><td>1</td></tr><tr><td>zn in zn: 2.0 - 6.0</td><td>zn</td><td>2.0 - 6.0</td><td>zn</td><td>Within boundary</td><td>1</td></tr><tr><td>zn in zn: < 2.0</td><td>zn</td><td>< 2.0</td><td>zn</td><td>Within boundary</td><td>1</td></tr><tr><td>zn in zn: > 6.0</td><td>zn</td><td>> 6.0</td><td>zn</td><td>Within boundary</td><td>1</td></tr></table> <ul style="list-style-type: none">Domain model runs and discretisation. <table><tr><th colspan="2">General</th><th colspan="2">Value clipping</th><th colspan="2">Discretisation</th><th colspan="2">Continuity Model</th></tr><tr><th>Name</th><th>Domain</th><th>Values</th><th>Estimate Name</th><th>Open</th><th>Close</th><th>Model Name</th><th>Model Name</th></tr><tr><td>kr, ag in STRAT MODEL H3</td><td>Stratigraphy: H3</td><td>ag</td><td>ag in STRAT MODEL H3</td><td>0.1</td><td>25</td><td>ag in STRAT MODEL H3</td><td>ag in STRAT MODEL H3</td></tr><tr><td>kr, ag in STRAT MODEL H4e</td><td>Stratigraphy: H4e</td><td>ag</td><td>ag in STRAT MODEL H4e</td><td>0.1</td><td>25</td><td>ag in STRAT MODEL H4e</td><td>ag in STRAT MODEL H4e</td></tr><tr><td>kr, ag in ag: 10.0 - 50.0</td><td>ag</td><td>10.0 - 50.0</td><td>ag</td><td>10.0 - 50.0</td><td>25</td><td>ag in ag: 10.0 - 50.0</td><td>ag in ag: 10.0 - 50.0</td></tr><tr><td>kr, ag in ag: 50.0 - 100.0</td><td>ag</td><td>50.0 - 100.0</td><td>ag</td><td>50.0 - 100.0</td><td>25</td><td>ag in ag: 50.0 - 100.0</td><td>ag in ag: 50.0 - 100.0</td></tr><tr><td>kr, ag in ag: < 10.0</td><td>ag</td><td>< 10.0</td><td>ag</td><td>< 10.0</td><td>25</td><td>ag in ag: < 10.0</td><td>ag in ag: < 10.0</td></tr><tr><td>kr, ag in ag: > 100.0</td><td>ag</td><td>> 100.0</td><td>ag</td><td>> 100.0</td><td>25</td><td>ag in ag: > 100.0</td><td>ag in ag: > 100.0</td></tr><tr><td>kr, pb in STRAT MODEL H3</td><td>Stratigraphy: H3</td><td>pb</td><td>pb in STRAT MODEL H3</td><td>0.001125</td><td>5</td><td>pb in STRAT MODEL H3</td><td>pb in STRAT MODEL H3</td></tr><tr><td>kr, pb in STRAT MODEL H4e</td><td>Stratigraphy: H4e</td><td>pb</td><td>pb in STRAT MODEL H4e</td><td>0.001125</td><td>5</td><td>pb in STRAT MODEL H4e</td><td>pb in STRAT MODEL H4e</td></tr><tr><td>kr, pb in pb: 2.0 - 5.0</td><td>pb</td><td>2.0 - 5.0</td><td>pb</td><td>2.0 - 5.0</td><td>5</td><td>pb in pb: 2.0 - 5.0</td><td>pb in pb: 2.0 - 5.0</td></tr><tr><td>kr, pb in pb: < 2.0</td><td>pb</td><td>< 2.0</td><td>pb</td><td>< 2.0</td><td>5</td><td>pb in pb: < 2.0</td><td>pb in pb: < 2.0</td></tr><tr><td>kr, pb in pb: > 5.0</td><td>pb</td><td>> 5.0</td><td>pb</td><td>> 5.0</td><td>5</td><td>pb in pb: > 5.0</td><td>pb in pb: > 5.0</td></tr><tr><td>kr, zn in STRAT MODEL H3</td><td>Stratigraphy: H3</td><td>zn</td><td>zn in STRAT MODEL H3</td><td>0.006180723</td><td>4</td><td>zn in STRAT MODEL H3</td><td>zn in STRAT MODEL H3</td></tr><tr><td>kr, zn in STRAT MODEL H4e</td><td>Stratigraphy: H4e</td><td>zn</td><td>zn in STRAT MODEL H4e</td><td>0.006180723</td><td>4</td><td>zn in STRAT MODEL H4e</td><td>zn in STRAT MODEL H4e</td></tr><tr><td>kr, zn in zn: 2.0 - 6.0</td><td>zn</td><td>2.0 - 6.0</td><td>zn</td><td>2.0 - 6.0</td><td>4</td><td>zn in zn: 2.0 - 6.0</td><td>zn in zn: 2.0 - 6.0</td></tr><tr><td>kr, zn in zn: < 2.0</td><td>zn</td><td>< 2.0</td><td>zn</td><td>< 2.0</td><td>4</td><td>zn in zn: < 2.0</td><td>zn in zn: < 2.0</td></tr><tr><td>kr, zn in zn: > 6.0</td><td>zn</td><td>> 6.0</td><td>zn</td><td>> 6.0</td><td>4</td><td>zn in zn: > 6.0</td><td>zn in zn: > 6.0</td></tr></table> <ul style="list-style-type: none">Domain searches and grade restrictions. <table><tr><th colspan="2">General</th><th colspan="2">Ellipsoid Ranges</th><th colspan="2">Ellipsoid Directions</th><th colspan="2">Number of Samples</th><th colspan="2">Outlier Restrictions</th></tr><tr><th>Name</th><th>Domain</th><th>Values</th><th>Maximum</th><th>Minimum</th><th>Dip</th><th>Up Azimuth</th><th>Pitch</th><th>Min</th><th>Max</th></tr><tr><td>kr, ag in STRAT MODEL H3</td><td>Stratigraphy: H3</td><td>ag</td><td>90</td><td>75</td><td>35</td><td>337.4468</td><td>73.54709</td><td>4</td><td>20</td></tr><tr><td>kr, ag in STRAT MODEL H4e</td><td>Stratigraphy: H4e</td><td>ag</td><td>90</td><td>75</td><td>35</td><td>337.4468</td><td>73.54709</td><td>4</td><td>20</td></tr><tr><td>kr, ag in ag: 10.0 - 50.0</td><td>ag</td><td>10.0 - 50.0</td><td>70</td><td>70</td><td>35</td><td>337.4468</td><td>73.54709</td><td>4</td><td>20</td></tr><tr><td>kr, ag in ag: 50.0 - 100.0</td><td>ag</td><td>50.0 - 100.0</td><td>70</td><td>70</td><td>35</td><td>337.4468</td><td>73.54709</td><td>4</td><td>20</td></tr><tr><td>kr, ag in ag: < 10.0</td><td>ag</td><td>< 10.0</td><td>70</td><td>70</td><td>35</td><td>337.4468</td><td>73.54709</td><td>4</td><td>20</td></tr><tr><td>kr, ag in ag: > 100.0</td><td>ag</td><td>> 100.0</td><td>80</td><td>70</td><td>35</td><td>337.4468</td><td>73.54709</td><td>4</td><td>20</td></tr><tr><td>kr, pb in STRAT MODEL H3</td><td>Stratigraphy: H3</td><td>pb</td><td>75</td><td>50</td><td>35</td><td>337.4468</td><td>147.8016</td><td>4</td><td>20</td></tr><tr><td>kr, pb in STRAT MODEL H4e</td><td>Stratigraphy: H4e</td><td>pb</td><td>75</td><td>50</td><td>35</td><td>337.4468</td><td>147.8016</td><td>4</td><td>20</td></tr><tr><td>kr, pb in pb: 2.0 - 5.0</td><td>pb</td><td>2.0 - 5.0</td><td>60</td><td>40</td><td>35</td><td>337.4468</td><td>147.8016</td><td>4</td><td>20</td></tr><tr><td>kr, pb in pb: < 2.0</td><td>pb</td><td>< 2.0</td><td>60</td><td>40</td><td>35</td><td>337.4468</td><td>147.8016</td><td>4</td><td>20</td></tr><tr><td>kr, pb in pb: > 5.0</td><td>pb</td><td>> 5.0</td><td>60</td><td>40</td><td>35</td><td>337.4468</td><td>147.8016</td><td>4</td><td>20</td></tr><tr><td>kr, zn in STRAT MODEL H3</td><td>Stratigraphy: H3</td><td>zn</td><td>50</td><td>40</td><td>35</td><td>337.4468</td><td>26.95437</td><td>4</td><td>20</td></tr><tr><td>kr, zn in STRAT MODEL H4e</td><td>Stratigraphy: H4e</td><td>zn</td><td>50</td><td>40</td><td>35</td><td>337.4468</td><td>26.95437</td><td>4</td><td>20</td></tr><tr><td>kr, zn in zn: 2.0 - 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General		Boundary Analysis		Compositing		Name	Domain	Values	Boundary	Composite in	Composite length	ag in STRAT MODEL H3	Stratigraphy: H3	ag	hard	Within boundary	1	ag in STRAT MODEL H4e	Stratigraphy: H4e	ag	hard	Within boundary	1	ag in ag: 10.0 - 50.0	ag	10.0 - 50.0	ag	Within boundary	1	ag in ag: 50.0 - 100.0	ag	50.0 - 100.0	ag	Within boundary	1	ag in ag: < 10.0	ag	< 10.0	ag	Within boundary	1	ag in ag: > 100.0	ag	> 100.0	ag	Within boundary	1	pb in STRAT MODEL H3	Stratigraphy: H3	pb	hard	Within boundary	1	pb in STRAT MODEL H4e	Stratigraphy: H4e	pb	hard	Within boundary	1	pb in pb: 2.0 - 5.0	pb	2.0 - 5.0	pb	Within boundary	1	pb in pb: < 2.0	pb	< 2.0	pb	Within boundary	1	pb in pb: > 5.0	pb	> 5.0	pb	Within boundary	1	zn in STRAT MODEL H3	Stratigraphy: H3	zn	hard	Within boundary	1	zn in STRAT MODEL H4e	Stratigraphy: H4e	zn	hard	Within boundary	1	zn in zn: 2.0 - 6.0	zn	2.0 - 6.0	zn	Within boundary	1	zn in zn: < 2.0	zn	< 2.0	zn	Within boundary	1	zn in zn: > 6.0	zn	> 6.0	zn	Within boundary	1	General		Value clipping		Discretisation		Continuity Model		Name	Domain	Values	Estimate Name	Open	Close	Model Name	Model Name	kr, ag in STRAT MODEL H3	Stratigraphy: H3	ag	ag in STRAT MODEL H3	0.1	25	ag in STRAT MODEL H3	ag in STRAT MODEL H3	kr, ag in STRAT MODEL H4e	Stratigraphy: H4e	ag	ag in STRAT MODEL H4e	0.1	25	ag in STRAT MODEL H4e	ag in STRAT MODEL H4e	kr, ag in ag: 10.0 - 50.0	ag	10.0 - 50.0	ag	10.0 - 50.0	25	ag in ag: 10.0 - 50.0	ag in ag: 10.0 - 50.0	kr, ag in ag: 50.0 - 100.0	ag	50.0 - 100.0	ag	50.0 - 100.0	25	ag in ag: 50.0 - 100.0	ag in ag: 50.0 - 100.0	kr, ag in ag: < 10.0	ag	< 10.0	ag	< 10.0	25	ag in ag: < 10.0	ag in ag: < 10.0	kr, ag in ag: > 100.0	ag	> 100.0	ag	> 100.0	25	ag in ag: > 100.0	ag in ag: > 100.0	kr, pb in STRAT MODEL H3	Stratigraphy: H3	pb	pb in STRAT MODEL H3	0.001125	5	pb in STRAT MODEL H3	pb in STRAT MODEL H3	kr, pb in STRAT MODEL H4e	Stratigraphy: H4e	pb	pb in STRAT MODEL H4e	0.001125	5	pb in STRAT MODEL H4e	pb in STRAT MODEL H4e	kr, pb in pb: 2.0 - 5.0	pb	2.0 - 5.0	pb	2.0 - 5.0	5	pb in pb: 2.0 - 5.0	pb in pb: 2.0 - 5.0	kr, pb in pb: < 2.0	pb	< 2.0	pb	< 2.0	5	pb in pb: < 2.0	pb in pb: < 2.0	kr, pb in pb: > 5.0	pb	> 5.0	pb	> 5.0	5	pb in pb: > 5.0	pb in pb: > 5.0	kr, zn in STRAT MODEL H3	Stratigraphy: H3	zn	zn in STRAT MODEL H3	0.006180723	4	zn in STRAT MODEL H3	zn in STRAT MODEL H3	kr, zn in STRAT MODEL H4e	Stratigraphy: H4e	zn	zn in STRAT MODEL H4e	0.006180723	4	zn in STRAT MODEL H4e	zn in STRAT MODEL H4e	kr, zn in zn: 2.0 - 6.0	zn	2.0 - 6.0	zn	2.0 - 6.0	4	zn in zn: 2.0 - 6.0	zn in zn: 2.0 - 6.0	kr, zn in zn: < 2.0	zn	< 2.0	zn	< 2.0	4	zn in zn: < 2.0	zn in zn: < 2.0	kr, zn in zn: > 6.0	zn	> 6.0	zn	> 6.0	4	zn in zn: > 6.0	zn in zn: > 6.0	General		Ellipsoid Ranges		Ellipsoid Directions		Number of Samples		Outlier Restrictions		Name	Domain	Values	Maximum	Minimum	Dip	Up Azimuth	Pitch	Min	Max	kr, ag in STRAT MODEL H3	Stratigraphy: H3	ag	90	75	35	337.4468	73.54709	4	20	kr, ag in STRAT MODEL H4e	Stratigraphy: H4e	ag	90	75	35	337.4468	73.54709	4	20	kr, ag in ag: 10.0 - 50.0	ag	10.0 - 50.0	70	70	35	337.4468	73.54709	4	20	kr, ag in ag: 50.0 - 100.0	ag	50.0 - 100.0	70	70	35	337.4468	73.54709	4	20	kr, ag in ag: < 10.0	ag	< 10.0	70	70	35	337.4468	73.54709	4	20	kr, ag in ag: > 100.0	ag	> 100.0	80	70	35	337.4468	73.54709	4	20	kr, pb in STRAT MODEL H3	Stratigraphy: H3	pb	75	50	35	337.4468	147.8016	4	20	kr, pb in STRAT MODEL H4e	Stratigraphy: H4e	pb	75	50	35	337.4468	147.8016	4	20	kr, pb in pb: 2.0 - 5.0	pb	2.0 - 5.0	60	40	35	337.4468	147.8016	4	20	kr, pb in pb: < 2.0	pb	< 2.0	60	40	35	337.4468	147.8016	4	20	kr, pb in pb: > 5.0	pb	> 5.0	60	40	35	337.4468	147.8016	4	20	kr, zn in STRAT MODEL H3	Stratigraphy: H3	zn	50	40	35	337.4468	26.95437	4	20	kr, zn in STRAT MODEL H4e	Stratigraphy: H4e	zn	50	40	35	337.4468	26.95437	4	20	kr, zn in zn: 2.0 - 6.0	zn	2.0 - 6.0	70	60	35	337.4468	133.3538	4	20	kr, zn in zn: < 2.0	zn	< 2.0	70	60	35	337.4468	133.3538	4	20	kr, zn in zn: > 6.0	zn	> 6.0	80	60	35	337.4468	133.3538	4	20
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Criteria	JORC Code explanation	Commentary																																			
		<ul style="list-style-type: none">As compared to the 2017 Mineral Resource above 5% Pb+Zn<table><tr><th>Classification</th><th>Mt</th><th>Pb%</th><th>Zn%</th><th>Ag g/t</th></tr><tr><td>Measured</td><td>-</td><td>-</td><td>-</td><td>-</td></tr><tr><td>Indicated</td><td>2.12</td><td>8.9</td><td>6.6</td><td>86</td></tr><tr><td>Inferred</td><td>0.11</td><td>7.9</td><td>6.8</td><td>79</td></tr><tr><td>Total</td><td>2.23</td><td>8.9</td><td>6.6</td><td>85</td></tr></table>No recovery assumptions are included in the Resource model.No deleterious elements have been identified for use in this estimation,The recoveries of the adjacent Century deposit are impacted by organic carbon within the black shales and should be a consideration in future. However, this is not considered a significant risk to the project or material to the Mineral Resource at this stage.The following table summarises the sample spacing relative to the block size -<table><tr><td>Sample spacing along strike</td><td>10-40m</td></tr><tr><td>Sample spacing down dip</td><td>15-30m</td></tr><tr><td>Parent block size xyz</td><td>5m x 10m x 2.5m</td></tr><tr><td>Sub-block size xyz</td><td>NA</td></tr><tr><td>Search</td><td>Variable on domain</td></tr></table>No selective mining units have been assumed in the global estimate.Correlation between lead and silver exists due to silver being present within the mineral lattice of the galena (PbS) crystals. This is also evident when comparing the population statistics of the two elements.A spatial correlation exists for all mineralised material due to the structurally controlled nature of the deposit. There are however, distinct zones internally where either Zn or Pb are dominant.A further assumption regarding the correlation of variables was made between that of the Base metal content by percentage and the overall rock density. The greater base metal content the greater the density - this relationship is displayed in the Bulk Density section.Block estimates were primarily checked visually in section against drillhole grades to highlight any fundamental flaws in the estimate.Subsequent drift analysis was also carried out to identify any significant variances between composite and block grades. This data showed some local variance, however globally the estimate appears reasonable.Zn Swath<div></div>Pb Swath<div></div>A sectional comparison of composites (pb discrete) vs blocks (lead discrete) for the more variable Pb estimates highlights the high variability between blocks and composites locally.	Classification	Mt	Pb%	Zn%	Ag g/t	Measured	-	-	-	-	Indicated	2.12	8.9	6.6	86	Inferred	0.11	7.9	6.8	79	Total	2.23	8.9	6.6	85	Sample spacing along strike	10-40m	Sample spacing down dip	15-30m	Parent block size xyz	5m x 10m x 2.5m	Sub-block size xyz	NA	Search	Variable on domain
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Criteria	JORC Code explanation	Commentary
		
Moisture	<ul style="list-style-type: none"> Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content. 	<ul style="list-style-type: none"> Dry density has been used for insitu estimation of the Mineral Resource
Cut-off parameters	<ul style="list-style-type: none"> The basis of the adopted cut-off grade(s) or quality parameters applied. 	<ul style="list-style-type: none"> A resource cut-off 4% combined Pb/Zn was used for reporting purposes, this was developed through the Silver King feasibility study results. 
Mining factors or assumptions	<ul style="list-style-type: none"> Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made. 	<ul style="list-style-type: none"> The only mining assumption considered in the Estimation of the Mineral Resource was the potential mining bench height. Based on a proposed open pit option, as well as the current equipment fleet, a block height of 5m was chosen. Block sizes in the x and y dimensions were optimised relative to the resolution of the data No other mining factors or assumptions have been used in the Mineral Resource Estimate.

Criteria	JORC Code explanation	Commentary
Metallurgical factors or assumptions	<ul style="list-style-type: none"> The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made. 	<ul style="list-style-type: none"> No Metallurgical factors or assumptions have been used in the Mineral Resource Estimation.
Environmental factors or assumptions	<ul style="list-style-type: none"> Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made. 	<ul style="list-style-type: none"> No Environmental factors or assumptions have been used in the Mineral Resource Estimation.
Bulk density	<ul style="list-style-type: none"> Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples. The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit. Discuss assumptions for bulk density estimates used in the evaluation process of the different materials. 	<ul style="list-style-type: none"> Block densities were calculated by a grade weighted regression calculation based on density sample data. All values used were dry. An equivalence factor was calculated to normalise the respective Pb & Zn grades relative to their elemental density. Pb specific gravity = 11.35 g/cm³ Zn specific gravity = 7.11 g/cm³ Pb equivalent adjustment factor = 0.627 * Zn grade Rock density was calculated based on 680 measurements carried out on drill core samples from the 2021 drilling campaign. Archimedes Method was used as opposed to pulps via pycnometer. <div data-bbox="763 1434 1369 1843"> <p>pbzn vstd</p> <p>$y = 0.0003x^2 + 0.0286x + 2.6511$</p> </div> <ul style="list-style-type: none"> The resulting density formula is - $SG = 0.0003x^2 + 0.0286x + 2.6511$

Criteria	JORC Code explanation	Commentary																																										
		<ul style="list-style-type: none">SG was applied using block grades in the post processing.In most cases core recovery approached 100% indicating minimal influence from voids, or vugs across the deposit. Where recovery was not 100% this could generally be attributed to sample loss due to poor rock competenceThe site method for determining rock density prior to 2012 was a hydrostatic immersion method based on Archimedes principle. Samples were weighed in their original state, saturated, dry, and submerged in water. From these measurements both rock density and moisture content may be calculated.Specific Gravity from Australian Laboratory Services (ALS) was calculated using a pycnometer method in 2012 and via hydrostatic method in the 2021 campaign.The pycnometer is filled with 3g of pulverised sample and then filled with a solvent (methanol). The specific gravity is determined by -Weight of Sample (g)/Weight of solvent displaced (g) x Specific Gravity of SolventSpecific Gravity from the laboratory is directly converted to Rock Density in the Silver King density calculations. No allowance has been made for temperature.Due to the high density contrast between mineralised and non-mineralised material when considering economic base metal deposits a grade based density formula was established. The process by which this was derived is outlined above. All density values used are dry.																																										
Classification	<ul style="list-style-type: none">The basis for the classification of the Mineral Resources into varying confidence categories.Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).Whether the result appropriately reflects the Competent Person's view of the deposit.	<table><tr><th>Classification</th><th>Mass</th><th>Pb + Zn</th><th>Pb</th><th>Zn</th><th>Ag</th><th>SG</th></tr><tr><td></td><td>Mt</td><td>%</td><td>%</td><td>%</td><td>g/t</td><td>t/m³</td></tr><tr><td>measured</td><td>1.0</td><td>10.7</td><td>5.7</td><td>5.1</td><td>58</td><td>2.91</td></tr><tr><td>indicated</td><td>2.1</td><td>10.2</td><td>5.2</td><td>5.0</td><td>44</td><td>2.89</td></tr><tr><td>inferred</td><td>0.6</td><td>8.4</td><td>6.0</td><td>2.5</td><td>32</td><td>2.86</td></tr><tr><td>Total</td><td>3.7</td><td>10.0</td><td>5.5</td><td>4.5</td><td>46</td><td>2.89</td></tr></table> <ul style="list-style-type: none">Silver King Deposit 2021 Mineral Resource, Resource cut-off Pb + Zn > 4%The Mineral Resource reflects the accepted Geological interpretation of the deposit. Only verifiable data sources were used, and pragmatic steps to validate assumptions were taken.Although the apparent down-hole nugget effect of the deposit is relatively low, the highly variable nature of the mineralisation style results in moderate to high variability at reasonably short ranges relative to the drill spacing. This results in some poor statistical metrics relevant to estimation quality.These limitations have been considered in the classification of the deposit. The classification reflects the Competent Person's view of the deposit.	Classification	Mass	Pb + Zn	Pb	Zn	Ag	SG		Mt	%	%	%	g/t	t/m ³	measured	1.0	10.7	5.7	5.1	58	2.91	indicated	2.1	10.2	5.2	5.0	44	2.89	inferred	0.6	8.4	6.0	2.5	32	2.86	Total	3.7	10.0	5.5	4.5	46	2.89
Classification	Mass	Pb + Zn	Pb	Zn	Ag	SG																																						
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Total	3.7	10.0	5.5	4.5	46	2.89																																						
Audits or reviews	<ul style="list-style-type: none">The results of any audits or reviews of Mineral Resource estimates.	<ul style="list-style-type: none">The 2021 geology and resource model was reviewed by NCR Geology Manager Damian O'Donohue.Much of the work done for the 2021 Resource Estimate was as a response to a review conducted by Mining Plus in 2019. All recommendation and drill spacing requirements were met.The Mineral Resource estimate is a global estimate to be used in Project Optimisation Planning work.																																										
Discussion of relative accuracy/ confidence	<ul style="list-style-type: none">Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or	<ul style="list-style-type: none">The Mineral Resource reflects the accepted Geological interpretation of the deposit. Only verifiable data sources were used, and pragmatic steps to validate assumptions were taken.Although the apparent down-hole nugget effect of the deposit is relatively low, the highly variable nature of the mineralisation style results in moderate to high variability at reasonably short ranges relative to the drill spacing. This results in some poor statistical metrics relevant to estimation quality.																																										

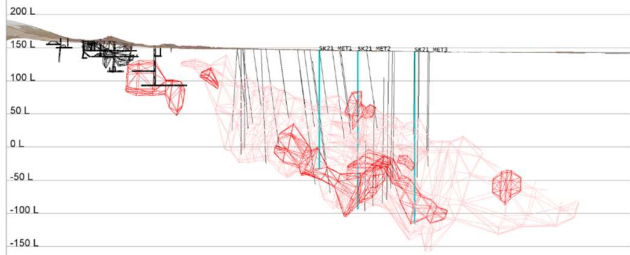
Criteria	JORC Code explanation	Commentary
	<p><i>geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</i></p> <ul style="list-style-type: none"> <i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i> <i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i> 	<ul style="list-style-type: none"> These limitation have been considered in the classification of the deposit.

Silver King Underground

Section 4: Reporting of Reserves

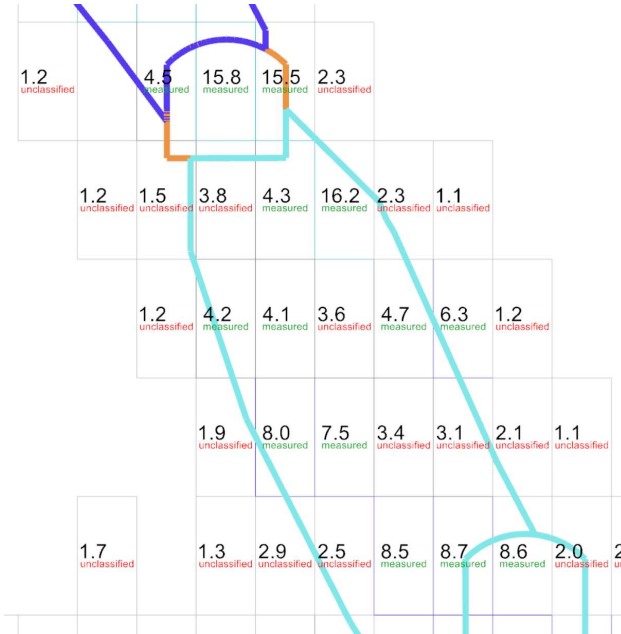
Criteria	JORC Code Explanation	Commentary
Mineral Resource Estimate for conversion to Ore Reserves	<ul style="list-style-type: none"> <i>Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.</i> <i>Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.</i> 	<ul style="list-style-type: none"> The underground Ore Reserve estimate is based on the Mineral Resource estimate carried out by New Century Resources. The Mineral Resource estimate used as a basis for conversion to an Ore Reserves is the 2021 Silver King Mineral Resource Estimate. The Mineral Resource Model used in this estimate is referred to as SK_UG_v3.dm Mineral Resources are reported inclusive of the Ore Reserves The Ore Reserve has been declared at the point where ore is delivered to the Run of Mine pad.
Site visits	<ul style="list-style-type: none"> <i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i> <i>If no site visits have been undertaken indicate why this is the case.</i> 	<ul style="list-style-type: none"> The Competent Person is employed full time on site at Century Mine, Lawn Hill, QLD
Study Status	<ul style="list-style-type: none"> <i>The type and level of study undertaken to enable Mineral Resources to be +converted to Ore Reserves.</i> <i>The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.</i> 	<ul style="list-style-type: none"> The level of study undertaken to enable the Mineral Resources to be converted to Ore Reserves is representative of a Feasibility Study and comprises of mining, infrastructure and process designs completed with sufficient rigour to serve as the basis of an investment decision, as defined in Clause 40 of the JORC Code 2012. The Silver King Underground mine plan exists wholly within a current Mining Lease and necessary amendments to approvals to allow for underground mining are expected to be approved by the relevant government departments within the specified project time frame. In the opinion of the Competent Person there are no reasonable grounds that statutory approvals will not be granted in the timeframes outlined in studies. A mine plan has been developed which is economically viable and technically achievable.
Cut-off parameters	<ul style="list-style-type: none"> <i>The basis of the cut-off grade(s) or quality parameters applied.</i> 	<ul style="list-style-type: none"> Cut-off parameters are based on costs calculated in a Life of Mine financial model. Inputs to the calculation of cut-off grades include mining costs, metallurgical recoveries, pipeline, shipping,

Criteria	JORC Code Explanation	Commentary
		<p>treatment and refining costs, general and administrative costs, royalties and metal prices.</p> <ul style="list-style-type: none"> • Cut-off grades are based on an assumption of: <ul style="list-style-type: none"> ◦ Zinc USD \$2450/t ◦ Lead USD \$1730/t ◦ Silver USD \$22/oz ◦ Exchange Rate 0.74 AUD/USD • Optimisation was completed on the underground design. In a process including several iterations, outputs from the plan were exported to the financial model to generate a range of simplified mining costs, with the schedule resource levelled after each iteration, results exported and then re-imported. The simplified mining costs from the model were re-imported into Deswik and evaluated against Net Smelter Return for each mining shape to determine inclusion/exclusion from the Ore Reserve Estimate. • Stopping - All Stopping Cut-Off parameters are considered on a fully costed basis. The cost is considered after the necessary development has been completed. The stopping cut-off grade is NSR of AUD \$105/t. The cost of double handling material, sourcing remnant material to meet a backfill deficiency, greater distribution of fixed costs as development is completed and the mine transitions to a stopping only phase, and the requirement for cemented rock fill in some stopes has resulted in the average stopping cost being slightly above that of fully costed development. • Development Fully Costed - Fully costed development is that generates a profit, without requiring an associated stope to generate a profit to pay for the costs of both activities. This cut-off grade is NSR of AUD \$100/t. • Development Incremental - Incremental development is considered development that: <ul style="list-style-type: none"> ◦ Would not pay for itself but must be mined to access a profit generating unit of ore which generates a fully costed profit for both tasks. ◦ This material is considered part of the Ore Reserve if the NSR is 1.1x the cost of Haulage, Maintenance, Processing and Site G&A costs. This cut-off grade is NSR of AUD \$53/t
Mining factors or assumptions	<ul style="list-style-type: none"> • <i>The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).</i> • <i>The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.</i> • <i>The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.</i> • <i>The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).</i> • <i>The mining dilution factors used.</i> • <i>The mining recovery factors used.</i> • <i>Any minimum mining widths used.</i> • <i>The manner in which Inferred Mineral Resources are utilised in</i> 	<ul style="list-style-type: none"> • A combination of underground mining methods have been incorporated into the Silver King Underground mine design and are predominantly described as modified avoca; sub-level open stoping; uphole stoping and transverse stoping in wide ore zones including double lift stoping where hanging wall conditions permit and floor benching with post cemented rock fill to establish sill pillar(s) to bring production forward. • A detailed mine design has been developed in Deswik Cad and Interactive Scheduler which includes a detailed underground mine plan and associated schedule. • All stope shapes were manually drafted due to the complex nature of the vein style mineralisation, and preference for selectivity and practicality. <ul style="list-style-type: none"> ◦ Stopes were all created based on a 20 m strike length and it was recognised that in operations the strike will vary in longitudinal zones. Stope height varies from 20 m single lift to 40 m double lift in transverse zones where the hangingwall conditions allow. ◦ Optimisation was completed on the underground design in an iterative process to determine the cut-off parameters ◦ Development dilution is assumed to be 10%. ◦ Stopping dilution assumptions are based on stope size. ◦ Stopes <2,200 t = 20% Dilution ◦ Stopes >2,200 t < 10 kt = 10% Dilution ◦ Stopes >10 kt = 5% Dilution ◦ Stopping dilution grade is calculated by the interrogating a 2m hanging wall dilution shell, offset adjacent to the stope shape, against the resource model.

Criteria	JORC Code Explanation	Commentary
	<p>mining studies and the sensitivity of the outcome to their inclusion.</p> <ul style="list-style-type: none"> The infrastructure requirements of the selected mining methods. 	<ul style="list-style-type: none"> Mining recovery is 100% for development and 95% for stopes
Metallurgical factors or assumptions	<ul style="list-style-type: none"> The metallurgical process proposed and the appropriateness of that process to the style of mineralisation. Whether the metallurgical process is well-tested technology or novel in nature. The nature, amount and representativeness of metallurgical test work undertaken, The nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied. Any assumptions or allowances made for deleterious elements. The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole. For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications? 	<ul style="list-style-type: none"> An expansion to the Century concentrator will be required to treat the Silver King ore separately to but concurrently with the existing tailings reprocessing operation. A new crushing and milling circuit is required, with a combination of new and floatation and product handling equipment being reconfigured to treat the Silver King ore. Zinc tailings from the lead circuit will be combined with the current tailings processing streams. Three PQ holes were drilled for the purpose of metallurgical test work. The diameter provided by the PQ core was selected to provide a larger sample mass of ~14 kg/m. The holes were designed for oblique intersection to increase the mass of mineralisation available for test work. The core utilised for metallurgical test work is representative of the mineralisation style of the deposit. The core was divided into shale hosted mineralisation and sandstone hosted mineralisation and split into composites using a rotary sample divider.  <p>SK21 MET holes in relation to SK21 ResDef holes</p> <ul style="list-style-type: none"> Metallurgical test work holes shown in blue in the figure above. Metallurgical test work results were analysed and interpreted by New Century Resources site-based metallurgists and Life of Mine plan recoveries estimated. A risk exists associated with carbonaceous hanging wall material; H4r, a carbonaceous shale unit contains appreciable levels of organic carbon and will be a dilution source. This will be managed on site at Century via a carbon pre-float. Conservative metallurgical recoveries to payable concentrate of 50% of Zn, 84% of Pb and 70% of Ag grades
Environmental	<ul style="list-style-type: none"> The status of studies of potential environmental impacts of the mining and processing operation. Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, <ul style="list-style-type: none"> the status of approvals for process residue storage and waste dumps should be reported. 	<ul style="list-style-type: none"> An Environmental Authority amendment is required before operations can commence. It is expected that approval will be granted in the timeframes required by the mine plan and that there is a reasonable basis to expect the approvals will be granted. Waste rock is planned to be stored temporarily on a conventional waste rock dump adjacent to the Silver King portal. All waste rock generated by the Silver King mine, with the exception of a small quantity of highly weathered and inert material generated near the surface, which will be unsuitable for use as backfill, will be transported back underground for use as backfill within than two years of the commencement of mining. The mine plan is waste deficient and will require waste to be sourced from other surface waste rock dump sources for use as backfill, contributing further to site rehabilitation.
Infrastructure	<ul style="list-style-type: none"> The existence of appropriate infrastructure: <ul style="list-style-type: none"> availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the 	<ul style="list-style-type: none"> Concentrate transportation and handling infrastructure existing between Century Mine and Karumba port, including the MV Wumna transport vessel, will be utilised for the handling of both lead and zinc concentrates from the Silver King mine. Costs associated with this are well understood. Existing camp infrastructure will be utilised for accommodating FIFO personnel, with some minor refurbishment works required.

Criteria	JORC Code Explanation	Commentary
	<i>infrastructure can be provided, or accessed.</i>	<ul style="list-style-type: none"> Hire diesel generators are planned to be located at Silver King mine for the purpose of supplying the full electricity needs of the operation. Clean water feed lines will be run from existing nearby Century infrastructure to the Silver King mine. Processing infrastructure will be constructed at existing Century open pit ROM and disused reclaim stockpile locations. Mine offices and workshops will be reclaimed from various locations around Century Mine site. Explosives magazines, a concrete batch plant, bath houses and sewerage treatment infrastructure will be acquired externally and constructed at the Silver King mine site. Existing site roads to the Silver King mine site are sufficient for commencement of mining operations. Minor upgrades will be completed to improve haulage efficiencies prior to the commencement of Ore haulage to the processing facility. Tailings will be pumped into the Century Open Pit via an existing line presently utilised for the tailings resulting from the reprocessing of the tailings dam material.
Costs	<ul style="list-style-type: none"> <i>The derivation of, or assumptions made, regarding projected capital costs in the study.</i> <i>The methodology used to estimate operating costs.</i> <i>Allowances made for the content of deleterious elements.</i> <i>The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co- products.</i> <i>The source of exchange rates used in the study.</i> <i>Derivation of transportation charges.</i> <i>The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.</i> <ul style="list-style-type: none"> <i>The allowances made for royalties payable, both Government and private.</i> 	<ul style="list-style-type: none"> Capital costs include site infrastructure construction, underground mine infrastructure and permanent (LOM) development, and underground operational readiness costs. A processing plant upgrade has been designed and estimated by GR Engineering Services to support a feasibility study estimate for the capital and operating costs associated with treating in situ ores concurrently with tailings reprocessing operations. Capital costs of processing infrastructure upgrades have been proportioned to Silver King and East Fault Block ores based on processed tonnage. Underground mining costs are well understood as they are derived from unit rates for salaries, wages, ground support, drilling and blasting, ventilation, services, diesel, and equipment hire and maintenance. The operational cost estimate is a first principles approach. A majority of the cost drivers in the Silver King mine plan have been broken down to the smallest practical unit for estimation. Unit consumptions have been estimated from individual tasks and budgeted pricing sought from suppliers for input into the schedule so far as practical. Pipeline, transportation, treatment and refining costs are well understood from actual costs incurred in the processing, handling and treatment of tailings material at Century Mine. Exchange rate used is 0.74 AUD/USD. The Queensland Government royalty of 3.9% for zinc, 4.8% for lead and 5.0% for silver have been applied to the gross value of each metal minus allowable deductions for ocean freight and metal playability deductions. A private royalty of 2% of NSR has been applied. Treatment charges of USD \$180 per zinc concentrate tonne, USD \$175 per lead concentrate tonne and shipping charges of USD \$50 per wet metric tonne of concentrate have been applied. No allowances have been made for deleterious elements. Two concentrate products will be produced. There will be zinc losses to lead concentrate and lead losses to zinc concentrate during transportation via the pipeline. No revenue or penalties have been assumed for the lead present in zinc concentrate nor the zinc present in lead concentrate. Cost estimates for overhead expenses including G&A, flights and accommodation were derived from current budget forecasts for Century Mine.
Revenue factors	<ul style="list-style-type: none"> <i>The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and</i> 	<ul style="list-style-type: none"> Revenue is calculated using a Net Smelter Return (NSR) formula applied to mining shapes due to the multiple revenue streams available from contributing elements (zinc, lead, silver). The NSR calculation estimates the value of the ore by subtracting estimated shipping costs, treatment charges, royalties and selling

Criteria	JORC Code Explanation	Commentary
	<p><i>treatment charges, penalties, net smelter returns, etc.</i></p> <ul style="list-style-type: none"> <i>The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.</i> 	<p>costs from the gross value of the recovered metal in the ore. A mining shape is included in the mine plan if the NSR exceeds the combined estimated mining and processing cost.</p> <ul style="list-style-type: none"> Reserve model revenue is based on an assumption of: <ul style="list-style-type: none"> Zinc USD \$2450/t Lead USD \$1730/t Silver USD \$22/oz Exchange Rate 0.74 AUD/USD
Market Assessment	<ul style="list-style-type: none"> <i>The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.</i> <i>A customer and competitor analysis along with the identification of likely market windows for the product.</i> <i>Price and volume forecasts and the basis for these forecasts.</i> <p><i>For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.</i></p>	<ul style="list-style-type: none"> Century has successfully sold zinc concentrates into the domestic and export markets since restart in 2018. Concentrate grades are estimated to be 48% zinc and are sold under both contracted and spot terms. Lead concentrate grades are estimated to be 65% lead in concentrate and are expected to be saleable into the export market. The volumes of lead produced from Silver King is not expected to impact the market price and the high concentrate grades are expected to be attractive to customers. Silver is payable in both lead and zinc concentrate sales agreements.
Economic	<ul style="list-style-type: none"> <i>The inputs to the economic analysis to produce the net present value (NPV) in the study,</i> <i>The source and confidence of these economic inputs including estimated inflation, discount rate, etc.</i> <i>NPV ranges and sensitivity to variations in the significant assumptions and inputs.</i> 	<ul style="list-style-type: none"> The Silver King Ore Reserve demonstrates a positive NPV. The Ore Reserve estimate has been evaluated through the site's life of mine planning financial model, combined with the Century tailings operation, and has been defined as economic. All operating and capital costs as well as revenue factors are included in the financial model. The Silver King Underground Ore Reserve is dependent on the continuation of Century tailings reprocessing operations. At the time of reporting, the Ore Reserve from the Century tailings operation will continue to be processed beyond the Silver King Underground Ore Reserve, based on a scheduled commencement of May 2022.
Social	<ul style="list-style-type: none"> <i>The status of agreements with key stakeholders and matters leading to social license to operate.</i> 	<ul style="list-style-type: none"> The Century Mining tenements ML90045 and ML90058 are subject to the Gulf Communities Agreement (GCA) which was negotiated between Pasminco, the Queensland Government and four native title groups - the Waanyi, the Mingginda, the Gkuthaarn and the Kukatj, under the right to negotiate provisions contained within the Native Title Act of 1993 (Commonwealth). The native title rights and interests associated with the Transport Infrastructure Corridor for the Pipeline and the Karumba Port Facility were acquired by the State of Queensland and Operational Licences were granted to Century Mining Limited. The consent from the relevant native title holders for the grant of the Operational Licence (and other grants) is contained in the GCA.
Other	<ul style="list-style-type: none"> <i>To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:</i> <i>Any identified material naturally occurring risks.</i> <i>The status of material legal agreements and marketing arrangements.</i> <i>The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals.</i> <i>There must be reasonable grounds to expect that all</i> 	<ul style="list-style-type: none"> All proposed mining activities are entirely within Century Mining Limited's existing Mining Lease ML90045.

Criteria	JORC Code Explanation	Commentary
	<p>necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.</p>	
Classification	<ul style="list-style-type: none"> The basis for the classification of the Ore Reserves into varying confidence categories. Whether the result appropriately reflects the Competent Person's view of the deposit. <p>The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).</p>	<ul style="list-style-type: none"> The Ore Reserve Estimate is based on the 2021 Silver King Mineral Resource Estimate (MRE). Measured and Indicated Resources become Probable Reserves based on majority percentage of MRE tonnes within an economically positive mining shape, provided an aggregation of these shapes supports the establishment of relevant underground capital infrastructure required for their extraction. Stopes where a majority of the contained MRE tonnage is Measured + Indicated Resource are classified as Probable Ore Reserves. Measured material has been withheld from conversion to a Proven reserve, instead being converted to a Probable Reserve due to uncertainties associated with some of the Modifying Factors which are considered in the economic assessment of the Ore Reserve, such as global estimates for stope dilution. It is the competent person's view that the classifications used for the Ore Reserve Estimate are appropriate. Approximately 0.53 Mt of Measured tonnes have been converted to a Probable Reserve. This accounts for 30% of the Reserve estimate. Material below the resource cut-off grade of 4% Combined Pb and Zn has been flagged as 'unclassified' material in the block model. This material is otherwise estimated in the same manner to indicated and measured resources. As such it has been included as internal dilution within the reserve mining shapes. An example of this is demonstrated below, with the resource model shown with combined Pb and Zn grades and the block resource category within reserve stoping and development shapes.  <p>Combined Pb + Zn grade and Block Model Resource Classification</p> <ul style="list-style-type: none"> The metal content of mineralised waste material within the resource model is negligible in the assessment of whether a

Criteria	JORC Code Explanation	Commentary
		mining shape is included in the Ore Reserve. Iterations of the mining schedule were conducted with this material tonnage accounted for but estimated at zero grade, with negligible impact on the mined tonnes observed.
Audits or reviews	<ul style="list-style-type: none"> The results of any audits or reviews of Ore Reserve estimates. 	<ul style="list-style-type: none"> No external audit of this Ore Reserve Estimate has been completed to date.
Discussion of relative accuracy/confidence	<ul style="list-style-type: none"> Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate. The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used. Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage. It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available. 	<ul style="list-style-type: none"> The Ore Reserve Estimate is determined by the order of accuracy associated with the Mineral Resource model, the metallurgical inputs and the cost adjustment factors used. Confidence of the inputs is considered to be typical of industry standard feasibility study assessments.

Silver King Open Pit

Section 4: Reporting of Reserves

Criteria	JORC Code Explanation	Commentary
Mineral Resource Estimate for conversion to Ore Reserves	<ul style="list-style-type: none"> Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve. Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves. 	<ul style="list-style-type: none"> The Silver King (SK) open pit Ore Reserve is based on the Mineral Resource estimate carried out by New Century Resources in 2021. The Mineral Resource Model used in this estimate is referred to as SK_OP_v4.dm. Mineral Resources are reported inclusive of the Ore Reserves. The Ore Reserve has been declared at the point where ore is delivered to the run of mine pad.
Site visits	<ul style="list-style-type: none"> Comment on any site visits undertaken by the Competent Person and the outcome of those visits. If no site visits have been undertaken indicate why this is 	<ul style="list-style-type: none"> The Competent Person is employed full time by New Century Resources, working on site at Century Mine, Lawn Hill, QLD.

Criteria	JORC Code Explanation	Commentary
	<i>the case.</i>	
Study Status	<ul style="list-style-type: none"> <i>The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.</i> <i>The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.</i> 	<ul style="list-style-type: none"> The level of study undertaken to enable the Mineral Resources to be converted to Ore Reserves is representative of a Feasibility Study and comprises of mining, infrastructure and process designs completed with sufficient rigour to serve as the basis of an investment decision, as defined in the JORC Code 2012. Ore Reserves have been calculated within detailed pit designs. A series of nested optimised pit shells were generated using Deswik software, an analysis of the shells was completed to identify the preferred shell. The detailed pit design follows the preferred pit shell as close as practical. A detailed mine plan has been developed, which is economically viable and technically achievable, and appropriate ore dilution and recoveries have been applied to the Mineral Resource model. The Silver King open pit mine plan exists wholly within a current Mining Lease and necessary amendments to approvals to allow for open pit mining are expected to be approved by the relevant government departments within the specified project time frame. In the opinion of the Competent Person there are no reasonable grounds that statutory approvals will not be granted in the timeframes outlined in studies.
Cut-off parameters	<ul style="list-style-type: none"> <i>The basis of the cut-off grade(s) or quality parameters applied.</i> 	<ul style="list-style-type: none"> Cut off parameters were estimated using the Net Smelter Return (NSR) calculation which has been applied to the reserve model. The NSR calculation estimates the value of the ore by subtracting estimated shipping costs, treatment charges, transportation costs, royalties and selling costs from the gross value of the recovered metal in the ore. A mining shape is included in the mine plan if the NSR exceeds the processing cost and the mining shape is within the pit design. The pit design (based on a pit optimisation process) was used to determine the incremental and combined impact of mining and processing costs and revenues to determine if a block would be included in the pit design. The Cut-off NSR was based off a Life of Mine (LOM) financial model for the combined in situ and tailings reprocessing operation. Inputs to the calculation of cut-off grade include mining costs, processing costs, metallurgical recoveries, transportation costs, pipeline, shipping, treatment and refining costs, general and administrative costs, royalties and metal prices. Cut-off grades are based on an assumption of: <ul style="list-style-type: none"> Zinc USD \$2,450/t Lead USD \$1,730/t Silver USD \$22/Oz Exchange Rate 0.74 AUD/USD The cut-off grade used for reporting purposes for the Silver King open pit Ore Reserve Estimate is based on a NSR greater than AUD \$38/t.
Mining factors or assumptions	<ul style="list-style-type: none"> <i>The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).</i> <i>The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.</i> <i>The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.</i> 	<ul style="list-style-type: none"> Ore Reserves were estimated through a standard mine planning process which included pit optimisation, mine design, mine scheduling and financial modelling. Mining factors and assumptions have been based on technical estimates, first principles calculations, benchmarking exercises. The Silver King open pit deposit is planned to be exploited by via conventional truck and excavator fleet mining techniques to extract ore to a local Silver King ROM and waste material to the waste rock dumps. Ore will be selectively mined to geological controlled grade boundaries over a 5m and 10m design bench height. An ore mining loss of 4% and a dilution factor of 9% have been applied which were estimated through a process of applying a dilution skin to the orebody. External and internal geotechnical studies were carried out to evaluate the operational designs and slope parameters were applied to the pit optimization and subsequent detailed pit designs. A minimum mining width of 25m is applied to the final mine design and is considered appropriate for the primary mining fleet of a 200t excavator and 170t rigid haul trucks.

Criteria	JORC Code Explanation	Commentary
	<ul style="list-style-type: none"> <i>The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).</i> <i>The mining dilution factors used</i> <i>The mining recovery factors used</i> <i>Any minimum mining widths used</i> <i>The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.</i> <i>The infrastructure requirements of the selected mining methods.</i> 	<ul style="list-style-type: none"> Inferred material is excluded from the Ore Reserve and treated as waste material, which incurs a mining cost but is not processed and does not generate revenue. Significant infrastructure is already in place to support the ore reserve and future mine plan due to the operating nature of the current site, however some minor capital investment is required.
Metallurgical factors or assumptions	<ul style="list-style-type: none"> <i>The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.</i> <i>Whether the metallurgical process is well-tested technology or novel in nature.</i> <i>The nature, amount and representativeness of metallurgical test work undertaken,</i> <i>The nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.</i> <i>Any assumptions or allowances made for deleterious elements.</i> <i>The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.</i> <i>For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?</i> 	<ul style="list-style-type: none"> An expansion to the Century concentrator will be required to treat the Silver King ore separately to but concurrently with the existing tailings reprocessing operation. New crushing and grinding circuits are required, with a combination of new and disused floatation and product handling equipment being reconfigured to treat the Silver King ore. Zinc tailings from the lead circuit will be combined with the current tailings processing streams. The ore is classified in two different categories: oxidised and fresh ore. The oxidised ore accounts for the shallower lying material with lower recoveries compared to the deeper fresh ore. Recoveries in line with the testwork were used. No allowances are made for deleterious elements.
Environmental	<ul style="list-style-type: none"> <i>The status of studies of potential environmental impacts of the mining and processing operation.</i> <i>Details of waste rock characterisation and</i> <i>the consideration of potential sites, status of design options considered and, where applicable,</i> <i>the status of approvals for process residue storage and waste dumps should be reported.</i> 	<ul style="list-style-type: none"> An Environmental Authority amendment is required before open pit operations can commence. It is expected that approval will be granted in the timeframes required by the mine plan and that there is a reasonable basis to expect the approvals will be granted. All waste rock material is considered as Potential Acid Forming (PAF) material. An extension of the Western Waste Rock Dump (WRD) is designed and is planned to be used to store waste materials. Environmental rehabilitation plans are produced and costs for the mine closure rehabilitation work is accounted for in the life of mine financial model.
Infrastructure	<ul style="list-style-type: none"> <i>The existence of appropriate infrastructure:</i> <i>availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour,</i> 	<ul style="list-style-type: none"> Infrastructure required for the proposed project has been accounted for and included in the capital improvement and operational schedules which form the basis of Reserve Estimate. Due to the previous open pit mining activities and current tailings reprocessing operations, most of the infrastructure required to

Criteria	JORC Code Explanation	Commentary
	<i>accommodation; or the ease with which the infrastructure can be provided, or accessed.</i>	<p>support the future planned mining operations is in place albeit requiring some refurbishment.</p> <ul style="list-style-type: none"> Existing site roads to the Silver King mine site are sufficient for commencement of mining operations. Minor upgrades will be completed to improve haulage efficiencies prior to the commencement of ore haulage to the processing facility. Mine offices will be reclaimed from various locations around Century Mine site and installed as required to support the proposed operation. Additionally, a heavy vehicle workshop, explosive's magazines, dewatering infrastructure, crib huts, bath houses and sewerage treatment infrastructure will be acquired externally and constructed at the Silver King mine site. Tailings will be pumped into the historic century open pit via an existing line presently utilised for the tailings resulting from the reprocessing of the tailings dam material. Existing camp and airport infrastructure will be utilised for accommodating FIFO personnel, with some minor refurbishment works required.
Costs	<ul style="list-style-type: none"> <i>The derivation of, or assumptions made, regarding projected capital costs in the study.</i> <i>The methodology used to estimate operating costs.</i> <i>Allowances made for the content of deleterious elements.</i> <i>The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co- products.</i> <i>The source of exchange rates used in the study.</i> <i>Derivation of transportation charges.</i> <i>The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.</i> <i>The allowances made for royalties payable, both Government and private.</i> 	<ul style="list-style-type: none"> A processing plant upgrade has been designed and estimated by GR Engineering Services to support a feasibility study estimate for the capital and operating costs associated with treating in situ ores concurrently with tailings reprocessing operations. The Silver King open pit capital costs consist mainly of mobile equipment refurbishment, site infrastructure and plant upgrade costs. The mobile mining equipment refurbishment costs have been determined based on contractor quotes. Capital costs are based on supplied quotes and haven been included in the economic cost model. Capital and overhead costs have been apportioned between the in-situ deposit (Silver King Underground & Open Pit and East Fault Block Open Pit) ores based on processed tonnage. The Silver King open pit operating costs are based on the detailed mine plan and are broken down to the smallest practical unit for estimation. Unit costs and consumption rates have been estimated from individual tasks, first principles and budgeted pricing sought from suppliers and mining contractors. Pipeline, transportation, treatment and refining costs are well understood from actual costs incurred in the processing, handling and treatment of tailings material at Century Mine. Exchange rate used is 0.74 AUD/USD. The Queensland Government royalty of 3.9% for zinc, 4.8% for lead and 5.0% for silver have been applied to the gross value of each metal minus allowable deductions for ocean freight and metal playability deductions. A private royalty of 2% of NSR has been applied. Treatment charges of USD \$180 per zinc concentrate tonne, USD \$175 per lead concentrate tonne and shipping charges of USD \$50 per wet metric tonne concentrate have been applied. No allowances have been made for deleterious elements. Two concentrate products will be produced. There will be zinc losses to lead concentrate and lead losses to zinc concentrate during transportation via the pipeline. No revenue or penalties have been assumed for the lead present in zinc concentrate nor the zinc present in lead concentrate. Cost estimates for overhead expenses including G&A, flights and accommodation were derived from current budget forecasts for Century Mine.
Revenue factors	<ul style="list-style-type: none"> <i>The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc</i> <i>The derivation of assumptions</i> 	<ul style="list-style-type: none"> Commodity price assumptions are based on New Century Resources' assessment of Consensus Economics data using a zinc price of USD \$2,450/t, lead price of USD \$1,730/t, a silver price of USD \$22/oz and an exchange rate of 0.74 AUD/USD to calculate the revenue. Revenue is calculated using a Net Smelter Return (NSR) formula applied to mining shapes due to the multiple revenue streams available from contributing metals (zinc, lead, silver). The NSR calculation estimates the value of the ore by subtracting

Criteria	JORC Code Explanation	Commentary
	<i>made of metal or commodity price(s), for the principal metals, minerals and co-products.</i>	estimated shipping costs, treatment charges, royalties and selling costs from the gross value of the recovered metal in the ore.
Market Assessment	<ul style="list-style-type: none"> <i>The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.</i> <i>A customer and competitor analysis along with the identification of likely market windows for the product.</i> <i>Price and volume forecasts and the basis for these forecasts.</i> <i>For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.</i> 	<ul style="list-style-type: none"> Century mine has produced and sold zinc concentrates into the domestic and export markets since restart in 2018. Concentrate grades are estimated to be 48% zinc and are sold under both contracted and spot terms. Lead concentrate grades are estimated to be 65% lead in concentrate and are expected to be saleable into the export market. The volume of lead produced from Silver King is not expected to impact the market price and the high concentrate grades are expected to be attractive to customers. Silver is expected to be payable in both lead and zinc concentrate sales agreements.
Economic	<ul style="list-style-type: none"> <i>The inputs to the economic analysis to produce the net present value (NPV) in the study,</i> <i>The source and confidence of these economic inputs including estimated inflation, discount rate, etc</i> <i>NPV ranges and sensitivity to variations in the significant assumptions and inputs.</i> 	<ul style="list-style-type: none"> The Ore Reserve estimate has been evaluated and through the site's life of mine planning financial model, showing that the Silver King open pit operation is economic. All operating and capital costs as well as revenue factors are included in the financial model. This process has demonstrated that the Ore Reserve for the Silver King open pit has a positive NPV. The Silver King Open Pit Ore Reserve Estimate is dependent on the continuation of Century tailings reprocessing operations and the processing of the Silver King Underground ore reserve. At the time of reporting, the Ore Reserve from the Century tailings operation will continue to be processed beyond the in situ mining Ore Reserve, based on a scheduled commencement of in situ operations in May 2022.
Social	<ul style="list-style-type: none"> <i>The status of agreements with key stakeholders and matters leading to social license to operate.</i> 	<ul style="list-style-type: none"> The Century Mining tenements ML90045 and ML90058 are subject to the Gulf Communities Agreement (GCA) which was negotiated between Pasminco, the Queensland Government and four native title groups - the Waanyi, the Mingginda, the Gkuthaarn and the Kukatj, under the right to negotiate provisions contained within the Native Title Act of 1993 (Commonwealth). The native title rights and interests associated with the Transport Infrastructure Corridor for the Pipeline and the Karumba Port Facility were acquired by the State of Queensland and Operational Licences was granted to Century Mining Limited. The consent from the relevant native title holders for the grant of the Operational Licence (and other grants) is contained in the GCA.
Other	<ul style="list-style-type: none"> <i>To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:</i> <i>Any identified material naturally occurring risks.</i> <i>The status of material legal agreements and marketing arrangements.</i> <i>The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals.</i> <i>There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-</i> 	<ul style="list-style-type: none"> There are typical risks for an open pit operation such as heavy rain fall events and geotechnical risks. These risks are managed through the implementation of various risk management mechanisms as far as practical.

Criteria	JORC Code Explanation	Commentary
	<i>Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.</i>	
Classification	<ul style="list-style-type: none"> • <i>The basis for the classification of the Ore Reserves into varying confidence categories.</i> • <i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i> • <i>The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).</i> 	<ul style="list-style-type: none"> • The Ore Reserve Estimate has been prepared in accordance with the guidelines of the JORC Code, 2012 and is based on the 2021 Silver King Mineral Resource Estimate. • The Ore Reserves are entirely derived from Indicated and Measured Resources. This classification is based on the density of drilling, the orebody and technical estimates pertaining to the mining method employed. In total 59% of the Ore Reserves are derived from Indicated Resources and 41% from Measured Resources. All Ore Reserves are categorized as Probable Reserves, because of the uncertainties in the modifying factors. • It is the Competent Person's view that the classification applied to the Ore Reserves is appropriate.
Audits or reviews	<ul style="list-style-type: none"> • <i>The results of any audits or reviews of Ore Reserve estimates.</i> 	<ul style="list-style-type: none"> • No external audit of this Ore Reserve Estimate has been done to date.
Discussion of relative accuracy/confidence	<ul style="list-style-type: none"> • <i>Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.</i> • <i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i> • <i>Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.</i> • <i>It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i> 	<ul style="list-style-type: none"> • The accuracy of the Ore Reserve estimate is directly influenced by the order of accuracy associated with the Mineral Resource model, the metallurgical input and the long-term costs and the revenue assumptions applied. • Confidence of the inputs is considered to be typical of industry standard feasibility study assessments.

East Fault Block Open Pit

Section 4: Reporting of Reserves

Criteria	JORC Code Explanation	Commentary
Mineral Resource Estimate for conversion to Ore Reserves	<ul style="list-style-type: none"> <i>Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.</i> <i>Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.</i> 	<ul style="list-style-type: none"> The East Fault Block (EFB) open pit Ore Reserve is based on the Mineral Resource estimate carried out by New Century Resources in 2021. The Mineral Resource Model used in this estimate is referred to as MIN_RES_EFB2017_rotated.bmf Mineral Resources are reported inclusive of the Ore Reserves. The Ore Reserve has been declared at the point where ore is delivered to the run of mine pad.
Site visits	<ul style="list-style-type: none"> <i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i> <i>If no site visits have been undertaken indicate why this is the case.</i> 	<ul style="list-style-type: none"> The Competent Person is employed full time by New Century Resources, working on site at Century Mine, Lawn Hill, QLD.
Study Status	<ul style="list-style-type: none"> <i>The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.</i> <i>The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.</i> 	<ul style="list-style-type: none"> The level of study undertaken to enable the Mineral Resources to be converted to Ore Reserves is representative of a Feasibility Study and comprises of mining, infrastructure and process designs completed with sufficient rigour to serve as the basis of an investment decision, as defined in the JORC Code 2012. Ore Reserves have been calculated within detailed pit designs. A series of nested optimised pit shells were generated using Deswik software, an analysis of the shells was completed to identify the preferred shell. The detailed pit design follows the preferred pit shell as close as practical. A detailed mine plan has been developed, which is economically viable and technically achievable, and appropriate ore dilution and recoveries have been applied to the Mineral Resource model. The East Fault Block open pit mine plan exists wholly within a current Mining Lease and necessary amendments to approvals to allow for open pit mining are expected to be approved by the relevant government departments within the specified project time frame. In the opinion of the Competent Person there are no reasonable grounds that statutory approvals will not be granted in the timeframes outlined in studies.
Cut-off parameters	<ul style="list-style-type: none"> <i>The basis of the cut-off grade(s) or quality parameters applied.</i> 	<ul style="list-style-type: none"> Cut off parameters were estimated using the Net Smelter Return (NSR) calculation which has been applied to the reserve model. The NSR calculation estimates the value of the ore by subtracting estimated shipping costs, treatment charges, transportation costs, royalties and selling costs from the gross value of the recovered metal in the ore. An ore mining shape is included in the mine plan if the NSR exceeds the processing cost, and the mining shape is within the pit design. The pit design (based on a pit optimisation process) was used to determine the incremental and combined impact of mining and processing costs and revenues to determine if a block would be included in the pit design. The Cut-off NSR was based off a Life of Mine (LOM) financial model for the combined in-situ and tailings reprocessing operation. Inputs to the calculation of cut-off grade include mining costs, processing costs, metallurgical recoveries, transportation costs, pipeline, shipping, treatment and refining costs, general and administrative costs, royalties and metal prices. Cut-off grades are based on an assumption of: <ul style="list-style-type: none"> Zinc USD \$2,450/t Lead USD \$1,730/t Silver USD \$22/Oz Exchange Rate 0.74 AUD/USD The cut-off parameter used for reporting purposes for the East Fault Block open pit Ore Reserve Estimate is based on a NSR greater than AUD \$38 /t.

Criteria	JORC Code Explanation	Commentary
Mining factors or assumptions	<ul style="list-style-type: none"> <i>The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).</i> <i>The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.</i> <i>The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.</i> <i>The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).</i> <i>The mining dilution factors used.</i> <i>The mining recovery factors used.</i> <i>Any minimum mining widths used.</i> <i>The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.</i> <i>The infrastructure requirements of the selected mining methods.</i> 	<ul style="list-style-type: none"> Ore Reserves were estimated through a standard mine planning process which included pit optimisation, mine design, mine scheduling and financial modelling. Mining factors and assumptions have been based on technical estimates, first principles calculations, benchmarking exercises. The East Fault Block open pit deposit is planned to be exploited by via conventional truck and excavator fleet mining techniques to extract ore to the Century ROM and waste material to the North and in-pit waste rock dumps. Ore will be selectively mined to geological controlled grade boundaries over a 6m and 12m design bench height. An ore mining loss of 3% and a dilution factor of 11% have been applied which were estimated through a process of applying a dilution skin to the orebody. External and internal geotechnical studies were carried out to evaluate the operational designs and slope parameters were applied to the pit optimization and subsequent detailed pit designs. A minimum mining width of 25m is applied to the final mine design and is considered appropriate for the primary mining fleet of a 200t excavator and 170t rigid haul trucks. Inferred material is excluded from the Ore Reserve and treated as waste material, which incurs a mining cost but is not processed and does not generate revenue. Significant infrastructure is already in place to support the ore reserve and future mine plan due to the operating nature of the current site, however some minor capital investment is required.
Metallurgical factors or assumptions	<ul style="list-style-type: none"> <i>The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.</i> <i>Whether the metallurgical process is well-tested technology or novel in nature.</i> <i>The nature, amount and representativeness of metallurgical test work undertaken,</i> <i>The nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.</i> <i>Any assumptions or allowances made for deleterious elements.</i> <i>The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.</i> <i>For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?</i> 	<ul style="list-style-type: none"> An expansion to the Century concentrator will be required to treat the East Fault Block ore separately to but concurrently with the existing tailings reprocessing operation. New crushing and grinding circuits are required, with a combination of new and disused floatation and product handling equipment being reconfigured to treat the East Fault Block ore. Zinc tailings from the lead circuit will be combined with the current tailings processing streams. Estimated average recoveries used in the estimation of the ore reserves are 60% lead, 70% zinc, 35% silver in zinc concentrate and 35% silver in lead concentrate. No allowances are made for deleterious elements.

Criteria	JORC Code Explanation	Commentary
Environmental	<ul style="list-style-type: none"> <i>The status of studies of potential environmental impacts of the mining and processing operation.</i> <i>Details of waste rock characterisation and</i> <i>the consideration of potential sites, status of design options considered and, where applicable,</i> <i>the status of approvals for process residue storage and waste dumps should be reported.</i> 	<ul style="list-style-type: none"> The EFB pit is part of cutback of the historic century pit. To recommence mining operations an Environmental Authority amendment is required. It is expected that approval will be granted in the timeframes required by the mine plan and that there is a reasonable basis to expect the approvals will be granted. The waste rock is categorized in PAF and NAF material. A small amount of PAF is planned to be dumped on the North WRD's to finalize its PAF design requirements. The remaining PAF is planned to be dumped on in-pit dumps within the historic century pit. One third of the mined material is NAF, which will be utilized as capping material contributing to the rehabilitation of the North waste rock dump. Environmental rehabilitation plans have been produced and costs for the mine closure rehabilitation work is accounted for in the financial evaluation model.
Infrastructure	<ul style="list-style-type: none"> <i>The existence of appropriate infrastructure:</i> <i>availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.</i> 	<ul style="list-style-type: none"> Infrastructure required for the proposed project has been accounted for and included in the capital improvement and operational schedules which form the basis of Reserve Estimate. Due to the previous open pit mining activities and current tailings reprocessing operations, most of the infrastructure required to support the future planned mining operations is in place albeit requiring some refurbishment. Existing site roads to the East Fault Block site are sufficient for commencement of mining operations. Minor upgrades will be completed to improve haulage efficiencies prior to the commencement of ore haulage to the processing facility. Mine offices will be reclaimed from various locations around Century Mine site and installed as required to support the proposed operation. Additionally, a heavy vehicle workshop, explosive's magazines, dewatering infrastructure, crib huts, bath houses and sewerage treatment infrastructure will be acquired externally and constructed as required. Tailings will be pumped into the historic century open pit via an existing line presently utilised for the tailings resulting from the reprocessing of the tailings dam material. Existing camp and airport infrastructure will be utilised for accommodating FIFO personnel, with some minor refurbishment works required.
Costs	<ul style="list-style-type: none"> <i>The derivation of, or assumptions made, regarding projected capital costs in the study.</i> <i>The methodology used to estimate operating costs.</i> <i>Allowances made for the content of deleterious elements.</i> <i>The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co- products.</i> <i>The source of exchange rates used in the study.</i> <i>Derivation of transportation charges.</i> <i>The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.</i> <i>The allowances made for royalties payable, both Government and private.</i> 	<ul style="list-style-type: none"> A processing plant upgrade has been designed and estimated by GR Engineering Services to support a feasibility study estimate for the capital and operating costs associated with treating in situ ores concurrently with tailings reprocessing operations. The East Fault Block open pit capital costs consist mainly of mobile equipment refurbishment, site infrastructure and plant upgrade costs. The mobile mining equipment refurbishment costs have been determined based on contractor quotes. Capital costs are based on supplied quotes and haven been included in the economic cost model. Capital and overhead costs have been apportioned between the in-situ deposit (Silver King Underground & Open Pit and East Fault Block Open Pit) ores based on processed tonnage. The East Fault Block open pit operating costs are based on the detailed mine plan and are broken down to the smallest practical unit for estimation. Unit costs and consumption rates have been estimated from individual tasks, first principles and budgeted pricing sought from suppliers and mining contractors. Pipeline, transportation, treatment and refining costs are well understood from actual costs incurred in the processing, handling and treatment of tailings material at Century Mine. Exchange rate used is 0.74 AUD/USD. The Queensland Government royalty of 3.9% for zinc, 4.8% for lead and 5.0% for silver have been applied to the gross value of each metal minus allowable deductions for ocean freight and metal playability deductions. A private royalty of 2% of NSR has been applied.

Criteria	JORC Code Explanation	Commentary
		<ul style="list-style-type: none"> Treatment charges of USD \$180 per zinc concentrate tonne, USD \$175 per lead concentrate tonne and shipping charges of USD \$50 per wet metric tonne concentrate have been applied. No allowances have been made for deleterious elements. Two concentrate products will be produced. There will be zinc losses to lead concentrate and lead losses to zinc concentrate during transportation via the pipeline. No revenue or penalties have been assumed for the lead present in zinc concentrate nor the zinc present in lead concentrate. Cost estimates for overhead expenses including G&A, flights and accommodation were derived from current budget forecasts for Century Mine.
Revenue factors	<ul style="list-style-type: none"> <i>The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc</i> <i>The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.</i> 	<ul style="list-style-type: none"> Commodity price assumptions are based on New Century Resources' assessment of Consensus Economics data using a zinc price of USD \$2,450/t, lead price of USD \$1,730/t, a silver price of USD \$22/oz and an exchange rate of 0.74 AUD/USD to calculate the revenue. Revenue is calculated using a Net Smelter Return (NSR) formula applied to mining shapes due to the multiple revenue streams available from contributing metals (zinc, lead, silver). The NSR calculation estimates the value of the ore by subtracting estimated shipping costs, treatment charges, royalties and selling costs from the gross value of the recovered metal in the ore.
Market Assessment	<ul style="list-style-type: none"> <i>The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.</i> <i>A customer and competitor analysis along with the identification of likely market windows for the product.</i> <i>Price and volume forecasts and the basis for these forecasts.</i> <i>For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.</i> 	<ul style="list-style-type: none"> Century mine has produced and sold zinc concentrates into the domestic and export markets since restart in 2018. Concentrate grades are estimated to be 48% zinc and are sold under both contracted and spot terms. Lead concentrate grades are estimated to be 65% lead in concentrate and are expected to be saleable into the export market. The volume of lead produced is not expected to impact the market price and the high concentrate grades are expected to be attractive to customers. Silver is expected to be payable in both lead and zinc concentrate sales agreements.
Economic	<ul style="list-style-type: none"> <i>The inputs to the economic analysis to produce the net present value (NPV) in the study,</i> <i>The source and confidence of these economic inputs including estimated inflation, discount rate, etc</i> <i>NPV ranges and sensitivity to variations in the significant assumptions and inputs.</i> 	<ul style="list-style-type: none"> The Ore Reserve estimate has been evaluated and through the site's life of mine planning financial model, showing that the East Fault Block open pit operation is economic. All operating and capital costs as well as revenue factors are included in the financial model. This process has demonstrated that the Ore Reserve for the East Fault Block open pit has a positive NPV. The East Fault Block Ore Reserve Estimate is dependent on the continuation of Century tailings reprocessing operations and the commencement of the Silver King Underground mine. At the time of reporting, the Ore Reserve from the Century tailings operation will continue to be processed beyond the in-situ mining Ore Reserve, based on a scheduled commencement of in situ operations in May 2022.
Social	<ul style="list-style-type: none"> <i>The status of agreements with key stakeholders and matters leading to social license to operate.</i> 	<ul style="list-style-type: none"> The Century Mining tenements ML90045 and ML90058 are subject to the Gulf Communities Agreement (GCA) which was negotiated between Pasminco, the Queensland Government and four native title groups - the Waanyi, the Mingginda, the Gkuthaarn and the Kukatj, under the right to negotiate provisions contained within the Native Title Act of 1993 (Commonwealth). The native title rights and interests associated with the Transport Infrastructure Corridor for the Pipeline and the Karumba Port Facility were acquired by the State of Queensland and Operational Licences was granted to Century Mining Limited. The consent from the relevant native title holders for the grant of the Operational Licence (and other grants) is contained in the GCA.

Criteria	JORC Code Explanation	Commentary
Other	<ul style="list-style-type: none"> <i>To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:</i> <i>Any identified material naturally occurring risks.</i> <i>The status of material legal agreements and marketing arrangements.</i> <i>The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals.</i> <i>There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.</i> 	<ul style="list-style-type: none"> There are typical risks for an open pit operation such as heavy rain fall events and geotechnical risks. These risks are managed through the implementation of various risk management mechanisms as far as practical.
Classification	<ul style="list-style-type: none"> <i>The basis for the classification of the Ore Reserves into varying confidence categories.</i> <i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i> <i>The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).</i> 	<ul style="list-style-type: none"> The Ore Reserve Estimate has been prepared in accordance with the guidelines of the JORC Code, 2012 and is based on the 2017 East Fault Block Mineral Resource Estimate. The Ore Reserves are entirely derived from Indicated Resources. This classification is based on the density of drilling, the orebody experience from the historic Century pit and the mining method employed. All Ore Reserves are categorized as Probable Reserves. It is the Competent Person's view that the classification applied to the Ore Reserves is appropriate.
Audits or reviews	<ul style="list-style-type: none"> <i>The results of any audits or reviews of Ore Reserve estimates.</i> 	<ul style="list-style-type: none"> No external audit of this Ore Reserve Estimate has been done to date.
Discussion of relative accuracy/confidence	<ul style="list-style-type: none"> <i>Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.</i> <i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions</i> 	<ul style="list-style-type: none"> The accuracy of the Ore Reserve estimate is directly influenced by the order of accuracy associated with the Mineral Resource model, the metallurgical input and the long-term costs and the revenue assumptions applied. Confidence of the inputs is considered to be typical of industry standard feasibility study assessments.

Criteria	JORC Code Explanation	Commentary
	<p><i>made and the procedures used.</i></p> <ul style="list-style-type: none"> <i>Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.</i> <i>It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i> 	

Century Tailings

Section 4: Reporting of Reserves

Criteria	JORC Code Explanation	Commentary
Mineral Resource Estimate for conversion to Ore Reserves	<ul style="list-style-type: none"> <i>Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.</i> <i>Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.</i> 	<ul style="list-style-type: none"> The Century tailings Ore Reserve conversion is based on the Mineral Resource estimate carried out by Optiro Pty Ltd in September 2017. The Mineral Resource Model used in this estimate is referred to as NCR_Production_model.bmf. Mineral Resources are reported inclusive of the Ore Reserves.
Site visits	<ul style="list-style-type: none"> <i>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</i> <p><i>If no site visits have been undertaken indicate why this is the case.</i></p>	<ul style="list-style-type: none"> The Competent Person is employed full time by New Century Resources, and works on site at Century Mine, Lawn Hill, QLD.
Study Status	<ul style="list-style-type: none"> <i>The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.</i> <i>The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.</i> 	<ul style="list-style-type: none"> The Century tailings reprocessing operations are established hydraulic mining operation which has been producing Zinc concentrates continuously since September 2018. The Ore Reserve estimate is based on demonstrated operational and operating cost performance and projected performance improvements and costs profiles. A detailed mine plan has been developed, which is economically viable and technically achievable, and appropriate ore dilution and recoveries have been applied to estimate the ore reserve.
Cut-off parameters	<ul style="list-style-type: none"> <i>The basis of the cut-off grade(s) or quality parameters applied.</i> 	<ul style="list-style-type: none"> Hydraulic mining at the Century tailings deposit does not allow for selective mining. All tailings material will be recovered and processed to generate a Zinc concentrate through the hydraulic mining process. A cut-off of AUD \$29 NSR has been calculated however due to the non-selective nature of the mining process, the cut-off was not used to constrain the Ore Reserve Estimate. A zinc price of USD \$2,450 and a Silver Price of USD \$22/Oz have been applied to determine the cut-off NSR.

Criteria	JORC Code Explanation	Commentary
Mining factors or assumptions	<ul style="list-style-type: none"> <i>The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).</i> <i>The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.</i> <i>The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.</i> <i>The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).</i> <i>The mining dilution factors used.</i> <i>The mining recovery factors used.</i> <i>Any minimum mining widths used.</i> <i>The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.</i> <i>The infrastructure requirements of the selected mining methods.</i> 	<ul style="list-style-type: none"> A detailed mining plan has been developed to convert the Mineral Resources to Ore Reserves in which mining shapes were created and scheduled accordingly to the resources available to achieve the target production rates. Mining factors and assumptions have been chosen based on historic site experience and forward projections based on the mine plan. Hydraulic mining of the Century tailings deposit is undertaken via top-down hydraulic mining method. Up to four active water cannons are located on top of the mining bench and use high pressure water to fluidise the tailings. The resultant slurry gravity feeds to a sump, in which multiple submersible pumps transfer the tailing to screen after which it is pumped to the Century concentrator. The mine plan has broken the deposit into 3 horizontal passes, with the hydraulic cannons working in strips and blocks with typical strip widths of 15-20 meters. The floor of the tailings facility will be cleaned up, utilising a combination of hydraulic mining, dozers and excavators. The current mining activities show the appropriateness of the method as the basis of the Ore Reserve. During the hydraulic mining process, a 300mm material layer will be left on the floor of the deposit, which is accounted as ore loss. Additionally, a dilution of 100mm at the bottom of the deposit for non-tailings material is applied to the resource model. This final layer including the 300mm of ore loss and 100mm of dilution will be removed in the final clean-up pass. A mining recovery of 95.5% has been assumed for all mining blocks removed with the hydraulic cannons which is based on the mine call factor estimated from monthly reconciliation data. Geotechnical studies have been carried out evaluate and continuously improve the operational design with batter face angles of between 25-30 degrees found to be appropriate. No inferred material is included in the Ore Reserve estimate. The mine plan includes provisions for additional infrastructure to support the operation. The majority of the infrastructure required was put in place in 2018.
Metallurgical factors or assumptions	<ul style="list-style-type: none"> <i>The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.</i> <i>Whether the metallurgical process is well-tested technology or novel in nature.</i> <i>The nature, amount and representativeness of metallurgical test work undertaken,</i> <i>The nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.</i> <i>Any assumptions or allowances made for deleterious elements.</i> <i>The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.</i> <i>For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?</i> 	<ul style="list-style-type: none"> The Century tailings deposit is processed through the on-site processing facility which was reconfigured to treat tailings material in 2018. The process involves further grinding followed by a froth flotation circuit. Zinc concentrates are thickened and pumped via a 304km long pipeline to the port in Karumba, where they are filtered and transferred to ocean going vessels for transport to smelters for further processing. Reconciled tailings reprocessing metallurgical data have been used to develop estimates for future mineral recoveries, which have been used in the estimation of the Ore Reserves. Due to the uncertainty associated with the timing and extent of planned improvements to metallurgical recoveries, the Ore Reserve Estimate is based on recovery estimates established from historical data for which a higher level of confidence is available. Assumed average recoveries are 47.5% for Zinc, 0% for Lead and 30% for Silver. No allowances are made for deleterious elements.

Criteria	JORC Code Explanation	Commentary
Environmental	<ul style="list-style-type: none"> <i>The status of studies of potential environmental impacts of the mining and processing operation.</i> <i>Details of waste rock characterisation and</i> <i>the consideration of potential sites, status of design options considered and, where applicable,</i> <i>the status of approvals for process residue storage and waste dumps should be reported.</i> 	<ul style="list-style-type: none"> The Century tailings operation has all environmental approvals in place and is compliant to those conditions set out in such approvals. Environmental rehabilitation plans are produced, and the cost of the mine close rehabilitation work is accounted for in the financial evaluation model.
Infrastructure	<ul style="list-style-type: none"> <i>The existence of appropriate infrastructure:</i> <i>availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.</i> 	<ul style="list-style-type: none"> All mining, processing and support infrastructure to support the current operation are already in place with minor incremental modifications required to support ongoing operations. Newly generated tailings from the reprocessing of the tailings dam material are pumped into the historic century open pit via existing pipelines.
Costs	<ul style="list-style-type: none"> <i>The derivation of, or assumptions made, regarding projected capital costs in the study.</i> <i>The methodology used to estimate operating costs.</i> <i>Allowances made for the content of deleterious elements.</i> <i>The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co- products.</i> <i>The source of exchange rates used in the study.</i> <i>Derivation of transportation charges.</i> <i>The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.</i> <i>The allowances made for royalties payable, both Government and private.</i> 	<ul style="list-style-type: none"> The hydraulic mining operating and processing costs are based on the detailed mine plan and historic data collected since 2018. An operational cost estimate been derived from the mine plan and associated input projections. Mining, processing, pipeline, transportation, treatment, refining and selling costs are well understood from actual costs incurred in the processing, handling and treatment of tailings material at Century mine. Cost estimates for overhead expenses including G&A, flights and accommodation were derived from current budget forecasts and actual incurred costs for Century mine. The exchange rate used is assumed to be 0.74 AUD/USD. The Queensland Government royalty of 3.8% for zinc and 5.0% for silver have been applied to the gross revenue for each metal minus allowable deductions for ocean freight and metal playability deductions. A private royalty of 2% of NSR has been applied. Treatment charges of USD \$180 per zinc concentrate tonne and shipping charges of USD \$50 per wet metric tonne of concentrate have been applied. No allowances have been made for deleterious elements outside of lead in the concentrate.
Revenue factors	<ul style="list-style-type: none"> <i>The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc</i> <i>The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.</i> 	<ul style="list-style-type: none"> Commodity price assumptions are based on New Century Resources' assessment of consensus economics data using a zinc price of USD \$2,450/t and a silver price of USD \$22/Oz and an exchange rate of 0.74 AUD/USD to calculate the revenue. The net revenue is calculated for each mining shape, based on royalties, treatment cost and revenue inputs. Mining costs are then subtracted from this, determining the revenue. All the costs associated with the net revenue are well known from the from the past three years of the tailings operation.
Market Assessment	<ul style="list-style-type: none"> <i>The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into</i> 	<ul style="list-style-type: none"> Century has successfully sold zinc concentrates into the domestic and export markets since restart in 2018. Concentrate grades are estimated to be 48% Zinc and are sold at both contracted and spot terms.

Criteria	JORC Code Explanation	Commentary
	<p><i>the future.</i></p> <ul style="list-style-type: none"> • A customer and competitor analysis along with the identification of likely market windows for the product. • Price and volume forecasts and the basis for these forecasts. • For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract. 	
Economic	<ul style="list-style-type: none"> • The inputs to the economic analysis to produce the net present value (NPV) in the study, • The source and confidence of these economic inputs including estimated inflation, discount rate, etc • NPV ranges and sensitivity to variations in the significant assumptions and inputs. 	<ul style="list-style-type: none"> • The Ore Reserve estimate has been evaluated through the site's life of mine planning financial model, showing that the Century tailings operation is economic. All operating and capital costs as well as revenue factors are included in the financial model. This process has demonstrated that the Ore Reserve for the tailings deposit has a positive NPV.
Social	<ul style="list-style-type: none"> • The status of agreements with key stakeholders and matters leading to social license to operate. 	<ul style="list-style-type: none"> • The Century Mining tenements ML90045 and ML90058 are subject to the Gulf Communities Agreement (GCA) which was negotiated between Pasminco, the Queensland Government and four native title groups - the Waanyi, the Mingginda, the Gkuthaarn and the Kukatj, under the right to negotiate provisions contained within the Native Title Act of 1993 (Commonwealth). • The native title rights and interests associated with the Transport Infrastructure Corridor for the Pipeline and the Karumba Port Facility were acquired by the State of Queensland and Operational Licences were granted to Century Mining Limited. The consent from the relevant native title holders for the grant of the Operational Licence (and other grants) is contained in the GCA.
Other	<ul style="list-style-type: none"> • To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves: • Any identified material naturally occurring risks. • The status of material legal agreements and marketing arrangements. • The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. • There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent. 	<ul style="list-style-type: none"> • There are typical risks for a tailings reprocessing operation such as heavy rain fall events, geotechnical risks and equipment failure. These risks are managed through the implementation of various risk management mechanisms as far as practical.
Classification	<ul style="list-style-type: none"> • The basis for the classification of the Ore Reserves into varying confidence categories. 	<ul style="list-style-type: none"> • The Ore Reserve Estimate has been prepared in accordance with the guidelines of the JORC Code, 2012 and is based on the Mineral Resource Estimate.

Criteria	JORC Code Explanation	Commentary
	<ul style="list-style-type: none"> Whether the result appropriately reflects the Competent Person's view of the deposit. The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any). 	<ul style="list-style-type: none"> The Ore Reserves are entirely derived from Measured Resources. This classification is based on the ore continuity, historic tailings deposition discharge data, density of drilling, the experience from the last three years of operation the mining method employed. All Ore Reserves are categorized as Proven Reserves. It is the Competent Person's view that the classification used for the Ore Reserves is appropriate.
Audits or reviews	<ul style="list-style-type: none"> The results of any audits or reviews of Ore Reserve estimates. 	<ul style="list-style-type: none"> No external audits of this Ore Reserve Estimate have been completed to date.
Discussion of relative accuracy/confidence	<ul style="list-style-type: none"> Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate. The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used. Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage. It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available. 	<ul style="list-style-type: none"> The accuracy of the Ore Reserve estimate is directly influenced by the order of accuracy associated with the Mineral Resource model, the metallurgical input and the long-term costs and the revenue assumptions applied. Confidence of the inputs is considered to be high due to the operating state of the mine. In the opinion of the Competent Person, the modifying factors and long-term cost assumptions used in the Ore Reserve estimate are reasonable.

Appendix 3: Silver King Drill Hole Results

Drill hole co-ordinates, orientations and type used in the estimation of the Silver King Resource. (Geotechnical and Metallurgical holes were not included in the estimation)

Hole_ID	E_AMG94	N_AMG94	RL	HOLE DEPTH	HOLE TYPE	Dip	Azim (AMG)
MMG900	246141.5	7926046	146.9	230	DD	-60	120
MMG901	246146.2	7926043	147	244.7	DD	-71	117
MMG902	246228.9	7925993	145.8	148.8	DD	-61	116
MMG903	246254.8	7926072	145.1	209	DD	-63	115
MMG904	246256.6	7926071	145	229.6	DD	-71	113
MMG905	246051.4	7925960	149.3	180.1	DD	-61	116
MMG906	245999.1	7925992	150	230	DD	-63	116
MMG907	246100.3	7926024	147.5	220.3	DD	-70	116
MMG908	246176.8	7925977	146.6	116.5	DD	-61	116
MMG909	246252.9	7926025	145.2	140.2	DD	-61	117
MMG910	246208.7	7926052	145.6	248.2	DD	-70	117
MMG911	246230.4	7926086	145.1	257.7	DD	-70	116
MMG912	246296.7	7926093	144.3	300	DD	-60	117
MMG913	246235.2	7926130	144.8	300	DD	-70	116
MMG914	246289.1	7926144	144.2	221.6	DD	-71	116
MMG915	246207.1	7926147	145	320.3	DD	-71	115
MMG916	246261.6	7926114	144.4	308.5	DD	-70	115
MMG917	246278.9	7926056	144.5	160	DD	-60	116
MMG918	246312.8	7926130	143.6	284.8	DD	-71	116
MMG919	246343.5	7926111	143.6	239.3	DD	-60	112
MMG920	246326.7	7926168	143.6	302.3	DD	-70	110
MMG921	246343.8	7926158	143.4	269.6	DD	-61	109
MMG922	246198.9	7926105	145.4	281.7	DD	-71	118
MMG923	246176.3	7926072	145.9	269.4	DD	-71	115
MMG924	246196.1	7926060	145.8	207.4	DD	-61	116
MMG925	246115.4	7926061	147	274.6	DD	-71	118
MMG926	246166.7	7926031	146.4	179	DD	-60	113
MMG927	246072.2	7926041	147.9	251.6	DD	-70	116
MMG928	246148.4	7925995	147.1	149.1	DD	-61	117
MMG929	246080	7925942	148.7	128.7	DD	-66	116
MMG931	246052.5	7925959	149.3	170.8	DD	-71	117
MMG932	246062.4	7925906	149.3	130	DD	-75	116
MMG933	246003.6	7925941	150.4	179.3	DD	-60	112
MMG957	246339.4	7926025	144	290	DD	-80	234
MMG958	246241.3	7926074	145	255.9	DD	-75	231
MMG959	246190.4	7926016	146.1	231.8	DD	-70	202
MMG960	246178.6	7925949	146.7	220	DD	-70	231
MMG961	246353.4	7926122	143.5	310	DD	-80	205
MMG962	246390.7	7926183	143.4	297.5	DD	-60	116
MMG963	246080.6	7925918	148.9	195.8	DD	-75	211
MMG964	246355.8	7926204	143.5	339.5	DD	-60	116
MMG965	246393.8	7926228	143.4	333.1	DD	-55	119
MMG966	246638.6	7926312	141.6	410.6	DD	-60	116
MMG967	246192.9	7925817	146.7	205	DD	-80	284
MMG968	246105.8	7925981	148.1	198.8	DD	-70	211
MMG969	246330.6	7925972	144.2	216.7	DD	-70	321
MMG970	246419.7	7925946	143.3	325	DD	-65	331
MMG971	246523.7	7926287	142.5	342.5	DD	-60	116
MMG972	246551.7	7926269	142.3	325	DD	-69	151
MMG973	246599.7	7926334	142.1	306.4	DD	-54	145
MMG976	246291.1	7925905	145.2	231.8	DD	-71	335
MMG977	246204.4	7926146	145.1	324.6	DD	-72	151
MMG979	246221.7	7925872	146.2	215.6	DD	-65	336
MMG980	246168.9	7926121	145.8	297.6	DD	-69	150
SK21_001	246078.1	7925917	148.8	133	DD	-82	171
SK21_002	246078.1	7925917	148.8	105.6	DD	-59	130
SK21_005	246075.6	7925934	148.4	130	DD	-68	134
SK21_006	246075.5	7925934	148.7	141.5	DD	-60	131
SK21_008	246062.5	7925999	148.8	195	DD	-66	140

Hole_ID	E_AMG94	N_AMG94	RL	HOLE DEPTH	HOLE TYPE	Dip	Azim (AMG)
SK21_009	246082.1	7925984	148.4	178.4	DD	-60	130
SK21_012	246164	7925954	146.7	100	DD	-60	130
SK21_015	246134.9	7926025	147.1	198.7	DD	-60	130
SK21_017	246100.8	7926074	147.1	250	DD	-62	127
SK21_018	246181.5	7926019	146.2	156	DD	-60	130
SK21_021	246247	7926019	145.1	141.7	DD	-59	133
SK21_023	246159.1	7926159	145.2	310.6	DD	-60	145
SK21_024	246182.5	7926151	145.1	306.8	DD	-60	145
SK21_025	246204.6	7926132	145.1	285.7	DD	-60	145
SK21_027	246241	7926098	144.8	220	DD	-59	144
SK21_028	246307.4	7926059	144.1	180.6	DD	-60	145
SK21_029	246281.4	7926105	144.2	221.6	DD	-59	145
SK21_031	246317.7	7926080	143.7	175	DD	-60	145
SK21_032	246303.8	7926102	143.9	209	DD	-59	146
SK21_036	245973.9	7925824	153.355	105.6	DD	-60	120
SK21_037	245950	7925802	156.361	102	DD	-60	121
SK21_038	245937.2	7926019	151.1765	99.8	DD	-60	129
SK21_039	245969.8	7926074	150.1348	98.5	DD	-60	130
SK21-040	245974.9	7925655	154.3707	100	RC	-60	300
SK21-041	245934.5	7925636	157.4311	100	RC	-60	300
SK21-042	245930.9	7925595	159.1748	100	RC	-60	300
SK21-043	245926.9	7925547	157.2098	100	RC	-60	300
SKDDH02	245963.5	7925877	152.3	136.2	DD	-60	121
SKDDH03	246021.4	7925889	150.7	118.5	DD	-60	121
SKDDH04	245955.3	7925836	153.5	115.5	DD	-60	121
SKDDH05	246000.5	7925855	152.2	70.7	DD	-60	121
SKDDH06	246097.6	7925937	148.8	112	DD	-60	121
SKDDH07	246030.2	7925744	151.4	134	DD	-55	301
SKDDH08	245954.3	7925790	158.7	67	DD	-45	121
SKDDH09	245953	7925743	163.3	49.2	DD	-50	121
SKDDH10	246002.9	7925900	150.7	104.5	DD	-60	121
SKDDH11	245933.6	7925847	153.5	136.5	DD	-60	121
SKDDH12	245901.8	7925774	158.2	183.1	DD	-60	121
SKDDH13	245974.4	7925828	153.5	72.5	DD	-60	121
SKDDH14	245918.7	7925811	155.5	145.5	DD	-55	121
SKDDH15	245932.1	7925662	158.6	15	DD	-55	301
SKQ006	246136.6	7925877	148	39.7	DD	-60	134
SKQ007	246121.3	7925901	148	74.6	DD	-60	134
SKQ008	246182.7	7925900	147	45.6	DD	-60	134
SKQ009	246165.3	7925926	147	75.6	DD	-60	134
SKQ010	246222.1	7925931	146	43.1	DD	-60	134
SKQ011	246202.9	7925954	146	87.6	DD	-60	134
SKQ012	246261.3	7925962	145	65	DD	-60	134
SKQ013	246241.5	7925986	147	96.6	DD	-60	134
SKQ014	246277.1	7926054	144.5	300.6	DD	-69	297
SKQ018	246079	7925965	148.8	147.2	DD	-60	116
SKQ019	246120.5	7925939	147.1	99.3	DD	-60	119
SKQ020	246064.2	7925975	148.9	172	DD	-65	116
SKQ021	246155.9	7925964	146	132.1	DD	-60	118
SKQ022	246134.6	7925977	146.1	132.1	DD	-60	119
SKQ023	246114.4	7925991	147	162.4	DD	-60	117
SKQ025	246192.7	7925991	146.2	131	DD	-60	117
SKQ026	246171.4	7926004	146	152.2	DD	-60	117
SKQ027	246149.7	7926019	147	177.3	DD	-60	117
SKQ028	246129.6	7926032	147.2	192.1	DD	-61	119
SKQ029	246107.1	7926046	146	245.4	DD	-61	118
SKQ030	246232	7926014	145.6	140	DD	-61	116
SKQ031	246210.3	7926028	144	155	DD	-60	117
SKQ032	246188.2	7926041	143	192	DD	-60	118
SKQ033	246167.9	7926055	146.1	205.4	DD	-60	116
SKRC01	246000.4	7925807	152.6	41	RC	-60	121
SKRC02	245988.8	7925815	152.9	58.3	RC	-60	121
SKRC03	245972.7	7925827	153.5	82.3	RC	-60	121
SKRC04	246031.8	7925836	151.7	40	RC	-60	121
SKRC05	246019	7925844	151.7	59	RC	-60	121
SKRC06	246001.7	7925854	152.2	56	RC	-60	121

Hole_ID	E_AMG94	N_AMG94	RL	HOLE DEPTH	HOLE TYPE	Dip	Azim (AMG)
SKRC07	246041.3	7925875	151.7	71	RC	-60	121
SKRC08	246083.7	7925898	149.2	77	RC	-60	121
SKRC09	246100.7	7925887	148.8	65	RC	-60	121
SKRC10	246117.7	7925876	148.1	50	RC	-60	121
SKRC101	246004.3	7925876	150.5	97	RC	-60	120
SKRC102	245995.9	7925882	150.7	100	RC	-60	120
SKRC104	246058.3	7925836	149.1	67	RC	-60	120
SKRC105	246050.1	7925842	151.5	61	RC	-60	120
SKRC106	246042.4	7925848	149.7	77	RC	-60	120
SKRC107	246034.7	7925854	149.8	59	RC	-60	120
SKRC108	246075.5	7925849	148.9	55	RC	-60	120
SKRC109	246067.2	7925854	150.7	55	RC	-60	120
SKRC11	246131.3	7925869	147.7	29	RC	-60	121
SKRC110	246059.5	7925860	149.4	83	RC	-60	120
SKRC111	246051.2	7925867	149.6	71	RC	-60	120
SKRC112	246093.9	7925860	148.7	49	RC	-60	120
SKRC113	246085.8	7925866	149.5	55	RC	-60	120
SKRC114	246078.1	7925872	149	89	RC	-60	120
SKRC115	246069.3	7925878	149.3	83	RC	-60	120
SKRC117	246102.5	7925879	148.5	95	RC	-60	120
SKRC118	246093.7	7925885	150.1	89	RC	-60	126
SKRC119	246020.3	7925864	150	79	RC	-60	120
SKRC12	246131.9	7925916	147.8	77	RC	-60	121
SKRC13	246165	7925894	147.2	77	RC	-60	121
SKRC14	246058.7	7925865	149.9	65	RC	-60	121
SKRC15	246076.8	7925855	149.5	53	RC	-60	121
SKRC16	246091.3	7925846	149.5	35	RC	-60	121
SKRC17	245918.9	7925904	153	23	RC	-60	121
SKRC18	245905.3	7925910	153.5	41	RC	-60	121
SKRC19	245898.9	7925870	154	25	RC	-60	121
SKRC20	245885.9	7925878	152	47	RC	-60	121
SKRC21	245984.1	7925865	152.2	83	RC	-60	121
SKRC22	246042.4	7925825	150.5	47	RC	-60	121
SKRC23	246114.7	7925926	148.3	95	RC	-60	121
SKRC24	245953.6	7925790	158.7	60	RC	-55	121
SKRC25	245937.8	7925800	156.7	98	RC	-55	121
SKRC26	245941.8	7925750	161.5	59	RC	-52	121
SKRC27	245940.1	7925751	161.5	77	RC	-61	121
SKRC28	245922.1	7925762	158.8	128.7	RC	-58	121
SKRC29	245935.5	7925708	162	65	RC	-55	121
SKRC30	245913.1	7925721	160.2	95	RC	-55	121
SKRC31	245928.9	7925663	159.5	77	RC	-55	301
SKRC32	245934	7925661	158.5	41	RC	-60	301
SKRC33	245919.3	7925622	159	29	RC	-60	301
SKRC34	245929.1	7925618	158.7	43	RC	-60	301
SKRC35	245900.9	7925915	154	45	RC	-60	121
SKRC36	245855.9	7925940	156.4	47	RC	-60	121
SKRC37	245892.3	7925918	153.2	61	RC	-60	121
SKRC38	245939.7	7925609	157.9	47	RC	-60	301
SKRC39	245909.8	7925582	162.6	35	RC	-60	301
SKRC40	245921.4	7925574	160	47	RC	-60	301
SKRC41	245906.1	7925536	157.8	35	RC	-54	301
SKRC42	245915.1	7925532	157.1	47	RC	-60	301
SKRC43	245998.2	7925814	153.6	47	RC	-60	121
SKRC44	245936.6	7925707	162.3	11	RC	-50	121
SKRC44A	245939.8	7925705	162.5	53	RC	-50	121
SKRC45	245944.4	7925655	157	68	RC	-61	301
SKRC46	245914.3	7925672	162.4	35	RC	-55	301
SKRC47	245889.5	7925643	168.9	17	RC	-50	301
SKRC48	245895.6	7925639	167.8	59	RC	-65	301
SKRC49	245984.6	7925795	155	52	RC	-60	121
SKRC50	245928.5	7925593	159.9	28	RC	-60	301
SKRC51	245964.4	7925805	156.2	71.5	RC	-60	121
SKRC52	245951.3	7925813	155	95	RC	-60	121
SKRC53	245992	7925788	153.8	33	RC	-50	121
SKRC54	246011.9	7925825	151.2	46	RC	-50	121

Hole_ID	E_AMG94	N_AMG94	RL	HOLE DEPTH	HOLE TYPE	Dip	Azim (AMG)
SKRC55	246002.4	7925831	151.4	71	RC	-60	121
SKRC56	245985.6	7925838	151.6	59	RC	-60	89
SKRC57	245971.7	7925849	152.1	97	RC	-60	121
SKRC58	245940.4	7925772	159.8	77	RC	-48	121
SKRC59	245938.9	7925773	159.3	88	RC	-60	121
SKRC60	245940	7925774	159.8	83	RC	-54	121
ZCL590	246118.6	7925914	148.1	105.5	DD	-70	120
ZCL591	246118.6	7925914	148	150.5	DD	-80	120
ZCL592	246152.8	7925944	147.3	120.3	DD	-60	120
ZCL593	246151.3	7925945	147.3	149.8	DD	-80	120
ZCL594	246151.3	7925944	147.3	249.8	DD	-90	360
ZCL595	246080	7925892	149.1	165.5	DD	-65	230
ZCL596	246080	7925892	149	149.6	DD	-60	120
ZCL597	246080	7925892	149	119.5	DD	-80	120
ZCL598	246063.8	7925919	149.3	142.2	DD	-60	200
ZCL599	245983.9	7925857	151.8	119.4	DD	-60	120
ZCL600	245982.4	7925857	151.8	150.5	DD	-80	120
ZCL601	245965.3	7925844	152.6	64.6	DD	-55	120
ZCL602	245965.3	7925844	152.6	118	DD	-70	120
ZCL603	245963.9	7925842	152.7	68.1	DD	-55	120
ZCL604	245963.9	7925843	152.7	120.4	DD	-70	120
ZCL605	246009.8	7925751	151.8	120.5	DD	-55	300
ZCL606	246009.8	7925751	151.8	162.1	DD	-70	300
ZCL607	246014.5	7925724	151.6	150.2	DD	-55	300
ZCL608	245964	7925625	155.1	99.6	DD	-55	300
ZCL609	245981.6	7925814	153.4	43.9	DD	-60	120
ZCL610	245981.6	7925815	153.4	108.5	DD	-75	120
ZCL611	245945.4	7925823	154	100	DD	-55	120
ZCL612	245944	7925823	154	150.5	DD	-75	120
ZCL624	246323.5	7926112	144	241.3	RC/DD	-70	150
ZCL625	246322	7926112	144.2	297	RC/DD	-74	206
ZCL626	246322	7926112	144.2	300.4	RC/DD	-90	360
ZCL627	246381.5	7926193	143.3	306.6	RC/DD	-60	120
ZCL628	246381.4	7926193	143.3	30	RC	-75	120
ZCL630	246288.9	7926004	144.6	177.4	DD	-90	360
ZCL631	246181.2	7925973	146.5	210.6	DD	-90	360
ZCL632	246141.1	7925952	147.4	177.6	DD	-90	360
ZCL633	246169.6	7925982	146.6	216.6	DD	-90	360
ZCL634	246309.3	7925987	144.4	174.6	DD	-90	360
ZCL635	246123.7	7925965	147.9	189.6	DD	-90	360
ZCL636	246232.9	7925988	145.7	198.5	DD	-80	120
ZCL637	246380	7926193	143.5	70	RC	-70	120
ZCL638	246381.5	7926191	143.5	102	RC	-75	120
ZCL739	245936	7925774	159.4	90	DD	-65	120
ZCL742	246192.9	7925964	146.4	185.3	RC/DD	-90	360
ZCL750	246378.6	7926192	143.4	368.8	RC/DD	-60	120
ZCL751	246377.1	7926193	143.4	423.4	RC/DD	-90	120
ZCL765	246347.5	7926148	143.6	271.3	RC/DD	-60	120
ZCL766	246346	7926149	143.5	307.2	RC/DD	-75	120

Drill hole Results from the 2021 Silver King Drilling Programme

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_001	103.7	104.7	0.03	0.18	1	1.56	0.06
SK21_001	104.7	105.5	15.8	23.9	100	5.18	17.05
SK21_001	105.5	106.5	0.17	1.1	1	4.69	0.5
SK21_001	115.3	116.3	0.14	0.27	1	2.1	0.18
SK21_001	116.3	117.3	1.14	6.21	8	4.67	3.32
SK21_001	117.3	118.3	0.18	0.88	1	2.34	0.22
SK21_001	118.3	119.3	0.36	3.29	6	3.57	1.28
SK21_001	119.3	120.3	8.9	20.2	70	2.93	11.9
SK21_001	120.3	121	8.01	16.8	89	3.43	10.3
SK21_001	121	121.5	10.55	10.9	80	2.78	7.69
SK21_001	121.5	122.5	1.48	2.07	7	3.58	1.24
SK21_001	122.5	123.4	2.32	2.24	9	5.5	3
SK21_001	123.4	124	0.93	4.41	8	18.95	2.8
SK21_001	124	125	0.44	6.6	8	17.35	3.74
SK21_001	125	125.7	0.06	9.44	8	12.85	5.49
SK21_001	125.7	126.7	0.02	2.46	2	7.8	1.31
SK21_001	126.7	127.7	0.01	0.29	1	4.44	0.15
SK21_001	127.7	133	0.01	0.01	1	-	-
SK21_002	82	83	0.06	0.19	4	3	2.1
SK21_002	83	84	2.35	22.1	25	1.65	12.3
SK21_002	84	85	0.32	1.4	3	2.95	3.13
SK21_002	85	86	0.11	1.14	2	1.09	0.82
SK21_002	86	86.55	1.52	2.45	14	1.48	2.01
SK21_002	86.55	87.6	82.6	0.76	1500	0.94	13.45
SK21_002	87.6	88.4	39.3	2.82	360	13.3	8.01
SK21_002	88.4	89	0.53	1.38	4	16.35	0.8
SK21_002	89	89.7	6.16	2.26	27	13.6	2.21
SK21_002	89.7	90.4	0.06	0.6	1	3.46	0.34
SK21_002	90.4	91.4	14.85	0.18	74	6.42	2.4
SK21_002	91.4	92.1	55.1	0.06	244	7.03	8.57
SK21_002	92.1	93.1	0.04	0.16	1	7.24	0.08
SK21_002	93.1	105.6	0.01	0.01	1	-	-
SK21_003	133.5	134.5	0.02	0.1	1	1.06	0.06
SK21_003	134.5	135	0.18	0.55	1	3.22	0.28
SK21_003	135	136	4.3	1.34	11	4.03	1.42
SK21_003	136	137	1.34	1.52	4	2.92	0.66
SK21_003	137	138	0.42	4.31	4	5.24	0.97
SK21_003	138	139	0.43	3.59	7	5.69	2.14
SK21_003	139	140	1.32	9.64	29	7.8	7.37
SK21_003	140	140.7	0.72	24.1	60	6.26	10.45
SK21_003	140.7	141.4	0.06	0.44	1	3.52	0.16
SK21_003	141.4	142.4	0.06	0.8	2	4.24	0.44
SK21_003	142.4	143.4	1.32	0.22	4	5.41	0.27
SK21_003	143.4	144.4	0.01	0.19	1	5.35	0.03
SK21_003	144.4	145.3	0.76	0.26	4	5.47	0.52
SK21_003	145.3	146.4	2.07	1.34	6	5.67	1.3
SK21_003	146.4	147.4	0.01	0.06	1	2.8	0.01
SK21_004	107	108.1	0.03	0.22	1	2.19	0.2
SK21_004	108.1	109	0.11	3.28	4	2	2.59
SK21_004	109	110	0.06	4.34	4	1.76	2.57
SK21_004	110	111.1	0.67	2.35	4	1.02	1.55
SK21_004	111.5	111.7	0.68	3.13	3	3.62	3.6
SK21_004	111.7	112.6	4.08	6.44	11	2.12	3.9
SK21_004	112.6	112.9	0.86	14.5	37	1.72	8.25
SK21_004	113.5	114.2	0.41	3.02	5	3.32	1.76
SK21_004	114.2	115	0.2	1.86	3	2.79	1.12
SK21_004	115	116	0.06	2.08	4	1.54	1.1
SK21_004	116	117	1.36	6.06	12	1.77	3.36
SK21_004	117	118	8.94	11.15	42	3.1	8.57
SK21_004	118	119	0.53	2.1	6	1.06	1.15
SK21_004	119	120.1	0.77	2.05	8	1.82	1.79
SK21_004	120.1	121	0.55	2.53	7	1.09	1.48
SK21_004	121	122	1.86	2.83	13	2.55	1.82

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_004	122	122.9	1.24	16	19	4.32	8.85
SK21_004	122.9	124	2.54	5.14	15	15.6	3.27
SK21_004	124	125.1	4.65	5.1	40	23.8	3.51
SK21_004	125.1	125.9	9.08	27.2	94	13.1	16.15
SK21_004	125.9	127	0.62	0.16	1	4.53	0.2
SK21_004	127	128	0.01	0.1	1	5.62	0.06
SK21_005	105.5	106	0.49	1.18	5	4.14	1.02
SK21_005	106	107	0.41	0.86	4	3.76	1.02
SK21_005	107	107.9	0.15	0.83	4	2.21	0.91
SK21_005	107.9	109	3.89	19.45	55	1.5	10.8
SK21_005	109	110	0.97	5.24	10	1.39	2.95
SK21_005	110	111	9.56	14.5	46	1.66	9.09
SK21_005	111	112	4.41	19.05	61	2.69	10.6
SK21_005	112	112.7	6.06	9.56	56	5.4	6.39
SK21_005	112.7	113.6	2	0.47	11	9.23	0.75
SK21_005	113.6	114.5	1.84	15.75	41	3.8	8.53
SK21_005	114.5	115.5	6.38	5.59	40	2.86	4.06
SK21_005	115.5	116	0.59	1.82	5	2.99	1.07
SK21_005	116	117	12.35	12.4	53	3.67	8.73
SK21_005	117	117.7	8.49	22.3	42	7.27	16.6
SK21_005	117.7	118.5	0.16	3.1	5	14.55	1.68
SK21_005	118.5	119	1.58	20.7	47	11.45	11.25
SK21_005	119	119.6	43.8	13.2	320	5.53	14.05
SK21_005	119.6	120.6	0.13	0.21	1	3.18	0.3
SK21_005	120.6	128.7	0.01	0.01	1	-	-
SK21_005	128.7	129.9	0.01	0.01	1	-	-
SK21_005	129.9	130	0.01	0.01	1	-	-
SK21_006	97.5	98.5	0.04	0.15	1	0.48	0.1
SK21_006	98.5	99	0.65	0.65	5	2.32	1.96
SK21_006	99	100	1.91	4.2	8	1.73	3.22
SK21_006	100	100.7	10.2	2.27	55	1.65	3.61
SK21_006	100.7	101.75	6.68	20.3	48	2.39	12.75
SK21_006	101.75	102.7	0.21	3.52	10	2.12	3.26
SK21_006	102.7	103.5	2.31	7.44	23	4.5	8.33
SK21_006	103.5	104.4	6.14	12.9	71	2.23	9.13
SK21_006	104.4	105.1	0.95	2.29	11	2	2.31
SK21_006	105.1	106.2	10.5	15.2	76	1.81	9.97
SK21_006	106.2	107.3	1.68	1.98	9	9.44	1.36
SK21_006	107.3	108.2	7.88	4.19	88	12.25	3.46
SK21_006	108.2	109	83.5	0.41	992	1.19	13.25
SK21_006	109	109.8	74.9	2.31	794	1.82	13.05
SK21_006	109.8	110.9	0.11	0.3	2	7.9	0.29
SK21_006	110.9	112	1	1.62	9	5.95	1.1
SK21_006	112	112.95	0.01	0.01	1	-	-
SK21_006	112.95	141.5	0.01	0.01	1	-	-
SK21_007	70.8	71.8	0.02	0.06	2	2.59	1.62
SK21_007	71.8	72.7	0.04	0.13	2	1.89	1.08
SK21_007	72.7	73.7	1.4	1.91	7	1.56	1.77
SK21_007	73.7	74.7	6.44	21	11	2.5	12
SK21_007	74.7	75.7	0.05	0.9	2	3.1	0.88
SK21_007	75.7	76.5	0.05	2.33	2	12.3	1.52
SK21_007	76.5	77.2	0.02	11.4	17	7.13	6.07
SK21_007	77.2	78.1	0.05	0.04	1	5.36	0.28
SK21_007	78.1	79	0.09	0.06	1	6.42	0.24
SK21_007	79	80	0.12	0.07	1	7.27	0.26
SK21_007	80	81	0.56	0.22	4	10.45	0.4
SK21_007	81	81.6	75	3.33	1140	1.28	14
SK21_007	81.6	82.3	68	0.07	1320	2.1	10.75
SK21_007	82.3	82.9	12.6	29.2	211	5.29	17.55
SK21_007	82.9	84	0.2	0.21	1	5.74	0.21
SK21_008	169	170	0.01	0.22	1	2.14	0.22
SK21_008	170	171	0.8	4.06	9	3.36	2.84
SK21_008	171	171.9	0.9	9.48	17	5.08	5.93
SK21_008	171.9	172.7	3.63	23.1	132	5.92	12.9
SK21_008	172.7	173.9	0.11	0.63	2	6.29	0.55
SK21_008	173.9	174.9	0.01	0.14	1	6.91	0.26

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_008	173.85	195	0.01	0.01	1	-	-
SK21_009	140	140.85	0.32	0.84	3	3.33	0.9
SK21_009	140.85	141.5	10.9	16.15	47	1.91	10.25
SK21_009	141.5	142.1	2.77	28.4	47	2.25	15.6
SK21_009	142.1	142.8	14	4.04	93	2.67	4.49
SK21_009	142.8	143.4	21.3	14	119	2.15	10.75
SK21_009	143.4	144.1	10.65	8.68	52	2.13	6.27
SK21_009	144.1	145.1	7.5	1.11	50	1.44	1.96
SK21_009	145.1	146.1	5.13	1.54	28	1.8	2.2
SK21_009	146.1	147.1	0.77	0.27	4	1.79	0.87
SK21_009	147.1	148.1	38.2	7.86	221	1.38	10.2
SK21_009	148.1	149	14.35	19.85	87	2.52	12.95
SK21_009	149	149.5	1.5	1.2	7	7.73	1.45
SK21_009	149.5	150.5	5.62	3.47	26	3.08	2.97
SK21_009	150.5	151.3	19.2	7.37	79	5.41	7.65
SK21_009	151.3	151.7	2.35	15.6	42	8.11	10.85
SK21_009	151.7	152.7	0.24	0.85	2	3.04	0.48
SK21_009	152.7	155.05	0.01	0.01	1	-	-
SK21_009	155.05	163.5	0.01	0.01	1	-	-
SK21_009	163.5	178.4	0.01	0.01	1	-	-
SK21_011	93.4	94.1	0.22	0.42	4	2.18	1.6
SK21_011	94.1	95.2	0.1	0.04	3	1.92	1.04
SK21_011	95.2	96.3	1.01	1.59	6	1.76	1.54
SK21_011	96.3	96.9	41.3	3.36	382	3.22	9.65
SK21_011	96.9	97.8	0.53	1.11	5	11.9	1
SK21_011	97.8	98.4	14.9	3.57	73	11.1	4.59
SK21_011	98.4	99	0.4	0.05	2	4.74	0.58
SK21_011	99	99.7	1.48	0.33	5	14.05	1.1
SK21_011	99.7	100.7	0.02	0.08	1	4.02	0.29
SK21_012	75.4	76.4	0.1	0.05	4	1.98	1.34
SK21_012	76.4	77.2	13.8	6.17	115	5.97	10.35
SK21_012	77.2	77.4	0.01	0.01	1	-	-
SK21_012	77.4	77.9	1.92	8.35	38	12.95	5.75
SK21_012	77.9	78.9	0.1	0.09	1	11	0.62
SK21_012	78.9	97	0.01	0.01	1	-	-
SK21_012	97	99.8	0.01	0.01	1	-	-
SK21_012	99.8	100	0.01	0.01	1	-	-
SK21_013	105	106	0.05	0.07	3	2.01	1.28
SK21_013	106	107	0.2	0.2	3	1.86	0.92
SK21_013	107	107.8	13.3	7.8	36	1.32	6.15
SK21_013	107.8	108.6	3.16	7.54	16	1.7	4.85
SK21_013	108.6	109.5	52.4	15.3	681	2.71	16.75
SK21_013	109.5	110.1	58.2	4.79	478	2.78	11.65
SK21_013	110.1	111	69.7	5.33	864	1.81	13.95
SK21_013	111	111.9	15.25	29.6	45	3.46	18.2
SK21_013	111.9	112.4	70.7	3.23	868	2.22	12.9
SK21_013	112.4	113.2	71.5	1.86	913	5.57	12.35
SK21_013	113.2	113.9	5.33	3.23	39	23	2.59
SK21_013	113.9	114.2	72.5	0.05	402	1.82	11.3
SK21_013	114.2	115	0.93	0.06	4	3.71	0.39
SK21_013	115	116	0.05	0.01	1	2.15	0.04
SK21_014	78	79	0.13	0.05	3	2.74	2.05
SK21_014	79	79.9	0.1	2.83	3	2.21	2.75
SK21_014	79.9	80.7	1.72	3.37	9	1.54	2.86
SK21_014	80.7	81.6	0.15	0.31	4	1.9	1.06
SK21_014	81.6	82.2	0.08	0.04	5	2.41	1.24
SK21_014	82.2	82.85	0.46	0.14	9	3.53	1.6
SK21_014	82.85	83.5	12	2.39	61	3.43	4.61
SK21_014	83.5	84.5	0.1	0.16	2	2.74	0.73
SK21_015	154.7	155.7	0.696	0.268	4	2.91	0.24
SK21_015	155.7	156	4.33	27.2	49	3.67	0.3
SK21_015	156	157	1.995	3.78	16	3.48	0.26
SK21_015	157	158	0.189	4.57	8	3.13	0.24
SK21_015	158	159	0.118	4.22	8	3.29	0.15
SK21_015	159	159.5	0.288	4	9	3.53	0.39
SK21_015	159.5	160.5	12.05	0.635	68	2.8	0.49

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_015	160.5	161.5	0.145	0.621	2	2.25	0.06
SK21_015	161.5	162.6	2.77	2.7	15	2.96	0.26
SK21_015	162.6	163	0.162	0.2	2	2.87	0.09
SK21_015	163	163.3	0.632	0.409	4	1.42	0.09
SK21_015	163.3	164	20	1.365	329	2.33	0.86
SK21_015	164	165.1	20	1.635	78	1.9	0.51
SK21_015	165.1	165.7	4.5	0.676	21	4.52	0.31
SK21_015	165.7	166.3	0.983	0.036	5	4.6	0.3
SK21_015	166.3	166.7	5.21	13.1	40	3.14	0.37
SK21_015	166.7	167.5	6.43	0.354	68	12.55	0.86
SK21_015	167.5	168.5	2.29	0.194	7	6.31	0.18
SK21_015	168.5	169.2	10.25	1.43	36	3.25	0.44
SK21_015	169.2	170.2	0.626	0.208	3	4.43	0.07
SK21_015	170.2	171.2	3.03	0.014	8	3.9	0.18
SK21_015	171.2	172	4.62	0.006	21	1.74	0.29
SK21_015	172	172.7	6.61	3.3	86	2.11	0.32
SK21_015	172.7	173	20	10.35	433	5.11	0.55
SK21_015	173	174	0.217	0.017	2	3.02	0.04
SK21_015	190	191	1.085	0.507	5	5.9	0.59
SK21_015	191	192.2	9.27	12.4	88	20.1	19.75
SK21_015	192.2	193.2	0.009	0.008	1	6.64	0.02
SK21_015	193.2	198.7	0.01	0.01	1	-	-
SK21_016	178	178.95	0.2	0.04	2	3.92	0.08
SK21_016	178.95	179.45	40	14.8	477	5.09	14.45
SK21_016	179.45	180.2	4.69	0.85	27	14.2	1.32
SK21_016	181.5	182	9.98	6.53	104	2.82	5.47
SK21_016	182	182.8	17.9	1.42	106	3.53	3.55
SK21_016	182.8	183.8	1.04	0.06	5	3.14	0.2
SK21_016	183.8	184.9	3.07	0.84	15	6.75	0.96
SK21_016	184.9	186	0.23	1.78	4	2.39	1
SK21_016	186	187	16.7	3.14	94	4.53	6.19
SK21_016	187	188	0.18	0.14	2	2.46	0.27
SK21_016	188	189	0.06	0.16	1	2.44	0.09
SK21_016	189	190	0.01	0.02	1	2.15	0.03
SK21_016	190	191	0.03	5.75	12	2.47	3.04
SK21_016	191	192	0.01	0.04	1	2.29	0.05
SK21_016	192	193	0.01	0.02	1	3.29	0.04
SK21_016	193	194	0.02	0.02	1	2.64	0.04
SK21_016	194	195	1.72	3.83	10	8.43	3.08
SK21_016	195	196	0.23	0.81	3	5.65	0.53
SK21_016	196	197	0.28	3.04	4	6.2	1.78
SK21_016	197	198	0.24	4.21	4	9.62	2.35
SK21_016	198	199	3.32	3.74	13	4.79	2.55
SK21_016	199	200	0.34	0.84	2	3.24	0.56
SK21_016	200	201	0.04	0.11	1	4.11	0.09
SK21_016	201	202	0.08	0.11	1	6.25	0.11
SK21_016	202	203	1.71	0.78	8	6.34	0.89
SK21_016	203	203.8	0.24	4.49	12	6.83	2.82
SK21_016	203.8	204.9	0.04	18.3	9	3.63	9.73
SK21_016	204.9	206	0.02	21.1	12	7.52	11.35
SK21_016	206	207	0.38	10.15	8	5.74	5.57
SK21_016	207	207.7	1.12	5.37	16	5.17	4.34
SK21_016	207.7	208.7	5.6	11.3	38	9.06	8.01
SK21_016	208.7	209.7	1.28	3.53	10	8.04	2.12
SK21_016	209.7	210.5	0.71	2.19	5	8.74	1.26
SK21_016	210.5	211.5	3.89	22.7	52	8.25	12.95
SK21_016	211.5	212.5	5.89	24.7	62	8.11	14.4
SK21_016	212.5	213.5	5.12	13.05	43	8.74	7.81
SK21_016	213.5	214.5	0.06	20.2	17	6.25	10.75
SK21_016	214.5	215.5	0.07	23.1	22	6.09	12.5
SK21_016	215.5	216.6	0.04	1.98	2	6.6	1.06
SK21_016	216.6	217.7	0.04	0.27	2	7.48	0.25
SK21_016	217.7	218.8	0.02	0.05	1	8.01	0.08
SK21_016	218.8	219.9	0.15	1.26	2	7.87	0.72
SK21_016	219.9	220.9	1.27	0.36	5	8.67	0.44
SK21_016	220.9	222	0.13	0.28	1	8.18	0.22

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_016	222	223	0.11	0.16	1	5.78	0.12
SK21_016	223	224	0.01	0.06	1	6.5	0.18
SK21_016	224	225	0.04	1.22	3	9.41	0.71
SK21_016	225	226.1	0.61	0.11	3	9.58	0.3
SK21_016	226.1	227.2	0.45	0.77	2	7.69	0.67
SK21_016	227.2	228.2	0.22	8.35	5	3.25	4.53
SK21_016	228.2	229	0.01	3.82	2	4.05	2.17
SK21_016	229	230	-0.01	0.01	1	2.35	0.03
SK21_016	80	81.1	0.07	0.01	1	1.66	0.14
SK21_016	81.1	81.4	2.46	3.55	17	11.1	4.95
SK21_016	81.4	81.9	0.84	0.48	5	3.73	0.76
SK21_016	81.9	82.2	46.7	7.37	225	6.31	11.25
SK21_016	82.2	83.2	0.32	0.13	2	4.61	0.16
SK21_017	175.4	176.4	1.5	0.13	7	4.84	0.37
SK21_017	176.4	177	31.3	24.4	399	7.48	19.5
SK21_017	177	177.9	58.9	12.3	679	3.88	15.65
SK21_017	177.9	178.8	0.31	0.21	4	4.04	0.18
SK21_017	178.8	180	0.97	0.47	7	3.64	0.43
SK21_017	180	181.2	0.49	0.08	5	3.46	0.24
SK21_017	181.8	182.6	40.8	27.4	553	2.49	20.8
SK21_017	182.6	183.3	43	5.58	329	8.22	9.41
SK21_017	183.3	184	1.45	2.97	21	7.41	1.81
SK21_017	184	184.9	11.3	7.69	77	6.18	5.91
SK21_017	184.9	185.7	6.73	5.23	48	7.59	3.91
SK21_017	185.7	186.9	0.32	2.77	5	6.52	1.6
SK21_017	186.9	188	39.5	17.45	437	3.76	15.5
SK21_017	188	189	32.7	22.5	373	7.2	18.1
SK21_017	189	190	10.2	16.95	114	7.83	10.55
SK21_017	190	191	7.98	25.7	116	8.22	14.6
SK21_017	191	192	2.65	15.05	37	14.15	8.45
SK21_017	192	193	3.06	15.35	35	15.25	8.65
SK21_017	193	194	1.3	15.5	16	15.8	8.25
SK21_017	194	195	12.15	13.7	78	11.25	9.41
SK21_017	195	196	2.17	21	46	13.5	11.35
SK21_017	196	196.8	12.5	7.58	50	8.11	6.05
SK21_017	196.8	197.8	4.73	39.2	48	6.75	20.9
SK21_017	197.8	198.6	1	18	32	16.3	10.7
SK21_017	198.6	199.4	1.45	34	17	4.36	17.8
SK21_017	199.4	200.4	2.08	27.6	16	3.53	14.4
SK21_017	200.4	201.4	0.67	32.8	14	2.97	16.85
SK21_017	201.4	202.4	0.1	3.41	5	9.83	2.12
SK21_017	202.4	202.9	0.13	5.9	6	26.7	3.38
SK21_017	202.9	203.3	0.06	0.59	2	6.41	0.38
SK21_017	203.3	203.8	1.33	41.5	135	3.95	21.3
SK21_017	203.8	204.5	0.49	14.85	20	4.13	7.57
SK21_017	204.5	205.4	0.27	2.92	4	3.32	1.84
SK21_017	205.4	206	0.43	2.7	4	5.43	1.78
SK21_017	206	207	0.15	0.59	2	7.55	0.46
SK21_017	207	208	1.19	10.45	26	6.3	5.63
SK21_017	208	209	0.64	6.71	7	2.34	3.6
SK21_017	209	210	0.34	4.52	4	1.93	2.45
SK21_017	210	211	0.85	2.79	5	1.7	1.74
SK21_017	211	212	3.18	4.72	17	1.7	3.1
SK21_017	212	213	0.3	6.76	6	3.38	3.79
SK21_017	213	214	2.4	20.2	23	4.34	10.8
SK21_017	214	215	1.08	14.55	25	19	8.57
SK21_017	215	215.8	34.9	5.69	186	15.3	14.35
SK21_017	215.8	216.8	6.89	17.45	158	18.95	21.2
SK21_017	216.8	217.8	12.95	15.7	125	10.15	10.15
SK21_017	217.8	218.8	3.6	20.2	81	10.3	10.7
SK21_017	218.8	219.6	45.5	13.15	319	5.61	14.5
SK21_017	219.6	220.1	4.47	13.15	60	9.65	8.05
SK21_017	220.1	221.2	31.7	28	348	5.1	19.75
SK21_017	221.2	222	0.21	3.52	7	15.8	1.85
SK21_017	222	223	0.25	0.96	3	8.18	0.7
SK21_017	223	224	0.23	0.27	2	6.17	0.35

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_017	224	225	0.05	1.93	3	5.28	1.28
SK21_017	225	226	0.06	0.54	2	5.32	0.58
SK21_017	226	227	0.02	0.06	1	5.89	0.12
SK21_017	227	227.8	0.18	0.05	1	9.72	0.11
SK21_017	227.8	228.5	1.86	9.8	16	6.53	5.25
SK21_017	228.5	229.5	0.11	0.84	2	5.16	0.61
SK21_017	249	249.9	1.45	0.24	4	17.9	0.38
SK21_017	249.9	250	0.01	0.01	1	-	-
SK21_018	123.4	124.4	0.026	0.084	4	3.37	2.46
SK21_018	124.4	125.4	0.032	0.068	4	2.35	1.74
SK21_018	125.4	125.8	0.028	0.501	3	2.15	1.4
SK21_018	125.8	126.8	0.032	0.339	2	2.08	1.3
SK21_018	126.8	127.5	0.022	0.125	2	1.73	0.97
SK21_018	127.5	128.5	0.054	0.042	3	3.49	3.09
SK21_018	128.5	129.5	0.096	0.035	5	3.34	2.48
SK21_018	129.5	130.5	0.18	0.2	4	3.69	1.63
SK21_018	130.5	130.7	3.71	0.745	25	3.03	2.21
SK21_018	130.7	131.2	1.62	7.28	21	2.36	4.44
SK21_018	131.2	131.55	1.335	1.965	14	4.18	1.9
SK21_018	131.55	131.9	11	4.8	68	11.8	4.42
SK21_018	131.9	132.6	8.38	2.69	37	9.27	2.95
SK21_018	132.6	132.9	20	2.58	695	7.62	11.05
SK21_018	132.9	133.4	4.81	0.28	33	12.15	1.17
SK21_018	133.4	133.6	20	0.481	659	4.38	9.13
SK21_018	133.6	134.6	1.765	0.261	24	7.52	0.54
SK21_018	134.6	135.6	0.101	0.011	3	4.34	0.12
SK21_018	135.6	136.6	0.026	0.074	2	1.88	0.11
SK21_018	136.6	138	0.01	0.01	1	-	-
SK21_018	138	145.6	0.01	0.01	1	-	-
SK21_018	145.6	155.9	0.01	0.01	1	-	-
SK21_018	155.9	156	0.01	0.01	1	-	-
SK21_019	33.7	34	0.18	5.89	2	1.94	4.04
SK21_019	35.8	36.2	0.03	4.52	1	2.18	3.12
SK21_019	80	80.7	0.03	0.03	1	3.64	1.39
SK21_019	80.7	81.2	2.4	6.89	4	1.68	4.57
SK21_019	81.2	82.2	1.57	0.01	4	1.97	1.14
SK21_019	82.2	83.3	0.05	0.09	1	1.54	0.82
SK21_019	83.3	84.4	0.21	0.01	3	1.74	1.04
SK21_019	84.4	85.4	0.51	1.97	4	1.37	1.76
SK21_019	85.4	86	0.07	0.07	2	1.66	0.9
SK21_019	86	87	0.19	0.1	3	2.67	2.26
SK21_019	87	88	0.06	0.04	3	2.59	1.78
SK21_019	88	89	0.05	0.17	3	2.97	1.34
SK21_019	89	90	0.3	0.33	4	2.58	1.48
SK21_019	90	91	16.15	6.56	80	10.05	10.2
SK21_019	91	92	1.02	8.8	22	9.3	5.09
SK21_019	92	92.9	0.13	12.9	25	6.62	7.19
SK21_019	92.9	93.5	30.9	19.05	526	7.62	15.5
SK21_019	93.5	94.1	46	11.6	693	3.72	13.85
SK21_019	94.1	95	1.1	0.48	6	7.9	1.98
SK21_019	95	96	0.02	0.06	1	3.76	0.58
SK21_020	102.9	103.5	0.08	0.04	3	6.78	5.77
SK21_020	112.5	113.3	0.95	0.35	4	3.9	2.35
SK21_020	113.3	114	7.43	9	41	4.39	8.01
SK21_020	114	114.7	7.34	0.87	26	7.66	3.15
SK21_020	114.7	115.3	3.73	0.45	17	5.15	1.82
SK21_020	115.3	115.8	2.18	12.75	52	7.48	7.15
SK21_020	115.8	116.7	0.35	1.43	5	2.98	0.98
SK21_020	116.7	117.6	1.1	2.34	13	17.75	1.46
SK21_020	117.6	118.5	11.1	3.87	177	22	3.94
SK21_020	118.5	119.1	75	0.35	1030	2.5	12.8
SK21_020	119.1	119.7	75	0.19	1110	0.45	13.8
SK21_020	119.7	120.1	36.9	12.25	375	11.55	12.25
SK21_020	120.1	120.5	56.9	11.35	1160	3.81	15.2
SK21_020	120.5	120.9	2.52	4.46	38	20.2	2.91
SK21_020	120.9	122	0.02	0.02	1	7.27	0.02

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_021	98.7	99.7	0.11	0.75	3	3.71	1.9
SK21_021	99.7	100.7	0.06	1.46	3	2.9	1.86
SK21_021	100.7	101.7	0.05	2.36	4	2.88	2.82
SK21_021	101.7	102.7	0.17	0.68	5	6.63	6.59
SK21_021	102.7	103.3	0.07	1.71	4	2.87	2.75
SK21_021	103.3	103.9	0.64	7.24	9	1.72	4.57
SK21_021	103.9	104.6	0.53	10.5	21	1.58	5.83
SK21_021	104.6	105.1	39.5	2.84	149	0.94	7.75
SK21_021	105.1	106	3.53	18.25	26	1.7	10.35
SK21_021	106	106.7	0.38	15.9	7	1.49	8.49
SK21_021	106.7	107.6	3.06	2.6	17	1.78	2.7
SK21_021	107.6	108.4	0.12	0.22	3	5.54	0.8
SK21_021	108.4	109.4	0.01	0.02	2	6.84	0.54
SK21_021	114	115	0.03	1.28	3	6.05	1.02
SK21_021	115	115.8	0.02	0.43	2	5.57	0.62
SK21_021	115.8	116.6	0.04	5.21	5	7.13	3.08
SK21_021	116.6	117.1	22.6	10.75	267	5.01	10.55
SK21_021	117.1	118.2	0.86	0.52	8	3.72	3.42
SK21_021	118.2	119	0.06	0.06	2	2.49	0.61
SK21_021	119	141.7	0.01	0.01	1	-	-
SK21_022	152.4	153.5	0.32	0.02	3	3.37	0.2
SK21_022	153.5	154.15	3.69	15.45	43	14.5	8.89
SK21_022	154.15	155.1	1.46	1.18	9	4.63	1.32
SK21_022	155.1	155.6	24.8	7.58	127	8.74	14
SK21_022	155.6	156.4	0.03	0.01	1	1.06	0.06
SK21_022	284.3	285.3	0.02	0.01	1	2.56	0.05
SK21_022	285.3	285.9	0.01	0.01	1	5	0.39
SK21_022	285.9	286.5	0.01	0.01	1	6.67	0.19
SK21_022	286.5	287.5	0.01	1.1	1	4.33	0.63
SK21_022	287.5	288.5	0.01	0.03	1	2.39	0.1
SK21_022	288.5	289.5	0.01	0.92	1	2.76	0.59
SK21_022	289.5	290.4	0.01	2.16	2	2.39	1.32
SK21_022	290.4	291.4	0.02	5.79	12	9.13	3.18
SK21_022	291.4	292	0.02	1.24	2	14.25	0.78
SK21_022	292	292.7	0.06	1.62	2	17.2	1.08
SK21_022	292.7	293.6	0.01	0.01	1	5.55	0.05
SK21_022	293.6	294.5	0.02	0.01	1	7.9	0.06
SK21_022	294.5	295.3	0.01	0.01	1	4.67	0.06
SK21_022	295.3	296.1	0.03	0.18	1	6.39	0.21
SK21_022	296.1	296.9	0.01	0.01	1	7.45	0.05
SK21_022	296.9	297.7	0.01	-0.01	1	4.85	0.51
SK21_022	297.7	298.7	0.02	-0.01	1	1.78	0.08
SK21_023	131.2	132.2	0.035	0.037	1	3.29	0.33
SK21_023	132.2	133.2	0.16	0.161	2	3.68	0.84
SK21_023	133.2	134.1	3.51	12.65	38	8.71	9.09
SK21_023	134.1	134.9	0.179	2.99	8	7.41	2
SK21_023	134.9	135.8	20	1.97	141	8.32	5.59
SK21_023	135.8	136.6	5.52	0.59	29	9.27	1.84
SK21_023	136.6	137.65	20	0.347	531	4.08	11.4
SK21_023	137.65	138.27	20	4.07	225	15.75	7.09
SK21_023	138.27	139	6.61	5.31	54	6.99	4.2
SK21_023	139	139.8	1.01	5.49	15	7.13	3.5
SK21_023	139.8	140.6	0.364	1.53	4	4.64	1.04
SK21_023	140.6	141.6	0.018	0.069	1	2.91	0.06
SK21_023	141.6	142.6	0.007	0.001	1	2.34	0.08
SK21_023	185.1	186.1	0.067	0.002	1	5.9	0.04
SK21_023	186.1	187.1	0.833	0.157	3	3.55	0.26
SK21_023	187.1	188.1	4.52	3.27	32	5.42	3.71
SK21_023	188.1	189.1	2.38	1.57	16	7.1	3.44
SK21_023	189.1	190.1	13.4	6.08	120	6.41	6.61
SK21_023	190.1	191.1	7.07	8.18	40	7.87	6.49
SK21_023	191.1	192.1	0.015	0.009	1	4.09	0.06
SK21_023	192.1	193	0.038	0.009	1	3.78	0.12
SK21_023	193	193.8	0.219	0.755	2	3.97	0.69
SK21_023	193.8	194.8	0.007	0.002	2	2.3	0.32
SK21_023	194.8	195.8	0.007	0.002	1	1.9	0.09

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_023	234.6	235.5	0.038	0.103	1	4.15	0.19
SK21_023	235.5	236.6	0.047	0.181	1	3.83	0.2
SK21_023	236.6	237.6	0.42	3.94	7	5.95	2.43
SK21_023	237.6	238.6	20	16.2	381	3.68	16.2
SK21_023	238.6	239.6	0.373	0.043	3	5.43	0.3
SK21_023	239.6	240.7	0.225	0.029	2	5.92	0.47
SK21_023	264.7	265.7	0.952	0.468	3	1.6	0.44
SK21_023	265.7	266.7	4.33	1.045	12	2.81	1.26
SK21_023	266.7	267.7	1.6	1.42	7	2.72	1.08
SK21_023	267.7	268.7	1.37	2	7	2.64	1.38
SK21_023	268.7	269.7	10.55	3.16	35	3.93	3.32
SK21_023	269.7	270.7	15.55	5.4	55	5.2	5.39
SK21_023	270.7	271.7	3.37	14.4	36	8.36	11.1
SK21_023	271.7	272.7	0.855	7.23	11	4.53	4.36
SK21_023	272.7	273.7	1.135	9.79	15	4.24	5.51
SK21_023	273.7	274.7	1.175	13.65	14	4.11	7.43
SK21_023	274.7	275.7	1.035	7.22	10	4.9	4.2
SK21_023	275.7	276.6	1.15	7.5	10	5.8	4.32
SK21_023	276.6	277.5	0.067	3.13	5	7.55	1.83
SK21_023	277.5	278.5	0.004	0.019	1	3.71	0.03
SK21_023	278.5	279.5	0.004	0.015	1	3.16	0.17
SK21_023	289.6	290.6	0.04	0.215	1	3.72	0.2
SK21_023	290.6	291.6	0.004	0.454	1	12.2	0.29
SK21_023	291.6	292.6	0.003	0.092	1	5.55	0.1
SK21_023	292.6	293.4	0.003	0.003	1	3.4	0.02
SK21_023	293.4	294.4	0.003	0.011	1	4.39	0.04
SK21_023	294.4	295.4	0.002	0.006	1	7.55	0.03
SK21_023	295.4	296.2	0.023	2.93	3	4.78	1.62
SK21_023	296.2	297.2	0.009	0.778	1	3.97	0.47
SK21_023	297.2	298.2	0.002	0.569	1	2.64	0.43
SK21_023	298.2	299.2	0.003	0.065	1	2.88	0.17
SK21_023	299.2	303.7	0.01	0.01	1	-	-
SK21_023	303.7	310.6	0.01	0.01	1	-	-
SK21_024	186	187	1.12	0.14	5	6.02	0.34
SK21_024	187	188	0.65	0.02	2	5.43	0.76
SK21_024	188	189	1.7	2.56	13	7.45	3.17
SK21_024	189	190	0.19	0.03	2	4.67	0.87
SK21_024	190	191	0.85	0.33	5	4.78	0.8
SK21_024	191	192	1.65	0.56	8	4.69	1
SK21_024	192	193	4.68	0.66	20	13.5	1.92
SK21_024	193	194	1	1.38	7	3.2	1.26
SK21_024	194	195	8.61	0.66	54	3.43	3.68
SK21_024	195	195.8	0.3	0.01	2	2.08	0.3
SK21_024	195.8	196.8	16.4	4.03	83	7.45	10.45
SK21_024	196.8	198	31.9	3.25	393	9.83	16.35
SK21_024	198	199	6.15	3.08	31	3.54	4.12
SK21_024	199	200	2.5	4.35	11	2.18	3.02
SK21_024	200	201	1.8	0.02	7	3.73	0.77
SK21_024	201	202	0.26	0.01	2	2.35	0.28
SK21_024	202	203	21.4	0.64	65	1.88	3.84
SK21_024	203	204	0.15	0.04	1	5.34	1.95
SK21_024	204	205	0.23	0.3	2	3.12	0.6
SK21_024	205	206	0.04	0.01	1	3.18	0.14
SK21_024	206	207	0.02	0.04	1	2.6	0.13
SK21_024	207	208	0.01	0.01	1	1.47	0.11
SK21_024	208	209	0.03	0.01	1	3.38	0.03
SK21_024	209	210.2	0.03	0.01	1	2.5	0.03
SK21_024	210.2	211.2	0.02	0.02	1	2.71	0.1
SK21_024	211.2	212.2	0.06	0.01	1	2.15	0.14
SK21_024	212.2	213.2	0.4	0.06	1	2.13	0.23
SK21_024	213.2	214.2	2.59	0.3	82	3.67	2.16
SK21_024	214.2	215.2	2.13	0.04	10	4.21	0.78
SK21_024	215.2	216.2	1.22	0.01	4	3.53	0.7
SK21_024	216.2	217.25	0.97	0.1	4	3.89	0.58
SK21_024	217.25	218.1	7.05	1.04	28	2.97	2.65
SK21_024	218.1	218.8	0.95	2.19	8	2.62	1.66

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_024	218.8	219.8	0.96	0.26	5	1.72	0.55
SK21_024	219.8	220.4	0.7	0.08	5	2.97	0.55
SK21_024	220.4	221.4	0.12	0.04	2	2.05	0.49
SK21_024	221.4	222	0.02	-0.01	1	0.89	0.16
SK21_024	222	223	0.09	0.25	2	1.42	0.62
SK21_024	240.2	241.2	0.3	0.11	5	2.53	0.98
SK21_024	241.2	242.2	4.2	3.84	30	2.06	3.17
SK21_024	242.2	243.2	0.83	0.27	4	2.75	0.62
SK21_024	243.2	244.2	0.2	0.75	2	2.3	0.66
SK21_024	244.2	245	4.49	0.8	16	1.79	1.31
SK21_024	245	246	1.38	0.02	5	3.57	0.38
SK21_024	246	247	0.36	0.01	2	5.35	0.22
SK21_024	247	248	0.45	0.01	3	2	0.21
SK21_024	248	249	3.7	0.02	17	3.81	0.72
SK21_024	249	250	0.77	0.04	7	3.71	0.3
SK21_024	250	251	0.08	0.01	2	3.85	0.12
SK21_024	251	251.9	0.07	0.01	1	3.83	0.12
SK21_024	251.9	252.4	0.58	3.57	8	4.28	2.12
SK21_024	252.4	253.4	14.75	6.66	63	5.35	5.77
SK21_024	253.4	254.2	45.7	14	587	5.26	15
SK21_024	254.2	255	82.7	1.06	794	0.87	13.55
SK21_024	255	256.1	46.9	12.15	543	4.9	14.15
SK21_024	256.1	257.2	12	5.41	67	7.8	4.85
SK21_024	257.2	258.3	14.5	16.55	89	10.2	10.8
SK21_024	258.3	259.2	1.28	0.43	6	10.95	0.48
SK21_024	259.2	260.3	5.54	24.9	66	6.12	14.8
SK21_024	260.3	261.3	9.61	4.43	35	4.62	3.89
SK21_024	261.3	262.4	17.15	9.56	111	3.04	7.85
SK21_024	262.4	263.4	3.28	2.36	19	3.55	1.96
SK21_024	263.4	264.4	0.03	0.02	1	2.12	0.17
SK21_024	264.4	265	0.5	0.01	3	2.34	0.23
SK21_024	265	266	0.09	1.12	3	2.65	0.78
SK21_024	266	267	0.01	0.01	1	1.74	0.04
SK21_024	267	268	0.06	0.42	2	2.78	0.49
SK21_024	268	269	0.38	0.39	2	2.82	0.3
SK21_024	269	270	0.29	0.1	2	3.19	0.43
SK21_024	270	271	1.67	0.51	6	19.3	0.93
SK21_024	271	272	24	0.21	77	16.3	3.95
SK21_024	272	273.1	12.4	2.3	83	16.7	3.61
SK21_024	273.1	274	0.05	0.06	1	10.9	0.08
SK21_024	274	275	0.05	0.07	1	6.87	0.07
SK21_024	275	276	0.02	0.01	1	7.83	0.01
SK21_024	276	277	0.01	0.05	1	5.71	0.04
SK21_024	277	278	0.06	0.47	1	5.8	0.29
SK21_024	278	279	0.01	0.01	1	6	0.03
SK21_024	279	280	0.01	0.01	1	6.1	0.05
SK21_024	280	281	0.01	0.01	1	5.96	0.07
SK21_024	281	282	0.02	0.06	1	5.43	0.05
SK21_024	282	283	0.01	0.82	1	5.36	0.56
SK21_024	283	284	0.02	0.24	1	8.46	0.21
SK21_024	284	285	0.01	0.99	1	14.95	0.58
SK21_024	285	286	0.01	0.05	1	11.1	0.05
SK21_024	286	287	0.02	1.52	1	4.2	0.94
SK21_024	287	288	0.02	0.24	1	14.35	0.77
SK21_024	288	289	0.01	0.02	1	14.35	0.06
SK21_024	289	289.5	0.01	0.01	1	14.9	0.11
SK21_024	289.5	290.5	0.01	-0.01	1	1.76	0.06
SK21_024	290.5	294.4	0.01	0.01	1	-	-
SK21_024	294.4	306.8	0.01	0.01	1	-	-
SK21_025	222	223.1	2.62	0.22	15	2.78	2.02
SK21_025	223.1	223.6	47.3	2.43	177	1.12	8.85
SK21_025	223.6	224.6	14.35	0.14	53	1.3	2.92
SK21_025	224.6	225.7	3.66	1	20	2.48	2.54
SK21_025	225.7	226.6	17.8	11.45	66	2.2	9.45
SK21_025	226.6	227.5	7.38	12.7	44	2.12	8.53
SK21_025	227.5	228.4	3.14	0.23	15	2.13	1.73

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_025	228.4	229	2.23	0.18	12	2.57	1.69
SK21_025	229	230	3.08	15.4	32	2.45	9.21
SK21_025	230	231	3.45	12.25	38	3.16	8.49
SK21_025	231	232	5.41	15	54	2.82	9.41
SK21_025	232	233	5.23	12.7	29	2.31	8.33
SK21_025	233	234.1	6.27	47.6	77	2.74	26.1
SK21_025	234.1	235	2.38	2.06	11	1.44	2.09
SK21_025	235	236	1.74	4.22	13	3.59	4.99
SK21_025	236	237	3.99	10.7	30	2.35	7.23
SK21_025	237	238	3.29	9.36	26	2.62	6.39
SK21_025	238	239	1.05	1.78	6	2.97	1.38
SK21_025	239	240	0.02	0.12	1	7.69	0.22
SK21_025	246.2	247.25	0.12	0.12	2	3.72	0.24
SK21_025	247.25	248.35	45.2	5.09	358	9.13	15.4
SK21_025	248.35	249.45	39	4.34	211	8.92	9.49
SK21_025	249.45	250	1.02	0.03	4	7.69	0.22
SK21_025	250	251	0.41	0.31	3	9.09	0.3
SK21_025	251	252	0.04	2.35	4	11.8	1.37
SK21_025	252	253	0.07	1.86	4	5.5	1.04
SK21_025	256.5	257.2	0.55	0.88	6	15.75	1.87
SK21_025	257.2	257.9	0.25	0.02	1	6.06	0.07
SK21_025	257.9	258.8	4.11	1.99	18	16.1	1.76
SK21_025	258.8	277	0.01	0.01	1	-	-
SK21_025	277	285.7	0.01	0.01	1	-	-
SK21_026	204	205	0.1	0.14	3	2.06	1.26
SK21_026	205	206	1.42	0.45	5	3.51	2.83
SK21_026	206	207	5.66	2.12	18	2.3	2.33
SK21_026	207	208	0.77	0.03	3	1.93	0.55
SK21_026	208	209	0.14	0.16	1	2.61	0.3
SK21_026	209	210	0.13	0.22	2	5.25	1.16
SK21_026	210	211	0.14	0.27	2	3.97	0.73
SK21_026	211	212	0.43	2.33	6	6.27	1.78
SK21_026	212	213	0.61	3.04	7	5.4	3.7
SK21_026	213	214	0.84	2.87	9	4.19	3.29
SK21_026	214.05	214.9	0.17	0.05	3	15.4	0.28
SK21_026	214.9	216	0.01	0.02	1	6.78	0.08
SK21_026	216	217	0.09	0.84	3	4.55	0.51
SK21_026	217	218	0.16	0.18	2	9.65	0.18
SK21_026	218	219	0.05	0.57	2	2.89	0.33
SK21_026	219	220	-0.01	0.01	1	3.64	0.05
SK21_026	220	221	0.02	0.01	1	8.64	0.04
SK21_026	221	221.9	0.35	1.35	5	6.62	0.85
SK21_026	221.9	222.9	29.1	17.5	357	10.6	13.8
SK21_026	222.9	223.8	0.2	5.13	20	13.1	2.87
SK21_026	223.8	224.9	0.01	0.1	1	11.45	0.06
SK21_027	170	171.1	0.1	0.06	2	3.94	1.4
SK21_027	171.1	172.2	1.34	0.02	8	4.07	3.3
SK21_027	172.2	173.3	0.48	0.04	5	3.41	1.19
SK21_027	173.3	174.4	2.19	0.4	14	4.64	3.76
SK21_027	174.4	174.95	17.7	0.62	82	3.95	4.55
SK21_027	174.95	175.8	9.93	9.92	49	12.6	7.21
SK21_027	175.8	176.9	0.51	5.58	16	6.57	3.29
SK21_027	176.9	177.5	3.7	2.12	22	8.36	1.93
SK21_027	177.5	178	15.3	13.7	245	9.93	9.81
SK21_027	178	178.8	75	2.88	917	1.62	13.65
SK21_027	178.8	179.8	61.3	5.28	746	6.53	12.6
SK21_027	179.8	180.9	59.8	2.55	476	5.9	10.65
SK21_027	180.9	181.7	32.3	5.98	224	2.72	8.29
SK21_027	181.7	182.7	72.1	0.16	567	5.18	11.5
SK21_027	182.7	183.9	33.4	3.23	184	5.85	7.13
SK21_027	183.9	184	0.64	0.02	5	0.55	0.12
SK21_027	184	185	1.95	0.68	11	0.68	0.69
SK21_027	185	185.8	3.43	0.22	15	0.62	0.71
SK21_027	185.8	186.8	4.66	1.35	28	1.26	1.72
SK21_027	186.8	187.3	3.27	12.15	22	1.7	6.67
SK21_027	187.3	188	0.16	0.03	4	2.9	0.71

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_027	188	189	0.32	0.25	4	5.44	1.42
SK21_027	189	190	0.89	1.5	7	6.3	1.36
SK21_027	190	191	1.34	0.96	15	13.9	1.24
SK21_027	191	192	0.59	0.03	5	9.13	0.74
SK21_027	192	192.8	2.9	0.63	17	9.51	1.02
SK21_027	203	203.9	0.4	0.27	4	1.65	1.29
SK21_027	203.9	204.45	51	1.46	462	14.05	22.4
SK21_027	204.45	205.4	1.62	0.03	8	0.67	0.44
SK21_027	205.4	207.4	0.01	0.01	1	-	-
SK21_027	207.4	213	0.01	0.01	1	-	-
SK21_027	213	219.7	0.01	0.01	1	-	-
SK21_027	219.7	220	0.01	0.01	1	-	-
SK21_028	0	1.8	0.01	0.01	1	-	-
SK21_028	1.8	8	0.01	0.01	1	-	-
SK21_028	8	19	0.01	0.01	1	-	-
SK21_028	19	81.2	0.01	0.01	1	-	-
SK21_028	81.2	84.7	0.01	0.01	1	-	-
SK21_028	84.7	103.9	0.01	0.01	1	-	-
SK21_028	103.9	123.9	0.01	0.01	1	-	-
SK21_028	123.9	143.5	0.01	0.01	1	-	-
SK21_028	143.5	180.6	0.01	0.01	1	-	-
SK21_029	178	179	0.54	0.59	5	2.03	1.68
SK21_029	179	180	0.34	0.7	4	1.91	1.6
SK21_029	180	181	0.37	0.29	5	1.47	0.64
SK21_029	181	182	0.43	0.02	6	3.18	2.28
SK21_029	182	183	3.58	1.44	15	1.56	2
SK21_029	183	183.6	1.06	3.2	7	1.81	2.7
SK21_029	183.6	184	2.66	6.72	25	7.69	8.45
SK21_029	184	184.5	11.1	7.2	54	5.54	8.25
SK21_029	184.5	185.1	29.3	2.68	324	12.7	17.8
SK21_029	185.1	185.4	9.42	22.7	118	10.35	13.45
SK21_029	185.4	186	41.8	12.6	766	9.06	13.05
SK21_029	186	186.75	57.9	5.98	926	6.85	12.8
SK21_029	186.75	187.8	0.4	0.43	5	6.46	0.5
SK21_029	187.8	188.9	0.09	0.04	2	1.51	0.11
SK21_029	188.9	189.2	0.01	0.01	1	-	-
SK21_029	189.2	190.5	0.01	0.01	1	-	-
SK21_029	190.5	209.75	0.01	0.01	1	-	-
SK21_029	209.75	221.6	0.01	0.01	1	-	-
SK21_031	140.2	141.2	0.06	0.02	3	2.96	1.22
SK21_031	141.2	142.2	5.56	6.8	41	7.87	10.55
SK21_031	142.2	143.2	1.12	21.9	183	4.32	12.15
SK21_031	143.2	144	1.48	6.78	16	4.69	4.4
SK21_031	144	145	0.04	0.07	1	2.06	0.69
SK21_031	145	174.7	0.01	0.01	1	-	-
SK21_031	174.7	175	0.01	0.01	1	-	-
SK21_032	150.6	151.6	0.01	0.02	2	3.67	1.12
SK21_032	151.6	152.8	0.04	0.06	2	2.52	1.38
SK21_032	152.8	154	0.06	0.08	4	3.92	3.25
SK21_032	154	155	0.03	0.01	3	4.15	3.16
SK21_032	155	156	0.02	0.01	3	3.3	2.01
SK21_032	156	157	0.05	0.02	3	3.99	2.29
SK21_032	157	158	-0.01	0.02	2	4.39	1.16
SK21_032	158	158.8	0.01	0.06	2	3.69	1.32
SK21_032	158.8	159.8	0.05	0.16	2	1.7	1.1
SK21_032	159.8	160.9	0.1	0.24	5	2.16	1.78
SK21_032	160.9	161.9	0.42	6.07	8	1.6	4.02
SK21_032	161.9	162.9	0.06	0.13	3	2.48	1.32
SK21_032	162.9	163.8	0.06	0.07	4	2.9	1.46
SK21_032	163.8	164.7	0.16	0.47	5	3.22	1.54
SK21_032	164.7	165.4	0.12	0.02	4	3.2	1.54
SK21_032	165.4	166	0.22	2.64	16	2.93	2.51
SK21_032	166	166.7	0.53	2.02	13	4.21	3.62
SK21_032	166.7	167.1	0.1	1.95	4	3.25	1.55
SK21_032	167.1	167.5	0.18	27.2	44	1.68	14.25
SK21_032	167.5	168	0.06	0.71	2	8.08	0.73

Hole_ID	From	to	Pb	Zn	Ag	Fe	S
SK21_032	168	168.6	0.21	0.9	5	11.45	0.88
SK21_032	168.6	169.2	24.6	1.78	229	6.55	5.95
SK21_032	169.2	169.7	48.6	14.6	637	3.34	16.4
SK21_032	169.7	170.7	0.17	0.13	2	4.88	0.45
SK21_032	170.3	183.7	0.01	0.01	1	-	-
SK21_032	183.7	197	0.01	0.01	1	-	-
SK21_032	197	209	0.01	0.01	1	-	-
SK21_MET01	138	160	7.24	2.73	45	3.31	2.86
SK21_MET01	161	177	9.01	1.36	190	9.96	2.58
SK21_MET02	169	187	3.27	6.77	33	6.85	4.2
SK21_MET03	216	220	24.67	11	139	3.89	11.06
SK21_MET03	221	227	10.5	2.5	47	3.21	3.06