ASX ANNOUNCEMENT

14 July 2026

ANNUAL MINERAL RESOURCE AND ORE RESERVE STATEMENT[1]

75% increase in Mineral Resources to 3.69 Moz and 159% increase in Ore Reserves to 610 Koz, strengthening the pathway to a larger, longer-life Davyhurst production base

- **Mineral Resources:**
  - **Total Mineral Resource Estimate is 56.5 Mt @ 2.0 g/t for 3.69 Moz, a 75% increase of 1.58 Moz from 1 July 2025, including:**
    - Round Dam Open Pit Mineral Resource increased 964% to 25.4 Mt @ 1.6g/t for 1,330 Koz, up from 125 Koz[2]
    - Waihi Open Pit and Underground Mineral Resource increased 114% to 7.3 Mt at 2.1 g/t for 482 Koz, up from 225 Koz[3]
    - Riverina Underground Mineral Resource increased 18% to 8.7 Mt at 2.5 g/t for 689 Koz, up from 586 Koz
    - Sand King Underground Mineral Resource increased 4% to 3.9 Mt at 2.9 g/t for 363 Koz, up from 348 Koz. Indicated & Measured increased 27% to 223 Koz from 176 Koz
- A maiden Mineral Resource Estimate for Little Gem is scheduled to be delivered in H1 FY27

- **Ore Reserves:**
  - **Total Ore Reserve Estimate increased 159% to 8.4 Mt at 2.3 g/t for 610 Koz,** net of mining depletion of 80 Koz to 1 April 2026.
    - The Ore Reserve base now comprises five principal mining sources across the Davyhurst Gold Project: Waihi Underground, Waihi Open Pit, Round Dam Open Pit, Sand King Underground and Riverina Underground, together with low-grade in-situ material and existing stockpiles
    - Central Davyhurst area Ore Reserves total 4.7 Mt at 2.2 g/t for 332 Koz, including the maiden Waihi Underground Ore Reserve of 825 kt at 3.8 g/t for 101 Koz and the maiden Round Dam Open Pit Ore Reserve of 3.7 Mt at 1.9 g/t for 223 Koz[4]
    - Sand King Underground Ore Reserve increased 49% to 1.24 Mt at 3.2 g/t for 125 Koz, supported by resource conversion drilling, positive grade reconciliation and improved geological confidence
    - Riverina Underground Ore Reserve increased to 844 kt at 3.7 g/t for 100 Koz, demonstrating continued growth of the underground reserve base

Ora Banda Mining Ltd (ASX: OBM or Company) is pleased to announce its Annual Mineral Resources and Ore Reserves Statement update as at 1 April 2026 marking a significant strengthening of the Davyhurst Gold Project inventory base. Since the previous statement as at 1 July 2025, the Company

[1] The Company's nominated annual review date for Mineral Resources and Ore Reserves is 1 April. The effective date of this Statement is 1st April 2026.
[2] The Round Dam MRE was previously announced on 11th Mar 2026
[3] The Waihi MRE was previously announced on 18th May 2026
[4] Waihi underground and Round Dam open pit maiden Ore Reserve Estimate was previously announced 18th May 2026

has delivered substantial growth in Resources and Reserves across the portfolio, including the delivery of a +1.3 Moz Mineral Resource at Round Dam, materially improving the scale, diversity and development flexibility to underpin the future at Davyhurst.

The standout contribution came from Round Dam, where successful exploration and resource definition drilling delivered a +1.3 Moz Mineral Resource and a maiden 223 Koz Ore Reserve, demonstrating the potential for rapid discovery to resource to reserve conversion across the Company's tenement holding.

With demonstrated exploration success, the Company has (and continues) to invest significantly in exploration and resource definition drilling across the Project. In FY26, the Company invested approximately $75 million in drilling activities, completing more than 310,000 metres of reverse circulation and diamond core drilling.

To date, this investment has delivered outstanding, rapid growth in the Company's resource base, with Mineral Resources increasing by 75% (1.58 Moz) to 3.69 Moz from 2.11 Moz and Ore Reserves increasing by 159% to 610 Koz, from 236 Koz (including low-grade material and stockpiles).

The Company's commitment to resource growth remains strong, with a further 340,000 metres of drilling planned for FY27 (excluding grade control drilling), supporting continued resource conversion, reserve growth and future development opportunities. Key focuses for this drilling programme are extensions to known mineralisation at Round Dam, Little Gem and Sand King.

Managing Director, Luke Creagh, commented:

"These excellent results are a credit to our geological team and highlight Ora Banda's commitment to exploration investment, which continues to drive strong organic growth across our highly prospective tenure.

"This is a step-change result for Ora Banda. In less than 12 months, our drilling investment has delivered a 75% increase in Mineral Resources and a 159% increase in Ore Reserves, materially strengthening the production platform at Davyhurst.

"Our ability to discover new deposits, develop them into mines and keep growing them in rapid time is setting us apart and gives us a clear line of sight to our goal to become Australia's next plus 300,000oz gold producer.

"We are currently working towards further additions to our mineral inventory with a maiden mineral resource estimate for Little Gem slated to be delivered in H1 FY27."

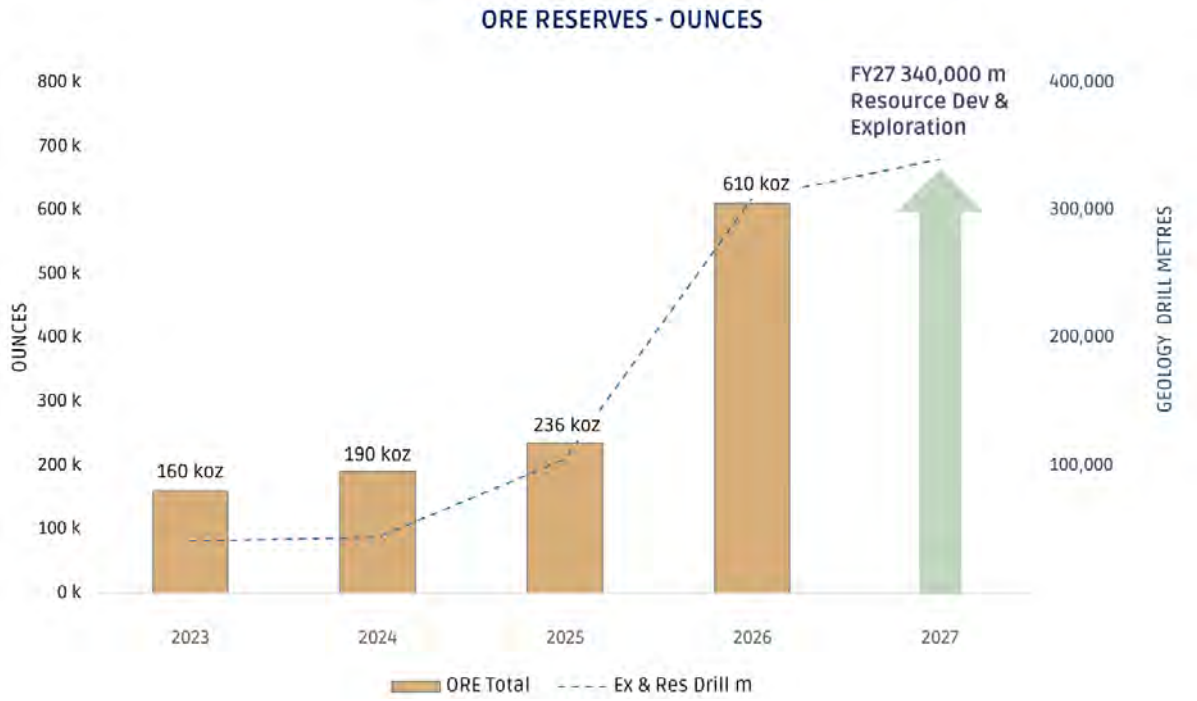

Figure 1 – *Combined Ore Reserve growth by year and total exploration and resource drilling metres*

Figure 2 – *Combined Mineral Resource growth by year and total exploration and resource drilling metres*

Table 1 - Combined Davyhurst Gold Project Mineral Resource estimate, as at 1 April 2026 [5]

MINERAL RESOURCE ESTIMATE	MEASURED			INDICATED			INFERRED			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000 oz.)
Total Project	1,200	2.6	99	25,200	2.1	1,726	30,100	1.9	1,870	56,500	2.0	3,690

Table 2 - Combined Davyhurst Gold Project Ore Reserve Estimate, as at 1 April 2026

ORE RESERVE ESTIMATE	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
Mining Project	297	3.3	32	6,477	2.5	531	6,774	2.6	562
Low Grade & Stockpiles	600	0.9	17	1,030	0.9	31	1,629	0.9	48
TOTAL	**900**	**1.7**	**49**	**7,500**	**2.3**	**560**	**8,400**	**2.3**	**610**

Table 3 - Davyhurst Gold Project Mineral Resource Estimates for deposits with Ore Reserves, as at 1 April 2026

DEPOSIT	MEASURED			INDICATED			INFERRED			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
RIVERINA												
Open Pit	476	1.7	26	2,118	1.6	106	117	1.5	5.8	2,711	1.6	138
Underground	396	3.2	41	4,182	2.3	311	4,151	2.5	338	8,729	2.5	689
SUB TOTAL	**872**	**2.4**	**68**	**6,300**	**2.1**	**417**	**4,268**	**2.5**	**343**	**11,440**	**2.3**	**828**
SAND KING												
Open Pit	-	-	-	-	-	-	-	-	-	-	-	-
Underground	339	2.8	31	2,110	2.8	192	1,439	3.0	140	3,888	2.9	363
SUB TOTAL	**339**	**2.8**	**31**	**2,110**	**2.8**	**192**	**1,439**	**3.0**	**140**	**3,888**	**2.9**	**363**
WAIHI												
Open Pit	-	-	-	224	2.3	16	1	1.0	0	225	2.3	16
Underground	-	-	-	3,833	2.2	268	3,207	1.9	197	7,040	2.1	466
SUB TOTAL	-	-	-	**4,057**	**2.2**	**285**	**3,208**	**1.9**	**197**	**7,265**	**2.1**	**482**
ROUND DAM												
Open Pit	-	-	-	7,152	1.8	408	18,199	1.6	924	25,351	1.6	1,330
Underground	-	-	-	-	-	-	-	-	-	-	-	-
SUB TOTAL	-	-	-	**7,152**	**1.8**	**408**	**18,199**	**1.6**	**924**	**25,351**	**1.6**	**1,330**
TOTAL MRE	**1,200**	**2.6**	**99**	**19,600**	**2.1**	**1,300**	**27,100**	**1.8**	**1,600**	**47,900**	**2.0**	**3,000**

Notes:

1. *This Mineral Resource estimate comprises 4 individual projects.*
2. *This Mineral Resource estimate is inclusive of in-situ Ore Reserves and is exclusive of surface stockpiles*
3. *This Mineral Resource estimate has been modified for mining depletion since 1 July 2025*
4. *The values in the above table have been rounded.*
5. *Further details on the makeup and preparation of this Mineral Resource can be found in the body of this report.*
6. *Refer to Table 5 in this report for the full MRE statement*

[5] Inclusive of Ore Reserve

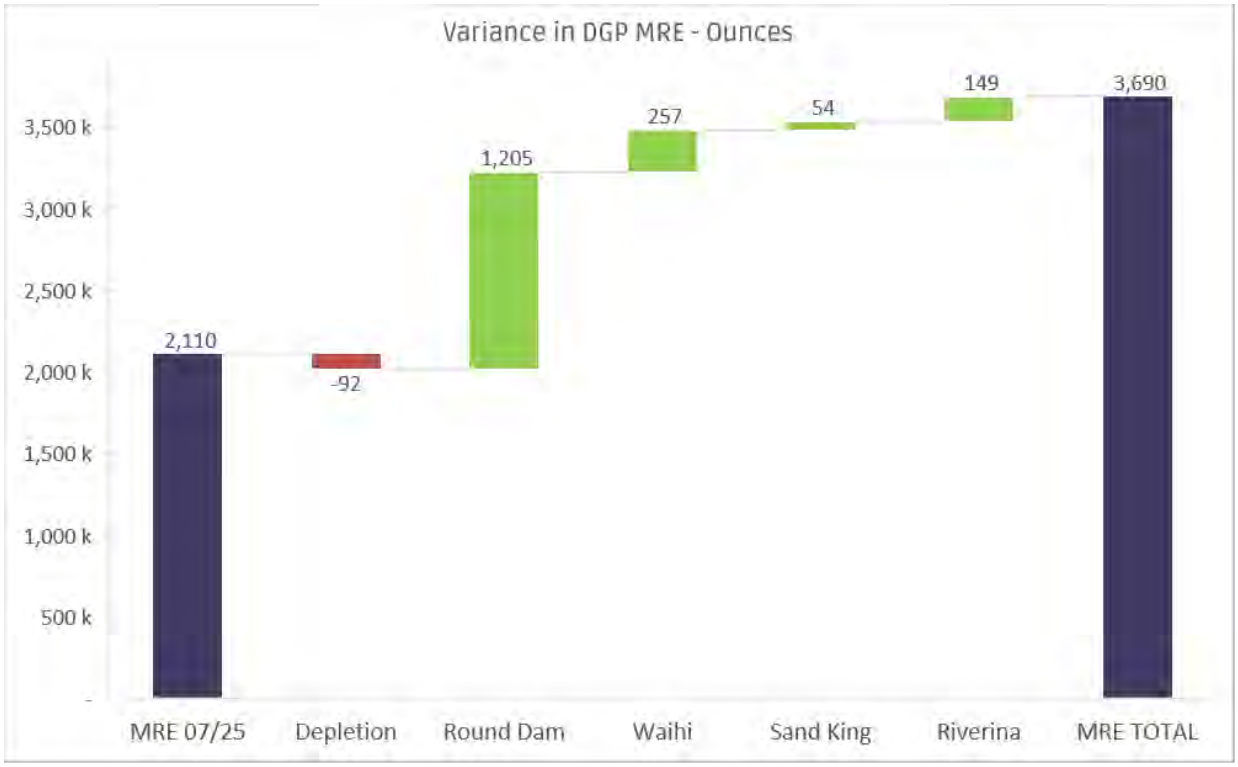

Figure 3 - Change to company MRE ounces - 1 July 2025 to 1 April 2026

MRE - 1 July 2025	**2.11 Moz**	
Material Ounce Changes attributable to:		
Mining Depletion	- 92 Koz	Material mined from Sand King and Riverina Underground mines between 1 July 2025 and 1 April 2026. Includes some material outside of 2025 ORE but within the MRE.
Round Dam	+ 1.205 koz	Significant 1.3 Moz MRE update announced on 11 March 2026.
Waihi UG	+ 257 koz	Maiden underground mine MRE announced to the ASX on 18 May 2026. Significant contribution from Golden Pole which was not included in 2025 MRE.
Sand King	+ 54 koz	Resource conversion, down dip and northern extensional drilling at Sand King have increased the MRE.
Riverina	+ 149 koz	Resource conversion and down dip extensional drilling at Riverina have increased the MRE.
MRE - 1 April 2026	**3.69 Moz**	

Table 4 – Davyhurst Gold Project Ore Reserve by deposit as at 1 April 2026

PROJECT	PROVED			PROBABLE			TOTAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
Davyhurst									
Waihi - Underground	-	-	-	825	3.8	101	825	3.8	101
Waihi - Open Pit	-	-	-	200	2.1	14	200	2.1	14
Round Dam - Open Pit	-	-	-	3,669	1.9	223	3,669	1.9	223
Sub-Total	-	-	-	4,703	2.2	332	4,703	2.2	332
Siberia									
Sand King - Underground	194	2.9	18	1,042	3.2	107	1,236	3.2	125
Sub-Total	194	2.9	18	1,042	3.2	107	1,236	3.2	125
Riverina									
Riverina - Underground	103	4.0	13	741	3.6	87	844	3.7	100
Sub-Total	103	4.0	13	741	3.6	87	844	3.7	100
Low Grade & Stockpiles									
Low Grade – In situ	-	-	-	1,030	0.9	31	1,030	0.9	31
Stockpiles	600	0.9	17	-	-	-	600	0.9	17
Sub-Total	600	0.9	17	1,030	0.9	31	1,629	0.9	48
Combined ORE TOTAL	**900**	**1.7**	**49**	**7,500**	**2.3**	**560**	**8,400**	**2.3**	**610**

Notes:

1. *The combined total is rounded to reflect accuracy and may not total exactly.*
2. *This Ore Reserve Estimate is current as at 1 April 2026.*
3. *This Ore Reserve was estimated from economic practical mining envelopes following the application of modifying factors for mining dilution and ore loss.*
4. *For the underground mine Ore Reserve, dilution skins were applied to the Mineral Resource estimate. Dilution was included at the background grade estimated into the model. The Riverina, Sand King and Waihi dilution was estimated to be 51%, 23% and 29% respectively and includes planned and unplanned dilution reflecting practical mining shapes for the defined mineralisation geometry.*
5. *Mining recovery for Riverina, Sand King and Waihi were estimated to be 83%, 82% and 82% respectively. This recovery allows for rib and sill pillars to remain in place and an additional 5% provision for operational losses.*
6. *The underground mine Ore Reserve was estimated for Riverina, Sand King and Waihi using cut-off grades of 2.5 g/t, 2.4 g/t and 2.2 g/t, respectively. The cut-off grades were based on a gold price of A$2,500/oz. Costs used in the cut-off grade calculation allow for ore haulage, processing, site and corporate overheads and royalties. Process recoveries are specific to the location with process recoveries for Riverina, Sand King and Waihi estimated to be 88%, 87% and 90%, respectively, based on metallurgical test work. The recovery performance through the Davyhurst plant, from processing Riverina and Sand King ores, was 92% in FY26 to EOM March-26.*
7. *For the Waihi and Round Dam open pit Ore Reserves, dilution skins were applied to the undiluted Mineral Resources. The method also included internal and edge planned and unplanned dilution resulting from forming practical mineable shapes. The average dilution at Waihi and Round Dam was estimated to be 27% and 20% respectively. Dilution was incorporated in the estimate at the background grades in the block model. The average grade of dilution for Waihi and Round Dam was 0.16 g/t and 0.11 g/t respectively. Ore loss was incurred in the Auto Stope Designer (ASD) Deswik™ process due to variation between mineralised lode geometry and practical dig block geometry. In addition, a nominal 5% loss was applied for further mining losses occurring through normal operations.*
8. *The open pit Ore Reserve was estimated for Waihi and Round Dam using cut-off grades of 1.2 g/t at A$2,400/oz and 0.7 g/t at A$3,600/oz, respectively. Low Grade material within the Ore Reserve for Waihi and Round Dam open pits were estimated using cut-off grades of 0.8 g/t at A$3,400/oz and 0.5 g/t at A$5,000/oz, respectively. Costs used in the cut-off grade calculation allow for ore haulage, processing, site overheads and selling costs. A weight average processing recovery for Waihi and Round Dam ores of 90% and 95%, respectively for oxide, transition and fresh.*
9. *The economic mining envelope at Waihi also considered the cost of disposal of existing in-pit tailings.*
10. *The Inferred Mineral Resource within the mining envelope was considered as waste when defining limits of the mining envelopes; however, minor inclusion of Inferred material occurs as a result of inherent in practical mining shapes within the Underground mines and is not relied upon for economic extraction. Inferred material within the Underground mine portion of the Ore Reserve was estimated at approximately 2% of ounces at 2.3 g/t. This material occurs at the edges of the mining envelope.*

11. *The Ore Reserve is inclusive of existing surface stockpiles above a cut-off grade of 0.5 g/t based on A$5,000/oz. All surface stockpiles were classified as Proved.*
12. *Costs were derived from the FY26 budget estimate including underground contract pricing current at the date of this Ore Reserve, tender contract pricing for Waihi open pit and a contractor budget cost estimate for Round Dam. Unit costs for haulage, processing and site and corporate overheads were estimated based on scheduled process plant throughput of ORE material.*
13. *For the purpose of the economic analysis, all low-grade material was considered to be blended with high grade to produce a head grade above the 0.7 g/t marginal cut off.*

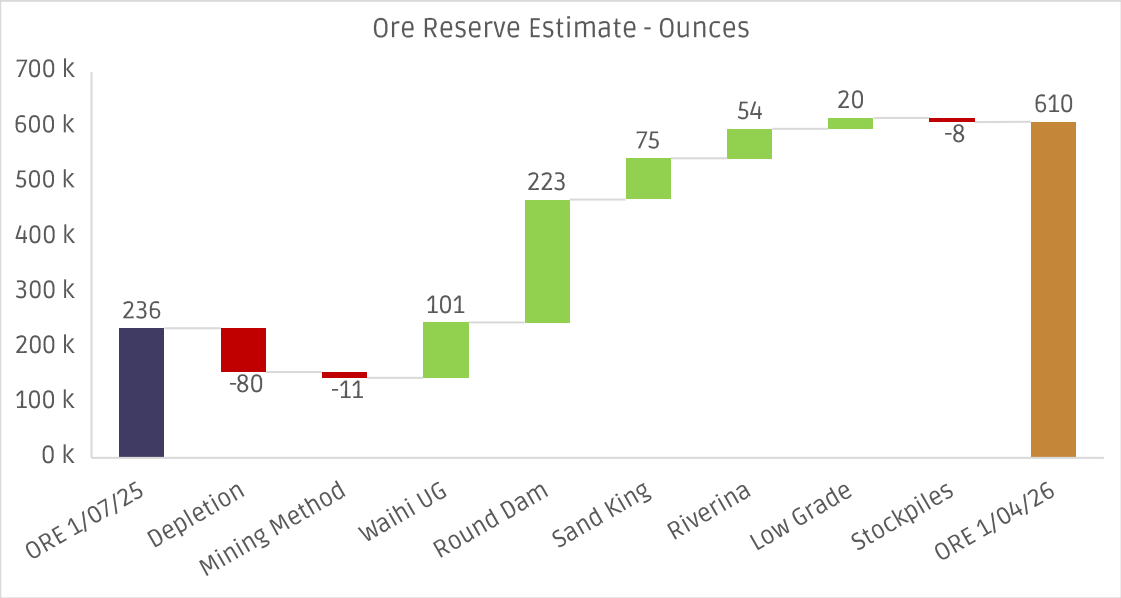

Figure 4 - Change to Company Ore Reserve ounces - 1 July 2025 to 1 April 2026

ORE - 1 July 2025	**236 Koz**	
Material Ounce Changes attributable to:		
Depletion	- 80 Koz	1 July 2025 ORE Material mined from Sand King and Riverina Underground mines between 1 July 2025 and 1 April 2026.
Mining Method	- 11 Koz	The Waihi open pit ORE was reduced 11 Koz as the north pit has been replaced by underground mining method in Waihi underground. The Waihi Central pit remains.
Waihi UG	+ 101 Koz	Further drilling down dip of Waihi and along strike of the Golden Pole mineralisation has increased the MRE and as such a Maiden underground mine ORE was announced to the ASX on 18 May 2026.
Round Dam	+ 223 Koz	Exploration targeting advanced to resource drilling on a 3.5km strike section of the Round Dam mineralised trend. Resulting in a significant 1.3 M oz MRE and five pits for a 223 Koz maiden ORE announced on 18 May 2026.
Sand King	+ 75 Koz	Infill down dip and northern extensional drilling at Sand King has increased the ORE. The grade has maintained at 3.2 g/t with the cut-off grade decreasing from 2.5 g/t to 2.4 g/t. The modifying factors stope dilution has increased from 5% to 10% and recovery unchanged.
Riverina	+ 54 Koz	Infill down dip drilling at Riverina has increased the ORE post depletion. The grade has increased from 3.5 g/t to 3.7 g/t. Dilution and recovery modifying factors are unchanged. The cut-off grade increased from 2.4 g/t to 2.5 g/t.
Low Grade	+ 20 Koz	Increased Low grade due to a A$5,000/oz gold price and 0.5 g/t cut-off grade. Additional mines of Waihi and Round Dam
Stockpiles	- 8 Koz	Reduction in Stockpiles across the operations due to increased processing capacity from a third party over the nine month period.
ORE - 1 April 2026	**610 Koz**	

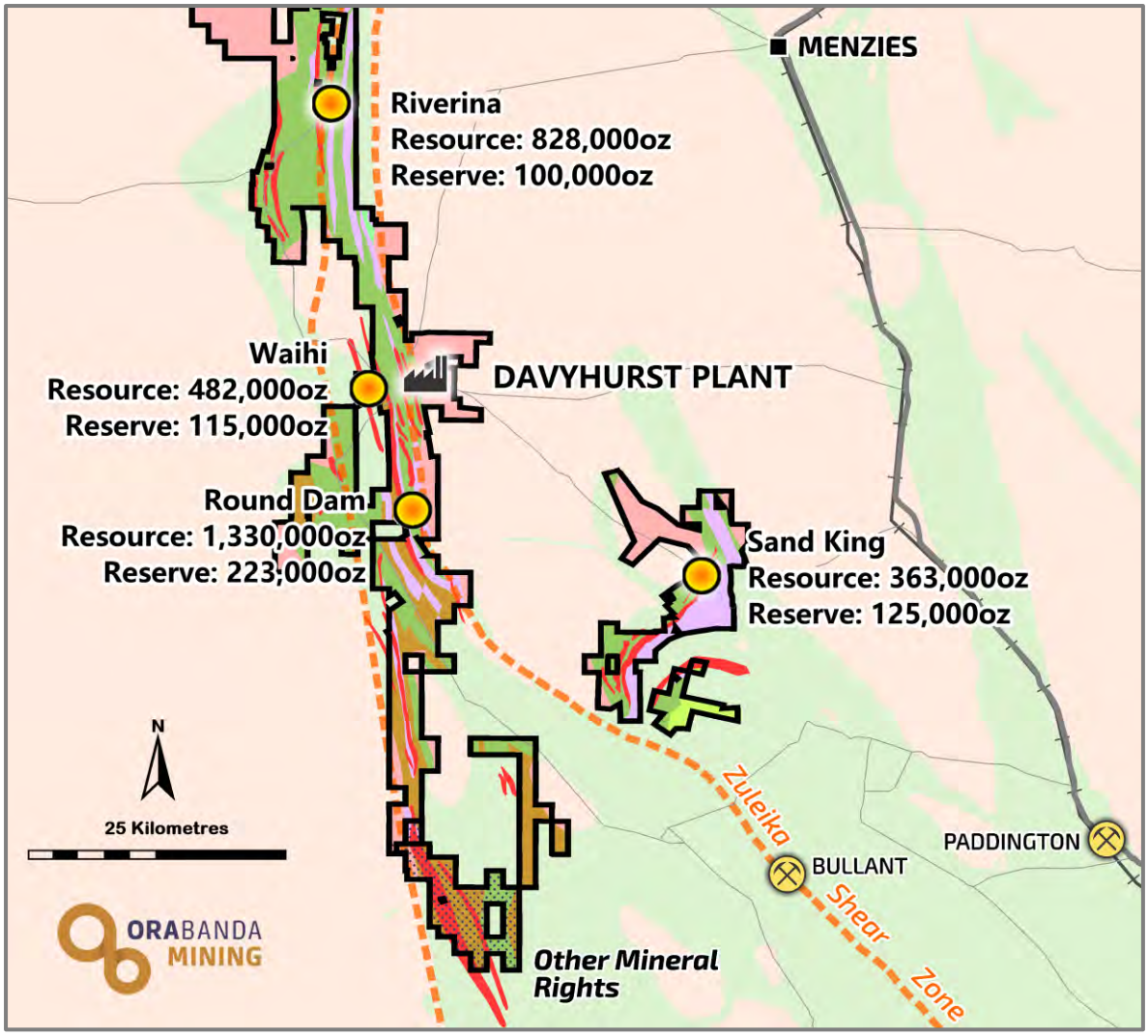

Figure 5 –Location of deposits with attributable Ore Reserves that are currently being mined or the subject of future development works

TOTAL MINERAL RESOURCE ESTIMATES

Table 5 - Total Mineral Resource Estimate by deposit

PROJECT		MEASURED			INDICATED			INFERRED			TOTAL MATERIAL		
		('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
LIGHTS OF ISRAEL		-	-	-	74	4.3	10	180	4.2	24	254	4.2	34
MAKAI SHOOT		-	-	-	1,985	2.0	128	153	1.7	8	2,138	2.0	136
	Open Pit	-	-	-	224	2.3	16	1	1.0	0	225	2.3	16
WAIHI	Underground	-	-	-	3,833	2.2	268	3,207	1.9	197	7,040	2.1	466
	TOTAL	-	-	-	4,057	2.2	285	3,208	1.9	197	7,265	2.1	482
Central Davyhurst Subtotal		**-**	**-**	**-**	**6,116**	**2.1**	**423**	**3,541**	**2.0**	**230**	**9,657**	**2**	**652**
LADY GLADYS		-	-	-	1,858	1.9	114	190	2.4	15	2,048	1.9	125
	Open Pit	476	1.7	26	2,118	1.6	106	117	1.5	6	2,711	1.6	138
RIVERINA AREA	Underground	396	3.2	41	4,182	2.3	311	4,151	2.5	338	8,729	2.5	689
	TOTAL	872	2.4	68	6,300	2.1	417	4,268	2.5	343	11,440	2.3	828
	Open Pit	-	-	-	386	1.6	20	17	1.6	1	403	1.6	21
BRITISH LION	Underground	-	-	-	36	3.2	4	3	3.8	0	39	3.2	4
	TOTAL	-	-	-	422	1.7	23	20	2.0	1	442	1.7	25
	Open Pit	-	-	-	-	-	-	691	1.5	33	691	1.5	33
FOREHAND	Underground	-	-	-	-	-	-	153	2.5	12	153	2.5	12
	TOTAL	-	-	-	-	-	-	844	1.7	46	844	1.7	46
	Open Pit	-	-	-	-	-	-	127	2.3	9	127	2.3	9
SILVER TONGUE	Underground	-	-	-	-	-	-	77	4.5	11	77	4.5	11
	TOTAL	-	-	-	-	-	-	204	3.1	21	204	3.1	21
SUNRAYSIA		-	-	-	175	2.1	12	318	2.0	20	493	2.0	32
Riverina-Mulline Subtotal		**872**	**2.4**	**68**	**8,755**	**1.9**	**566**	**5,844**	**2.4**	**446**	**15,471**	**2.2**	**1,075**
	Open Pit	-	-	-	-	-	-	-	-	-	-	-	-
SAND KING	Underground	339	2.8	31	2,110	2.8	192	1,439	3.0	140	3,888	2.9	363
	TOTAL	339	2.8	31	2,110	2.8	192	1,439	3.0	140	3,888	2.9	363
	Open Pit	-	-	-	-	-	-	-	-	-	-	-	-
MISSOURI	Underground	-	-	-	464	3.4	51	246	4.9	39	710	3.9	89
	TOTAL	-	-	-	464	3.4	51	246	4.9	39	710	3.9	89
PALMERSTON / CAMPERDOWN		-	-	-	118	2.3	9	174	2.4	13	292	2.4	23
BLACK RABBIT		-	-	-	-	-	-	434	3.5	49	434	3.5	49
Siberia Subtotal		**339**	**2.8**	**31**	**2,692**	**2.9**	**252**	**2,293**	**3.3**	**241**	**5,324**	**3.1**	**524**
	Open Pit	-	-	-	241	3.7	29	28	1.6	1	269	3.5	30
CALLION	Underground	-	-	-	255	6.0	49	156	5.5	28	411	5.8	77
	TOTAL	-	-	-	496	4.9	78	184	4.9	29	680	4.9	107
Callion Subtotal		**-**	**-**	**-**	**496**	**4.9**	**78**	**184**	**4.9**	**29**	**680**	**4.9**	**107**
WALHALLA	Open Pit	-	-	-	4,921	2.0	313	15,559	1.7	830	20,480	1.7	1,142
SALMON GUMS	Open Pit	-	-	-	2,231	1.3	95	2,640	1.1	93	4,871	1.2	188
	TOTAL	-	-	-	7,152	1.8	408	18,199	1.6	924	25,351	1.6	1,330
Round Dam Subtotal		**-**	**-**	**-**	**7,152**	**1.8**	**408**	**18,199**	**1.6**	**924**	**25,351**	**1.6**	**1,330**
Davyhurst Total		**1,200**	**2.6**	**99**	**25,200**	**2.1**	**1,726**	**30,100**	**1.9**	**1,870**	**56,500**	**2.0**	**3,690**

Notes:

1. Riverina, British Lion, Callion, Forehand and Silver Tongue Open Pit Mineral Resource Estimates are reported within a A$2,400/oz pit shell above 0.5 g/t. The British Lion, Missouri, Callion, Forehand and Silver Tongue Underground Mineral Resource Estimates are reported from material outside a A$2,400 pit shell and above 2.0 g/t. Round Dam Open Pit Mineral Resource Estimate is reported above 0.3g/t cut-off inside an optimised A$5,000/oz reporting shell. Waihi Open Pit is reported from Waihi Central within a 2023 pit design shell at a 0.5 g/t cut-off grade. Riverina Underground Mineral Resource Estimates are reported from fresh material below the A$2,400/oz pit shell within ASD solids of dimensions 10 m x 10 m x 1.6 m minimum width at a diluted cut-off grade of 0.8 g/t. Sand King Underground Mineral Resource Estimates are reported from fresh material below 350mRL (base of open pit) within ASD solids of dimensions 10 m x 10 m x 1.6 m minimum width at a diluted cut-off grade of 0.8 g/t. Waihi Underground Mineral Resource Estimates are reported from fresh material within ASD solids of dimensions 10 m x 10 m x 1.6 m minimum width outside the 2023 pit design shell at a diluted cut-off grade of 0.8 g/t.
2. Resources are inclusive of in-situ ore reserves and are exclusive of surface stockpiles.
3. The values in the above table have been rounded.

COMPETENT PERSONS STATEMENTS

Ore Reserves

The information in this announcement that relates to the underground Ore Reserves for Riverina, Sand King, Waihi and stockpiles is based on, and fairly and accurately represents, information and supporting documentation compiled by Mr Leroy Savage, who is an employee of Ora Banda Mining Limited, and has sufficient relevant experience on matters relating to mine design, mine scheduling, mining methodology and mining costs. Mr Savage is a member of the Australian Institute of Mining and Metallurgy. Mr Savage consents to the inclusion in the announcement of the matters based on his information in the form and context in which it appears.

The information in this report that relates to the open pit Ore Reserves for Waihi and Round Dam is based on, and fairly and accurately represents, information and supporting documentation compiled by Mr Geoff Davidson, who is a mining engineering consultant and employed by Mining and Cost Engineering Pty Ltd, and has sufficient relevant experience to advise Ora Banda Mining Limited on matters relating to mine design, mine scheduling, mining methodology and mining costs. Mr Davidson is a Fellow member of the Australian Institute of Mining and Metallurgy. Mr Davidson currently holds shares in Ora Banda purchased independently of the company. Mr Davidson consents to the inclusion in the announcement of the matters based on his information in the form and context in which it appears

Mineral Resource

The information in this announcement that relates to the Round Dam, Waihi, Sand King and Riverina Mineral Resources is based on, and fairly and accurately represents information and supporting documentation compiled under the supervision of Mr Ross Whittle-Herbert, an employee of Ora Banda Mining Limited, who is Member of the Australian Institute of Geoscientists. Mr Whittle-Herbert has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Whittle-Herbert consents to the inclusion in the announcement of the matters based on his information in the form and context in which it appears.

The information in this announcement that relates to the:

- Missouri Mineral Resource estimate is extracted from the ASX announcement titled "Mineral Resource and Ore Reserve Statement" dated 2 July 2024
- Forehand, Silver Tongue & British Lion Mineral Resource estimate is extracted from the ASX announcement titled "Davyhurst Gold Project Mineral Resource and Ore Reserve Statement" dated 29 July 2021;
- Callion Mineral Resource estimate is extracted from the ASX announcement titled "Maiden Callion Underground Resource of 77,000 oz" dated 29 June 2020;

each of which is available to view at asx.com.au. The Company confirms that it is not aware of any new information or data that materially affects the information included in the original market announcement and that all material assumptions and technical parameters underpinning the estimates in the relevant market announcement continue to apply and have not materially changed. The Company confirms that the form and context in which the Competent Person's findings are presented have not been materially modified from the original market announcement.

The information in this announcement that relates to Mineral Resources other than those listed above is extracted from the Swan Gold Mining Limited Prospectus released to the market on 13 February 2013. These Mineral Resources were first reported in accordance with the JORC 2004 Code and have not been updated to comply with JORC Code 2012 on the basis that the information has not materially changed since it was last reported. The Company is not aware of any new information or data that materially affects the information in that Prospectus and confirms all material assumptions and technical parameters underpinning the estimates continue to apply and have not materially changed.

FORWARD-LOOKING STATEMENTS

This announcement contains forward-looking statements which may be identified by words such as "forecast", "guidance", "target", "outlook", "estimates", "believes", "expects", "anticipates", "intends", "may", "will", "would", "could", or "should" and other similar words that involve risks and uncertainties. These statements are based on an assessment of present economic and operating conditions, and on a number of assumptions regarding future events and actions that, as at the date of this announcement, are expected to take place.

Such forward-looking statements are provided as a general guide only, are not guarantees of future performance and involve known and unknown risks, uncertainties, assumptions and other important factors, many of which are beyond the control of the Company, the Directors and management of the Company. When forecasting or providing guidance on costs and production the Company has taken into account current operating costs, design, plans for the mine, cost escalation, required personnel numbers and inputs including capital estimates, submitted tender rates from contractors and

suppliers, and average industry productivity and mining specification metrics. These and other factors could cause actual results to differ materially from those expressed or implied in any forward-looking statements.

The Company has no intention to update or revise forward-looking statements, or to publish prospective financial information in the future, regardless of whether new information, future events or any other factors affect the information contained in this announcement, except where required by law (including the ASX Listing Rules).

The Company cannot and does not give assurances that the results, performance or achievements expressed or implied in the forward-looking statements contained in this announcement will actually occur and investors are cautioned not to place undue reliance on these forward-looking statements.

Abbreviations

The following abbreviations are used in this report unless otherwise defined within the body of the report and which are specific to the relevant technical discussion in which they are used.

Abbreviation	Definition
ASD	Auto Stope Designer
CIL	Carbon in Leach
COG	Cut-off grade
DGP	Davyhurst Gold Project
DMPE	The Department of Mines, Petroleum and Exploration
HV	High voltage
mbs	Metres below surface
MDCP	Mine Disturbance and Closure Plan
MRE	Mineral Resource Estimate
NSR	Net Smelter Return
OBM, Ora Banda or Company	Ora Banda Mining Limited and its subsidiaries
ORE	Ore Reserve Estimate
RoM	Run of Mine
RESCAT	Resource classification category
RL	Reduced level
SO or MSO	Stope Optimiser/Mineable Shape Optimiser
TSF, IPTFS	Tailings Storage Facility, In Pit Tailings Storage Facility
WRL	Waste Rock Landform

Asset Fundamentals

The Davyhurst Gold Project area has over 140 km of combined strike of mineralised trends inside a 1,135 km^2 tenement package (Figure 6). The tenements cover highly prospective ground at the convergence of two regionally significant, deep-seated structures, the Zuleika Shear and the Ida Fault. Ora Banda Mining (OBM) is the registered holder to 37 Mining Leases, 21 Exploration Licences, 14 Prospecting Licences, 36 Miscellaneous Licences and 4 General Purpose Leases.

Gold ore is treated at its 1.2 Mtpa centrally located Davyhurst processing facility. This facility is supported by multiple workshops and stores along with administration offices. A 7.5 MW gas power station provides power for the Davyhurst central hub and is supported by a connection to mains grid power. Two villages are established: the Davyhurst Village with 387-person capacity and the Riverina Village with 220-person capacity. Support infrastructure includes several bore fields and pipelines, haul roads, access to nearby airstrips, two TSF cells along with in pit storage (IPTSF) with +5 years capacity. Both Riverina and Siberia have established mine site offices and workshops.

Location

OBM's Davyhurst Gold Project is in the eastern goldfields, 125 km from Kalgoorlie via roads, 67 km sealed road to Ora Banda and 58 km of unsealed public and private haul roads. The tenement package extends from 44 km north of Coolgardie at the southern extent to 20 km north of Menzies at the northern extent. The tenements are well connected with rural roads from Coolgardie,

Menzies, Ora Banda and Canegrass with most roads established from the 1890 to early 1900's gold rush.

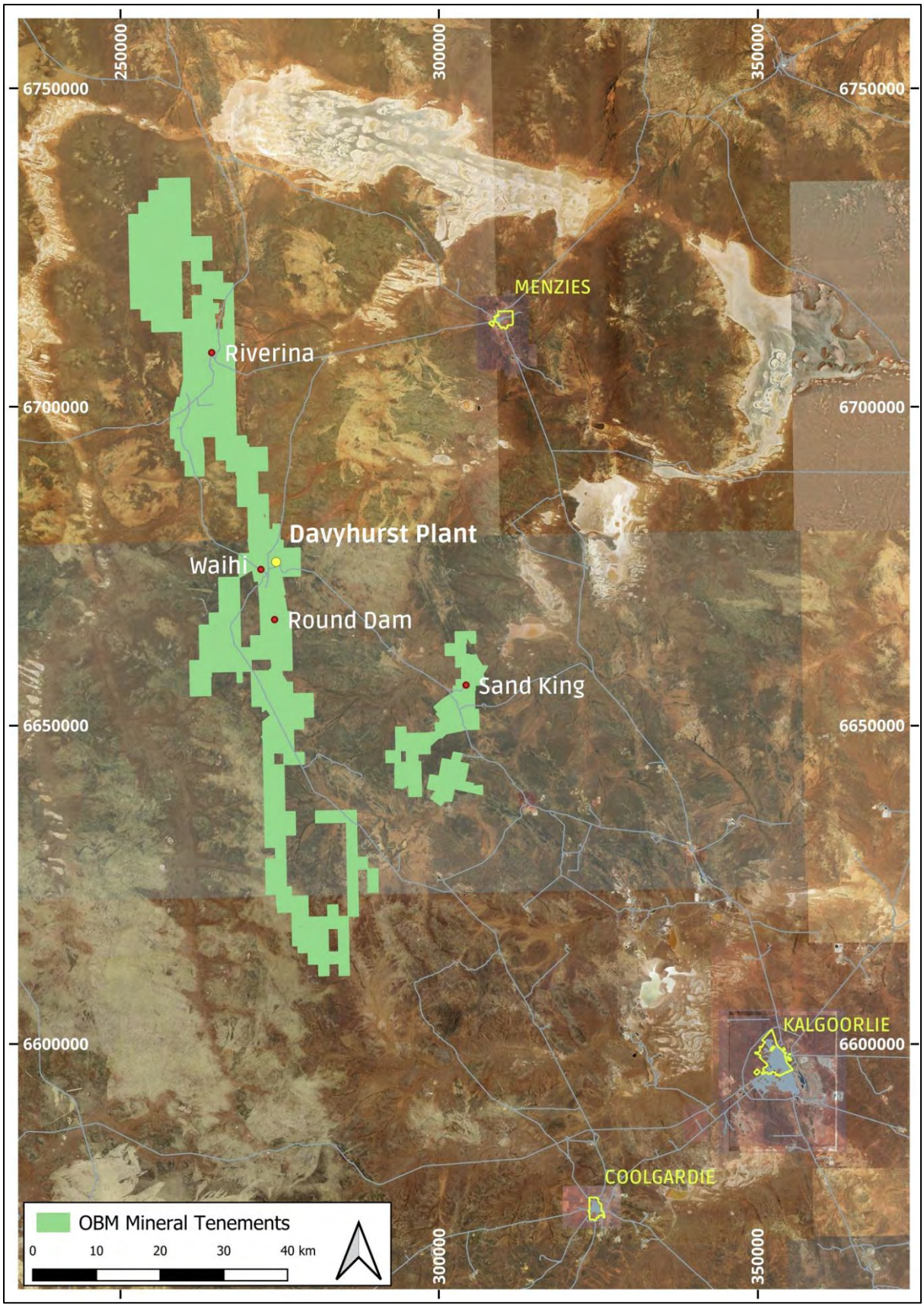

Figure 6 - Regional map, OBM Mineral Tenements and ORE deposits

SAND KING RESOURCE AND RESERVE

SUMMARY

Sand King MRE increased by 4% to 363 Koz. Material in the Measured and Indicated categories increased by 27% to 223 Koz from 176 Koz, result of UG drilling focussed on resource conversion. Between July '25 and 1 April '26 321 kt at 3.3g/t for 34 Koz of ORE material were mined, representing the depletion in Figure 7. The reconciliation to the ORE for the July '25 to April '26 period shows a 7% positive grade reconciliation. Geological drilling and mining have improved the orebody knowledge and as a result contributed to the 75 Koz of growth to the ORE resulting in an increase of 41 Koz (49%) after depletion.

A summary of the Sand King Mineral Resource and Ore Reserve as at 1 April 2026 are shown in Table 6 and Table 7.

Table 6 - Sand King Gold Project Mineral Resource Estimate

SAND KING GOLD PROJECT MINERAL RESOURCE ESTIMATE:												
	MEASURED			INDICATED			INFERRED			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
OPEN PIT	-	-	-	-	-	-	-	-	-	-	-	-
UNDERGROUND	339	2.8	31	2,110	2.8	192	1,439	3.0	140	3,888	2.9	363
TOTAL	**339**	**2.8**	**31**	**2,110**	**2.8**	**192**	**1,439**	**3.0**	**140**	**3,888**	**2.9**	**363**

Table 7 - Sand King Gold Project Ore Reserve Estimate

SAND KING GOLD PROJECT ORE RESERVE ESTIMATE:									
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	194	2.9	18	1,042	3.2	107	1,236	3.2	125
LOW GRADE[6]	-	-		172	1.3	7	172	1.3	7
TOTAL	**194**	**2.9**	**18**	**1,214**	**2.9**	**114**	**1,408**	**2.9**	**132**

6 Insitu material

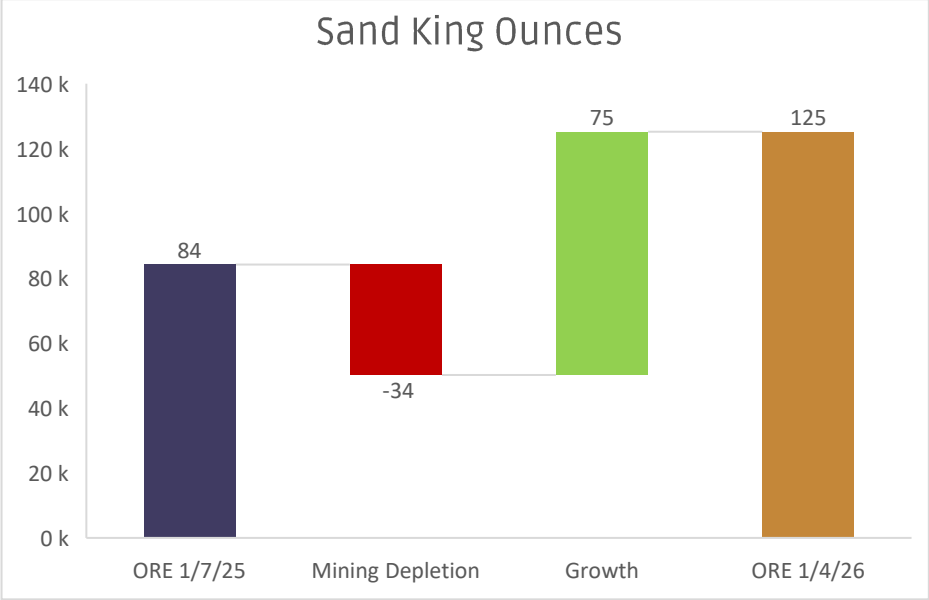

Figure 7 - Change in Sand King ORE ounces

INTRODUCTION

Tenement

The Sand King deposit is located on the granted mining tenement M24/960, which is 100% owned by Siberia Mining Corporation Pty Ltd, a wholly owned subsidiary of Ora Banda Mining Limited. OBM holds rights to gold and its byproducts over all this tenement. There are no known heritage or native title issues. The tenement is in good standing with no known title risk. Tenement M24/39 is held by Robert Gardner, and Gardner granted Siberia the right to explore for Gold Minerals (gold and silver mineralisation in any form) (entire tenement). In relation to the "Reduced Area", Siberia has continued exclusive and overriding rights to carry out exploration and mining operations. Robert Gardner has priority of rights over the "Remaining Area" of M24/39. Various infrastructure is in place or planned in the M24/39 tenement including haul roads, an open pit ramp, a section of decline and a WRL.

Permits and Licenses

The required environmental approvals to operate the Sand King Underground mine are in place:

- Siberia Gold Operations Mining Proposal Amendment (Reg Id 500381)
- Siberia Gold Operations Mine Closure Plan for Mining Proposal (Reg Id 121808)
- Mine Dewatering Works approval number W6904/2024/1
- Clearing Permit 6968/4
- Prescribed Premise Licence L3017/2025/1

The operations remain compliant with all the current permitting requirements, and as such they remain in full force. A rehabilitation obligation remains at Siberia post open pit mining.

Mine Infrastructure

The Siberia Gold Operation is an established mining centre with extensive offices, workshops and communications. ROM pads, waste rock landforms and haul roads are established along with bore fields and water storage dam and pits. The facilities are sufficient for operation of the Ore Reserve mine design. The mine is located in the Siberia Gold Operation 37 km to the southeast of Davyhurst processing facility

The Sand King underground mine commenced in August 2024, establishing declines, rises, ventilation and escapeway infrastructure. Seven production levels have been accessed up to 1 April 2026 with development and stoping ongoing. A 5 MW diesel power station supplies HV power via a service hole to underground substations and distribution network. A dewatering capacity of 30 l/s is currently in place along with 3,265 ML in nearby pit storage capacity. Permitted waste rock storage capacity remains as well as pit backfilling opportunities.

The Davyhurst village is 35 km from the mine offices with a capacity of 387 rooms.

The Davyhurst processing facility is located 37 km via well-established public and private roads to the northwest of Siberia. Road trains are used to haul ore from the mine ore pad at Sand King to the Davyhurst RoM pad.

MINERAL RESOURCES

Mineral Resource Estimation: Summary Information as required under Australian Securities Exchange (ASX) Listing Rule 5.8.1 follows.

GEOLOGY & GEOLOGICAL INTERPRETATION

Lithology

Mafic rocks of the Siberia area have been assigned to the Wongi and Missouri Basalt Units of the Pole Group, while the ultramafics to their south and east are assigned to the Walter Williams Formation. Gold mineralisation associated with the Sand King deposit is hosted entirely within Missouri basalt, immediately west of the boundary with the komatiite-dominated Walter Williams Formation. Within the Missouri Basalt are two distinct units, a pillowed unit and a younger feldspar phyric, columnar jointed unit. Stratigraphic layering in the Siberia area strikes NE-SW and dips moderately towards the south-east and forms part of the western limb of the regional-scale Kurrawang Syncline. Numerous examples of younging direction in pillows are observable in the pit. The pillowed unit is more massive (competent) than the columnar basalt and is the preferred host for gold mineralisation. Two narrow interflow sediments and two narrow ultramafic units with limited continuity have been observed in core logging within the mafic package. A thin dolerite is also present.

Aplite dykes form a NE-trending, NW dipping dyke swarm that cuts both the western and eastern units of the Missouri Basalt. The dykes are up to 5 m thick. The composition of the dykes is probably equivalent to that of monzogranite. Aplite dykes predate mineralisation and are occasionally mineralised where proximal to mineralised structures.

Structure

There are several structural styles and orientations associated with Sand King gold mineralisation. The current structural history includes development of early conjugate, ductile shear structures striking ~010° and 330° and dipping moderately to the east. Subsequently brittle tension veins

striking 060° and 090° developed and introduced the bulk of the gold mineralisation. An additional set of tension veins oriented 165° has been recently identified in the northern part of the mine.

Kinematics show dextral movement on the 010° and sinistral movement on the 330° shears. 010° shears are frequently exploited by the later aplite dykes. Shears are sometimes quartz filled with weak boudinage and sometimes dry with no observable quartz or alteration. Quartz deposition and gold precipitation at Sand King is dominantly associated with later tension veins in either 060° or 090° orientation and dipping steeply north. 060° striking veins tend to have the greatest continuity while the 090° veins tend to form linking structures between the 060° veins and have shorter continuity. Movement along the tension vein structures is primarily strike-slip, supported by sub-horizontal slicken lines on exposed planes. Later dextral movement along 060° tension veins is evident, and an extreme example is in the north-east of the pit. Here shearing has formed en-echelon quartz arrays. Tension vein mineralisation presents as linear en-echelon veins, sigmoidal vein arrays and laminated quartz veins.

When the tension veins intersect the 330° and 010° shears the ore bearing fluids migrate up and down the shear, causing grade and volume "blowouts". The intersection of the steep north dipping tension veins with the moderate east dipping 330° and 010° shears give a steep north plunge to the high-grade blowouts. The blowouts form pipe-like features.

Syn to late breccia structures strike 110° and dip moderately north. These lodes feature distal carbonate alteration, with the main Husky structure centrally silicified. Bonanza-grade hits associated with the Husky breccia indicate a late mineralisation event, aligned with 060 lode stress orientations, where gold endowment depends on local structural traps rather than the biotite-silica-sulphide alteration and chemical controls typical of 060 and 090 lodes. The high-grade mineralisation tends to be highly discontinuous, with bonanza-type grades seen in drilling, interpreted to be associated with the intersection of 060 and 090 lodes with the breccia.

Alteration & Mineralisation

There are three alteration events at Sand King, including an initial pervasive greenschist alteration event related to regional metamorphism, a hydrothermal alteration event related to typical gold mineralisation and a later event related to the breccia structures where gold could have been introduced and/or remobilised. Gold mineralisation typically occurs in a series of quartz veined, biotite-albite-calcite-pyrite-pyrrhotite lodes. Typically, the lode alteration extends for only 1-1.5 m away from the quartz veining although at times, zones of alteration up to 5m from veining have been noted. Pyrite is the dominant sulphide as disseminations in wall rock and clusters within veins. Pyrrhotite (FeS) is noted to replace pyrite (FeS_2), infilling pressure shadows around pyrite euhedra. This suggests an evolution of the mineralising hydrothermal fluid from a S_2 rich to S_2 depleted composition. Other sulphide minerals, observed in hand specimen and/or polished thin sections include, galena, altaite (Pb telluride), chalcopyrite, molybdenite, Ilmenite, bismuth tellurides and sphalerite with arsenopyrite notably absent. Tungsten, in the form of scheelite is commonly present.

Weathering

The oxidation profile at Sand King is also thin (<20 m) outside the main deformation corridor that hosts mineralisation. Within the mineralised corridor weathering extends to approximately 40 m below surface at which point the transition to unweathered material occurs over an average distance of 20 m.

DRILLING AND SAMPLING, AND SAMPLE ANALYSIS TECHNIQUES

Modern exploration in the Siberia area commenced in the 1980s by Western Mining Corporation (WMC) and was followed by numerous operators who held the tenure for various periods. Although a significant proportion of drilling data is from previous operators, it is generally well documented and to industry standards of the time. In addition, OBM has added significant drilling to the Siberia deposits. All RC and diamond drilling at the deposit is deemed suitable for resource estimation purposes.

Previous operators include WMC, Gilt-Edged Mining, Gold Fields Ltd, Siberia Mining Corporation (SMC), Monarch Gold Ltd and Eastern Goldfields (EGS).

RC drilling was completed by all operators. Hole diameters for WMC, Gilt-Edged Mining and Gold Fields Ltd are unknown. All other operators drilled either 4 inch (Monarch Gold) or >5-inch diameter holes (Ora Banda). Diamond core holes were generally HQ or NQ diameter, though WMC drilled some BQ diameter holes. Diamond core by WMC was not oriented, other operators oriented the core. Collar locations were surveyed by various contractors and methods including theodolite (WMC), Differential GPS (Gilt-Edged Mining, GoldFields Ltd, SMC, EGS) and RTKGPS (Monarch Gold, OBM). Underground diamond collars are surveyed by mine surveyors.

RC holes by WMC were generally not downhole surveyed. RC holes by other operators were downhole surveyed by magnetic methods such as Eastman single shot or electronic multi shot. Early diamond holes by WMC were downhole surveyed by Eastman single shot or multi-shot camera approximately every 30 m. Later operators surveyed RC holes with electronic multiple shot, Eastman single shot (SMC, EGS) or Gyro (OBM). Diamond holes by more recent operators (Siberia Mining Corporation - Ora Banda) were north seeking gyro surveyed. Underground GC holes are downhole surveyed by Devi rate gyro.

All RC grade control holes drilled by OBM were surveyed by the mine surveyor and downhole surveyed by rig north seeking gyro.

Percussion samples were generally collected at 1 m intervals, split in the field, generally using a riffle splitter to produce a 2-3 kilogram subsample. Some operators composited the 1 m samples to either 2 m, 4 m or 5 m intervals using a spear or scoop to sample from the split reject. The bagged, split 1 m samples were submitted for assay if anomalous composite assay results were returned. Core was generally cut in half and sampled at geological boundaries (Gold Fields Ltd, OBM) or 1 m intervals (SMC). RC samples from Delta Gold were collected through a cyclone in large plastic bags at 1 m intervals. Underground GC core was sampled to geological boundaries with a minimum sample length of 0.3 m. GC core was whole core sampled. All drill holes were logged by qualified geologists.

OBM RC drill sample recovery is monitored and visually checked for recovery, moisture and contamination. RC sample weights were recorded at the laboratory and monitored.

Historical QAQC protocols used by companies prior to Gilt Edged Mining's ownership have not been documented in any detail. Gilt Edged Mining routinely used standards, field duplicate samples and check analyses at a second laboratory to monitor analytical quality. SMC used standards and field duplicates (1 in 20) during drilling campaigns to provide a reference material to monitor laboratory performance. Monarch Gold submitted Certified Reference Material every 20th sample in both RC drilling programmes. Duplicate samples were submitted every 25th sample for RC drilling. The protocol adopted by OBM required CRM standards and blanks be inserted every 25 samples for RC and diamond drilling. The frequency rate of duplicate samples was nominally 1 every 25 m. Underground diamond drilling and face CRM standards and blanks were inserted at a rate of 1:20.

Post the 2025 MRE Ora Banda completed 181 UGGC holes (31,597 m) and sampling of 670 faces (2,917 m). This significant program of drilling and face sampling is included in the current MRE.

Sample Analysis Methods

All WMC samples were analysed at the WMC exploration division laboratory by 25g Aqua Regia with AAS finish. Gilt Edged mining analysed composite samples by MinLab, Kalgoorlie using 25g Aqua Regia, AAS finish. Individual 1 m samples from composite results >0.2 g/t were submitted to Genalysis in Perth for fire assay with a 50 g charge. RC and diamond samples collected by Gold Fields Ltd were dried, crushed, split, pulverised and a 50 g charge taken for fire assay at Australian Laboratory Services in Kalgoorlie. All assaying by SMC was done by either SGS Analabs in Kalgoorlie or Ultratrace using a 50 g charge taken for fire assay. Monarch gold assayed by 50g fire assay with AAS finish. Samples were submitted to both ALS Laboratories and Ultratrace.

Eastern Goldfields utilised Intertek-Genalysis in Kalgoorlie, Kalassay in Kalgoorlie, SGS in Kalgoorlie and Nagrom Laboratories in Perth for sample analysis. A 50gm charge was taken and analysed by fire assay ICP-OES. Drilling completed in 2020 by Ora Banda utilised Nagrom Laboratories in Perth and SGS in Kalgoorlie for sample analysis. A 50 g charge was taken and analysed by fire assay ICP-OES. For 2023 and 2024 drilling Ora Banda utilised the SGS on-site facility for sample preparation with pulps sent to SGS in Kalgoorlie for analysis. A 50 g charge was taken and analysed by fire assay MP-AES. From September 2025 surface drill samples were sent to SGS on-site laboratory for crushing in orbis crushers and photon analysis in Kalgoorlie. Initial underground drilling and face sampling was assayed by SGS, Kalgoorlie by fire assay MP-AES. From December 2024 underground sample submissions were sent to SGS on-site laboratory for sample preparation (crushing in Orbis crushers) and transported to SGS Kalgoorlie for assay by Photon assay method. Transfer of analytical method from fire assay to Photon assay followed a program of comparison assaying whereby Photon assay analysis was done on the crush reject of samples already assayed by fire assay. Underground diamond core is predominantly whole core sampled.

ESTIMATION METHODOLOGY

All lode interpretations and block models were created in Sand King Mine Grid (SMG). This grid is rotated through 60° so that 060° (MGA) is 000° in SMG. 4000 m is added to AHD elevations. The block model was also prepared in SMG so that the long axis of blocks is parallel to the strike of the dominant mineralisation.

Ore lode interpretation was based on a ~1 g/t cut-off, determined from a log-probability of raw assays from resource drilling, and influenced by the presence and intensity of quartz veining and the dominantly biotite+sulphide rich alteration. Sub 1 g/t intervals were included in the interval selection if alteration was observed in core photos and logging. Typically, structural measurements of vein boundaries are used to get tension vein orientations and foliation measurements are used to determine shear orientations. Core photos are used extensively to assist the interpretation. Where tension veins interact with shears the width and tenor of mineralisation is often increased and core photos are used to assign portions of the intercepts to either shear or tension vein orientations.

High grade mineralisation on the Husky (Breccia), Pug (010°) and Wolfhound (330°) lodes is highly discontinuous and is interpreted to be coincident with cross-cutting tension vein structures. These domains have been sub-domained using the numeric modelling functionality in Leapfrog™. A structural trend has been created using the domain and cross-cutting solids and applied to the numeric model. High and low grade domains have been created for each parent domain, generally at a cut-off of 0.5 g/t Au and iso value of 0.3. This has resulted in significantly reduced smearing of grade in these domains and is believed to be representative of the grade distribution.

One metre composites were calculated from the raw assay data with a minimum length of 0.3 m. Residual intervals were distributed across the composited interval. Supervisor™ software was used to establish spatial grade continuity. Top cuts were applied to the composite data on a domain basis to reduce the influence of occasional extreme gold grades.

Block model block size is 4mE x 10mN x 10mRL (SMG) with sub-celling to 0.5mE x 0.625mN x 0.625mRL. Estimation was done into the parent blocks. Kriging Neighbourhood Analysis (KNA) was used to define the estimation neighbourhood parameters, including search distances, minimum and maximum samples and discretisation. Estimation was completed using three runs. Pass 1 was at the range of the variogram and passes 2 and 3 at twice and three times the variogram range respectively. Samples were set at a minimum of 10 and maximum of 30 samples for pass 1. Second and third passes have minimum samples of 6 applied with a maximum of 10 with slight variations for smaller domains. Search anisotropy was established from the geostatistical evaluation. Grade thresholds were used for certain lodes to limit the influence of high-grade composites at significant distances from the block being estimated. Grade thresholds are applied when distances exceed a given percentage of the search distance.

Oxidation was applied based in DTM surfaces defined from geological drill logs and observations of the pit walls. Values were applied according to oxidation state. Density values were established from 4,378 drill core measurements (water immersion method) and referencing historic results from bulk metallurgical samples. Densities are applied to mineralisation and waste. Waste densities are domained by lithology.

Surface topography was established by recent completion of mining pit surveys completed by the Mine Survey department and a regional Arvista survey completed in 2017.

Underground mining depletion is applied as at 1 April 2026 from solid wireframes produced by the mine survey department.

CRITERIA USED FOR CLASSIFICATION

Wireframe solids were constructed to encompass areas considered to adequately fulfil the requirement to be classified as either, Measured, Indicated or Inferred.

The classification criteria are as follows:

Measured resources are defined by volumes between two ore drives which have adequate face sampling and GC-spaced drilling.

Indicated resources are defined where there is reasonable confidence in the geological framework based on sufficient drilling to define geological and grade continuity. Indicated resources are defined by:

- Good support from drilling, averaging a nominal 30mE x 30mRL.
- Areas where the estimation quality is reasonable, assessing kriging slope.

Inferred resources are defined where there is a lower confidence in geological and grade continuity as defined by a lower concentration of drilling data. Inferred resources are defined by:

- Drill spacing is typically greater than 30mE x 30mRL up to a maximum of 60m x 60mRL.
- Areas where the estimation quality is lower, mainly assessing kriging slope.

CUT-OFF GRADES AND MODIFYING FACTORS

The Mineral Resources have been reported from fresh material at a diluted cut-off of 0.8 g/t Au inside Auto Stope Designer (ASD) derived solids with dimensions of 10mN x 10mRL and a minimum

width of 1.6 m. Individual ASD blocks were assessed and removed if above the 350RL (base of current as-mined pit).

ORE RESERVES

Material Assumptions and Outcomes, Criteria for Classification

The Ore Reserve was derived from technical studies incorporating project-specific costs as well as geotechnical analysis, dilution and recovery parameters and is based on the current 2026 MRE. Processing parameters were based on recent test work combined with historical recent processing recoveries. Hydrogeological conditions were determined from recent mining of the Sand King pit and underground, as well as information obtained from extensive Resource drilling.

Costs were derived from the FY26 budget estimate including contract pricing current at the date of this Ore Reserve. Unit costs for mining were estimated based on fully resourced contracted scope of work of which this Ore Reserve forms a portion. Unit costs for haulage, processing, site administration and head office overheads were calculated using the combined project cost model with the Ore Reserve mine schedules and stockpiles.

The Sand King Underground Ore Reserve was estimated using a gold price of A$2,500/oz.

The dilution skin method was employed to reflect the selective mining method proposed for Sand King Underground. Dilution parameters were based on a geotechnical assessment of the expected mining environment. A cut-off grade of 2.4 g/t was applied to determine economic mining envelopes using Deswik™ ASD. Costs derived from the FY26 budget including contract pricing current at the time were used to validate the Ore Reserve cut-off grades.

Mining extraction ratios for the underground Ore Reserve are dependent upon the dimensions and spacing of pillars throughout the orebody. The Sand King mine design is based on open stopes of nominally 40 m along strike, though stope lengths vary where necessary to conform to orebody geometry and maximise extraction, with rib pillars of 5 m by 17.5 m maintained throughout. The 40 m stope strike extents are considered a practical distance over which to successfully operate remote loaders to recover ore from open stopes. Sill pillars have been considered via a stope recovery of 65% where stoping extends more than 4 levels down dip on a mineralised lode A 5% stope ore loss was also included for operational losses. The overall mining recovery was estimated to be 82%.

Mining Method

The underground mine design is premised on a conventional longhole open stoping mining method, commonly used in the Western Australian Goldfields.

Mining equipment will be mechanised, with equipment to include electric-hydraulic drills for development and production, and rubber tyred loaders and trucks for load and haul activities. Production loading will incorporate conventional and tele-remote loading for non-entry mining stopes.

Based on the geotechnical assessment, which identified favourable ground conditions and low stress environment, as would be expected at the shallow mining depths of no more than 250mbs, no stope backfill is contemplated.

Cut-off Grades

The Sand King cut-off grade was calculated to be 2.4 g/t for production stoping ore. The cut-off grade calculation was estimated at a gold price of A$2,500/oz, and is inclusive of mining, transport, processing, overheads, sustaining capital and royalties.

A cut-off grade of 2.0 g/t was applied to the underground development based on the incremental cost of developing hauling and processing of the ore. The calculation was estimated at a gold price of A$2,500/oz.

Low Grade insitu material is 0.6 g/t to 2.0 g/t, based on the surface SP cut-off where haulage, processing, admin costs are applicable and using a gold price of A$5,000/oz.

Recent Sand King mine contractor costs and OBM budget costings were used.

The WA state royalty of 2.5% NSR plus a 1%NSR Private company royalty apply.

Processing Method

The process for treating ore at the Davyhurst Gold Plant (DGP) is conventional CIL with some gold recovered via gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. The process plant has a nominal throughput rate of 1.2 Mtpa based on a grind size of 106 µm. The process plant has been successfully operated at this rate with recent improvements made. The processing recovery applied to Sand King Underground was 87% and was based on metallurgical test work. The recovery performance was 92% through Davyhurst plant in FY26 to EOM March-26, processing Riverina and Sand King ores which have an average metallurgical test work recovery of 88%.

Estimation Methodology, and Modifying Factors

Given the nature of the mineralisation, the global dilution, inclusive of stoping and ore drive development, equates to 23% of material. Background grades were estimated into the block model and were included in the dilution modelling. Dilution grades varied between zero and 1.0 g/t depending on the nature of the alteration halo. The global average grade of dilution was estimated to be 0.25 g/t. Dilution being all included material less than 0.6 g/t.

Delineation of economic stoping areas was completed using Deswik™ software. Mineable “stope” shapes were created to simulate fully diluted stope blocks. The stope shapes are then depleted by development ore drives and modifying factors are applied in the mine schedule. Stope selection was optimised using a cut-off grade of 2.4 g/t.

A minimum stope mining width of 1.6 m was applied in the dilution modelling process, with an additional 0.6 m dilution skin applied to all valid stope shapes (0.3 m hanging wall and 0.3 m footwall). In addition, a nominal provision for unplanned dilution of 10% @ 0 g/t was also included as a contingency to all stoping panels.

Inferred material was not considered in defining the stoping envelopes; however, due to practical mining geometries a small portion of incidental Inferred material is included within the Underground Ore Reserve. This material occurs at the edges of the mining envelope and is estimated at approximately 63 kt at a grade of 1.9 g/t, representing 3% of the Sand King Underground Ore Reserve ounces and is not relied upon for economic extraction. The incidental Inferred inventory was not considered material to the economics of the project. The RESCAT for each scheduled task was attributed with the RESCAT of the dominant mass of material above 0.6 g/t.

The economic viability of the Sand King Underground was confirmed using current commercial parameters in a project evaluation cash flow model inside the greater multiple mine company model. This model also considered project phasing, stockpiling, sustaining capital and the effect of fixed costs. The cash flow modelling was based on a gold price of A$3,600/oz. The mine demonstrated a positive net cash flow with acceptable returns. Overall unit mining costs for the underground was estimated to be A$149/t ore, inclusive of sustaining capital.

Mine Design

The mine design for the Sand King Underground on which this Ore Reserve was based is shown in Figure 8. The mine entries consist of a main access portal and primary ventilation portal. Both are located in the fresh rock portion of the existing Sand King pit.

The primary ventilation is via a vent portal to the Sand King open pit. Return air drives are designed 5 m x 5 m with vertical rises ~6 m x 4 m. The system can meet the demand at various stages of mine life including the Ore Reserve design and schedule.

Underground pump stations are in place and have been allowed for in the design. Mine dewatering is further pumped 500 m to a water storage pit with 175,000 kl capacity. Dewatering pipelines are capable of 40 l/s and pumps to suit demand.

The decline is 5.5 m wide x 5.7 m high with a typical gradient of 1:7. Ore drives are designed to be 4.5 m wide x 4.5 m high. The average floor to floor slope distance between levels is set at 22 metres, with an average stope panel height of approximately 17.5 metres. Stope parameters used in the Sand King mine design are shown in Table 8.

The current Ground Control Management Plan provides stope and pilar analysis and guidance in line with the stope parameters used.

Table 8 - Sand King stope parameters

Stoping Parameters		
Sub-Levels	22	m
Stope Width	1.6	m
Dilution FW	0.3	m
Dilution HW	0.3	m
Stope Length	~40	m
Ave Stope Width	3.5	m
Pillar Width	5	m
Sil Pillar Recovery	65	%
Sil Pillar frequency	~88	m
COG	2.4	g/t
Schedule Dilution	10%	0g/t Dilution
Schedule Recovery	95%	

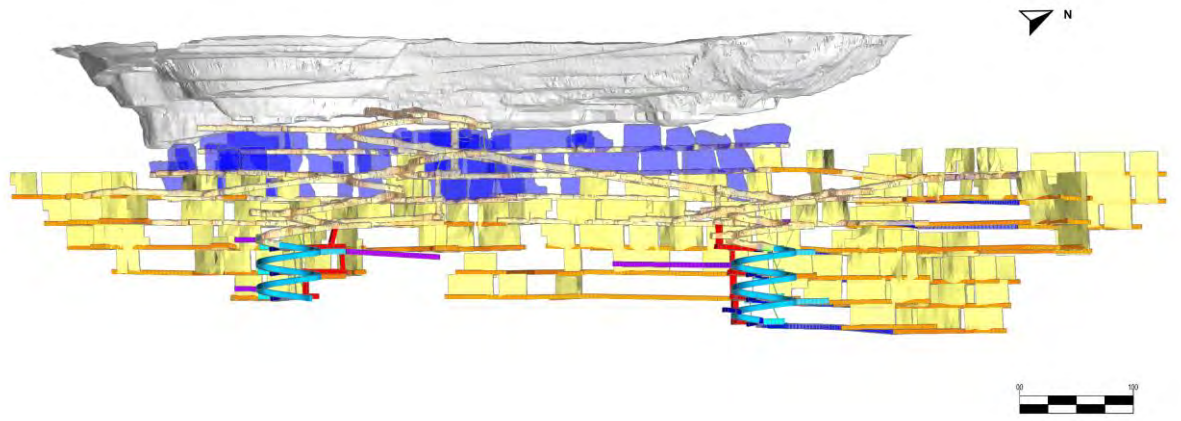

Figure 8 - Sand King Underground Ore Reserve mine design with Sand King pit (looking northwest)

Sand King Underground Mine Schedule

A mine schedule for the Sand King Underground Ore Reserve was developed, with productivity rate assumption in line with contractor expectations.

The mining sequence assumes top-down echelon mining with no current plans to backfill stopes.

The primary mining equipment levels on which the mine schedule was based are shown in Table 9. The ORE schedule was used in the economic assessment.

Table 9 - Sand King primary mining equipment levels

Equipment		
2x Jumbo	Sandvik DD421	Twin Boom
2x Long Hole Drill	Sandvik DL431	76mm holes
3-2x Loader	Cat 2900XE	17T
2-3x Truck	Sandvik TH663	60T

Economic Assessment

An economic assessment was carried on the Sand King Underground to validate the Ore Reserve Financials. The cash flow was modelled in real terms on a pre-tax basis. Recovery and revenue parameters used were as described above.

Costs were derived from the FY26 budget estimate including contract pricing current at the date of this Ore Reserve. Unit costs for mining were estimated based on fully resourced contracted scope of work.

Mining overheads were based on OBM budget provisions for supervision and technical support, as well as contractor fixed costs, general operating expenses, FIFO flights and accommodation. Dayworks provisions were also included for miscellaneous works during operations as well as closing of the site.

Unit costs for haulage, processing, site administration and head office overheads were calculated using the combined project cost model with the Ore Reserve mine schedules and stockpiles.

An allowance for capital has been used in the economic modelling and based on recent actuals and budget forecasts. The allowance covers:

- UG sub stations with HV cabling,
- Power station payments,
- Dewatering and mine water pipeline and pump stations,
- Escapeway ladders, and
- Primary ventilation controls and concrete works.

The ORE is based on a feasibility level of accuracy. A gold price of A$3,600/oz was used for financial assessment, and the competent person is satisfied that the mine demonstrated a positive net cash flow with acceptable returns.

Ore Reserve

On the basis of the outcomes of the analysis described above, the estimated economic mining inventory was classified as an Ore Reserve under the 2012 JORC code. All of the Ore Reserve Estimate was derived from the economic portion of the Measured & Indicated Mineral Resource. Measured Mineral Resource within the economic mining envelope was classified at Proved Ore Reserve Estimate. Indicated Mineral Resource within the economic mining envelope was classified at Probable Ore Reserve Estimate. Low grade was all classified as Probable Ore Reserve Estimate. The Ore Reserve is shown in Table 10.

Table 10 - Sand King Ore Reserve, as at 1 April 2026

	SAND KING GOLD PROJECT ORE RESERVE ESTIMATE:								
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	194	2.9	18	1,042	3.2	107	1,236	3.2	125
LOW GRADE[7]	-	-		172	1.3	7	172	1.3	7
TOTAL	**194**	**2.9**	**18**	**1,214**	**2.9**	**114**	**1,408**	**2.9**	**132**

7 Insitu material

RIVERINA RESOURCE AND RESERVE

SUMMARY

Riverina Underground MRE increased by 18% to 689 Koz. Material in the Measured and Indicated categories decreased by 5%, material in the inferred category increased by 55%. Between July '25 and 1 April '26 364 kt at 3.9 g/t for 46 Koz of ORE material were mined, representing the depletion in Figure 9. The reconciliation to the ORE for the July '25 to April '26 period shows a 6% positive grade reconciliation. Geological drilling and mining have improved the orebody knowledge and as a result contributed to the 54 Koz of growth to the ORE resulting in an increase of 8 Koz (9%) after depletion.

A summary of the Riverina Mineral Resource and Ore Reserve as at 1 April 2026 are shown in Table 11 and Table 12 respectively.

Table 11 - Riverina Gold Project Mineral Resource Estimate

RIVERINA GOLD PROJECT MINERAL RESOURCE ESTIMATE:												
	MEASURED			INDICATED			INFERRED			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
OPEN PIT	476	1.7	26	2,118	1.6	106	117	1.5	6	2,711	1.6	138
UNDERGROUND	396	3.2	41	4,182	2.3	311	4,151	2.5	338	8,729	2.5	689
TOTAL	**872**	**2.4**	**68**	**6,300**	**2.1**	**417**	**4,268**	**2.5**	**343**	**11,440**	**2.3**	**828**

Table 12 - Riverina Gold Project Ore Reserve Estimate

RIVERINA GOLD PROJECT ORE RESERVE ESTIMATE:									
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	103	4.0	13	741	3.6	87	844	3.7	100
LOW GRADE	-	-		208	1.3	9	208	1.3	9
TOTAL	103	4.0	13	**949**	**3.1**	**95**	**1,052**	**3.2**	**108**

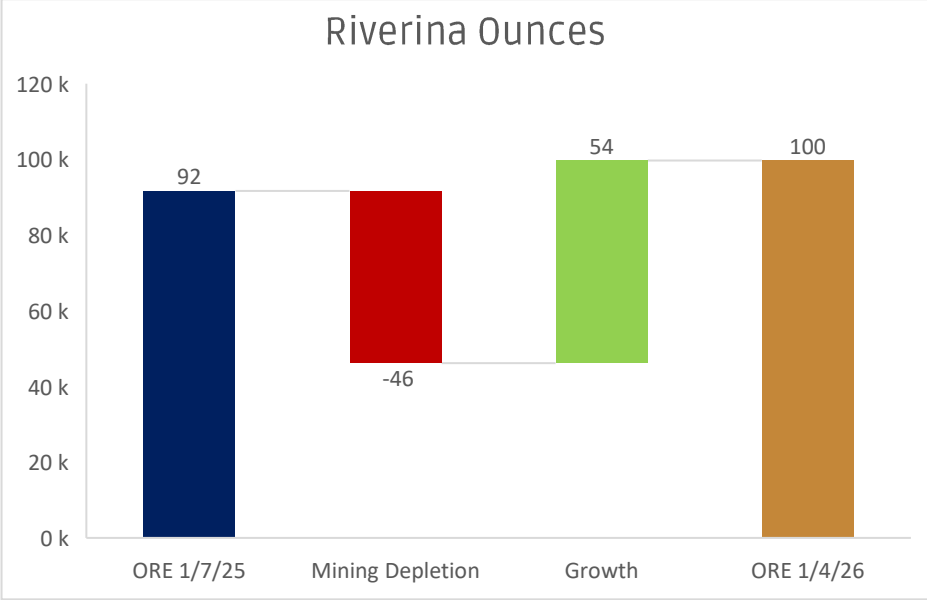

Figure 9 - Change in Riverina ORE ounces

INTRODUCTION

Tenement

The Riverina gold project is located on the granted mining tenement M30/256, which is 100% owned by Carnegie Gold Pty Ltd, a wholly owned subsidiary of Ora Banda Mining Limited. OBM holds rights to gold and its byproducts over this tenement. There are no known heritage or native title issues within the tenement. The tenement is in good standing with DMPE with no known title risk.

Permits and Licenses

The required environmental approvals to operate the Riverina Underground mine are in place. The operations remain compliant with all the current permitting requirements which remain in full force. A rehabilitation obligation remains at Riverina post open pit mining.

- Riverina Gold Operations Mining Proposal (Reg Id 128331, Approved September 2024)
- Riverina Gold Operations Mine Closure Plan for the Mining Proposal (Reg Id 98123)
- "Prescribed Premise Licence 9402/2023/1
- Groundwater Well Licence GWL108490 (3)
- Clearing Permit 8854-3

Infrastructure

The Riverina Underground mine commenced in May 2023, establishing declines, raises, ventilation and escapeway infrastructure. 16 production levels have been accessed, and stope production commenced on these levels up to 31 March 2026 with development and stoping ongoing. A 5 MW power station supplies HV power via a service hole to underground substations and distribution network. A dewatering capacity of 60 l/s is currently in place along with 2,365 ML in pit storage capacity. Permitted waste rock storage capacity remains as well as pit backfilling opportunities.

The Riverina office, workshop, communications and surface facilities are sufficient for the ongoing underground operation. Approved waste storage is sufficient for the Ore Reserve mine design.

The Riverina village is 2.8 km from the mine offices and was built in 2021. Additional rooms were made available in FY26 for a total of 220-person capacity.

The Davyhurst processing facility is located 46 km via well-established public roads to the south of Riverina. Road trains are used to haul ore from the mine ore pad at Riverina to the Davyhurst RoM pad.

MINERAL RESOURCES

Mineral Resource Estimation: Summary Information as required under Australian Securities Exchange (ASX) Listing Rule 5.8.1 follows.

GEOLOGY & GEOLOGICAL INTERPRETATION

Lithology

Mafic and ultramafic volcanics and volcanogenic sedimentary lithologies (wacke, siltstone, shales) are found in the main Riverina resource area. The Riverina deposit sits on the western limb of a regional significant syncline with the mine sequence generally dipping steeply (approximately 80-70°E) to the east.

Mafic basalts are the dominant rock type and host the Main Lodes within the Riverina deposit. Narrow, tightly constrained shear zones within the basalt host mineralised quartz veining with relatively tight alteration halos. Immediately to the west of the host basalt at Riverina is a thick body of peridotite (ultramafic). Several discrete, narrow ultramafic bodies have also been identified in the Riverina mine area. These narrow ultramafic bodies are interleaved with the mafic and sediment units proximal to the orebody in the Murchison and Reggie Lodes.

Metasedimentary bodies are host to mineralisation within both the Murchison and Reggie Lodes. Originally fine-grained greywackes and siltstone, they are now represented as moderately foliated to highly deformed felsic schists with zones that appear mylonitic in nature. The widths of the metasedimentary units range from very thin discontinuous lenses to more robust strike extensive units locally up to 15 m wide. A thinly bedded/laminated interflow sediment horizon lies in close proximity to the Main Lode ore zones in the southern portion of the deposit area. Semi-massive and massive sulphide zones are found within carbonaceous shale beds in the Murchison and Reggie Lode areas. These black shales are typically gold poor.

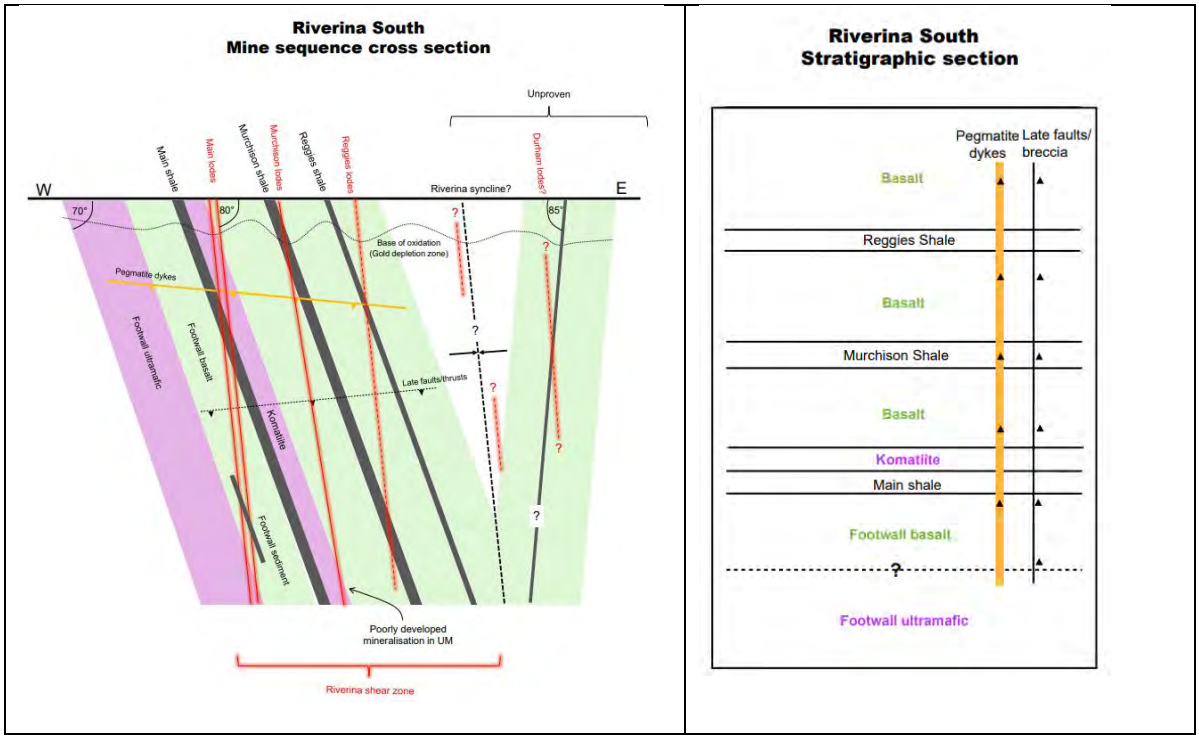

Figure 10 - Diagrammatic cross section of the defined mine sequence of the Riverina Deposit and indicative stratigraphic section

Late pegmatite dykes form a shallow S-SW dipping dyke swarm that crosscut all lithologies including alteration related to gold mineralisation. Narrow, steep east and north dipping dykes are also visible in the open pit. Dykes can be up to several metres true thickness but are more commonly 1 m or less and often pinch out/terminate on late structures.

Structure

The Riverina deposit is interpreted to lie in a low strain zone of a several kilometre long macro shear boudin, bounded to the east and west by thick ultramafic bodies. This macro boudin has developed around the core of a regional syncline that has been rotated and deformed within a ductile stress regime. The deposit is located within the western limb of this tightly folded syncline, with the stratigraphy within the limb dipping at approximately 70°E. Major shear zones have developed on this steep east dipping fold limb and control the line of historic workings north and south of the deposit.

There are three main mineralised horizons which make up the Riverina Deposit, namely Main Lodes, Murchison Lodes and Reggie Lodes. The Main Lode is defined as several discrete steep dipping to sub-vertical structures striking between 340° and grid north, running parallel while maintaining a separation of between 5 m and 15 m. These structures are remarkably consistent in their strike and dip continuity and have been consistently intersected in drilling for over 1.7 km of strike and over 1 km vertical metres down dip.

The Murchison Lodes are a series of parallel/sub-parallel mineralised structures that strike more north-south and also dip steeply to the east. The tenor of the mineralisation is influenced by the different lithologies that these steep shears cross-cut. The mineralised structures are generally narrow, displaying tight alteration halos.

The Reggie Lodes make a minor contribution to the overall MRE.

The Riverina area is dominated by tight to isoclinal folding (F1) that has an overall plunge of ~30° to the south. This mirrors the average plunge of mineralisation across the deposit, although observations from drill core show there are localised areas where the plunge is measured as sub-horizontal (5-10^0) to the south and possibly coincides with an increased tenor of grade and width.

An early extensional deformation event led to emplacement of N-S steep dipping extensional quartz veins with initial Au deposition. A later structural event involved ENE-WSW shortening and continued intense strike slip shearing over a period of time. In zones of high strain and low stress, early quartz veins were boudinaged and in places mylonitised, and gold was remobilised and redeposited. A strong ductile S-C fabric is developed with the intersection of the S and C fabrics plunging gently to the south. This is coincident with measurements of the plunge of well-developed quartz boudin necks, which range from sub-horizontal to up to 35^0 to the south.

The rocks at Riverina exhibit a diverse range of deformation over short distances. Only metres from mineralised shear zones, where rocks are intensely deformed and often mylonitic, pillow basalts are relatively undeformed, showing their distinctive flat bases and domal tops (younging direction to east). Undeformed sediment units also exhibit fine graded bedding and laminations. Pegmatite dykes, although weakly deformed by later structural events, tend to remain fairly pristine.

The post-mineralisation structural architecture based on pit mapping, drill core logging and underground mapping, highlights the presence of multiple shallow south-dipping thrust faults that transect the entire Riverina area. In the Riverina North pit, one such thrust is marked by a 30-40 cm thick zone of fault gouge (cataclasite) and saccharoidal quartz. Associated ramp structures, back thrusts and antithetic shears form a complex structure array in the Riverina North pit. N-S sub-vertical mineralised shear zones have also been reactivated and acted as transfer faults associated with the late-stage thrusting. Several of these structures have been intersected in underground development. An additional structural event, post north-south shortening and thrust development, resulted in conjugate strike slip faulting. Faults are steep ENE dipping (sinistral) and moderate SE dipping (dextral). Fault offsets are from a few metres to several metres. The steep ENE dipping set are open spaced structures and act as a fractured aquifers and transfer meteoric water into the mine.

Alteration & Mineralisation

Mineralisation at Riverina is hosted within three distinct mineralised shear systems; from west to east, they are the Main Lodes, the Murchison Lodes and the Reggie Lodes.

The Main Lode mineralised zone is hosted within pillowed basalts, the dominant rock type in the area and comprises several continuous discreet lodes running sub-parallel to each other, although only two form the bulk of the mineralisation. The individual ore zones range from <0.5 m to up to 3 m wide with the high-grade core characterised by intense shearing/mylonitisation of boudinaged quartz-sulphide veins and surrounding strong banded silica-biotite-sericite alteration of the mafic host. The Main Lodes exist within a broader shear zone characterised by weaker shearing and alteration. High gold grades are occasionally noted in the broader shear, associated with localised stronger silica alteration/veining, but are discontinuous. High grade mineralisation has a shallow southerly plunge consistent with geological observations (boudin neck plunge and S-C fabric intersection.

The dominant sulphide minerals are pyrrhotite and pyrite, with arsenopyrite and galena observed in the highest gold grade intervals. Highest concentration of sulphide tends to be within intensely altered wallrock adjacent to quartz veining. Visible gold is present as fine discreet flakes, however in very high-grade zones, forms small foliation parallel accumulations.

The Murchison Lodes comprise several parallel/sub-parallel mineralised zones ranging from <1 m to several metres thick with variable grades. Lodes are hosted within both strongly sheared and altered basalts, and finely bedded volcanogenic sediments (wacke, siltstone, shale). Basalt hosted ore zones exhibit strong shearing and boudinaged quartz-sulphide veining with associated strong silica-biotite-sulphide alteration. Strong shearing with boudinaged quartz-sulphide veining and associated silica-sericite alteration characterise the mineralisation with the sediment hosted ore zones in the Murchison. Sulphides are dominantly pyrite and pyrrhotite with localised arsenopyrite, galena and chalcopyrite.

Reggie Lodes are similar in character to the Murchison, comprising several sub-parallel, semi-continuous mineralised zones within both basalt and sediment host rocks.

Weathering

The weathering profile at Riverina is highly variable. Weathering increases significantly within shear zones and depth to fresh rock reaches vertical depths of 80 m in the centre of Riverina deposit and 40 to 50 m on the flanks of the main shear structures. The base of complete oxidation can extend to depths of up to 50 m vertical metres within the main shear zones. The base of complete oxidation over unaltered, massive mafic and ultramafic lithologies can be as shallow as 3–5 m below the current ground surface, as is evident in the north of the Riverina open pit. In places, possible zones of depletion in the upper saprolite are interpreted, where weaker mineralised shears appear to terminate ~20 m below surface. Stronger shears project to surface, although some redistribution of gold may have taken place from these shears as well. Significant areas of supergene enrichment are not evident.

DRILLING AND SAMPLING, AND SAMPLE ANALYSIS TECHNIQUES

Modern exploration in the Riverina area began in the mid 1980's. Numerous operators have held the tenure since. Although a proportion of drilling data is from previous operators, it is generally well documented and to industry standards of the time. In addition, OBM has added significant drilling to the Riverina deposit. All RC and diamond drilling at the deposit is deemed suitable for resource estimation purposes. Previous operators include Riverina Gold NL, Riverina Gold Mines, Greater Pacific Gold NL, Barminco, Barra Resources Ltd, Riverina Resources Ltd, Monarch Gold Ltd and Eastern Goldfields.

RC holes drilled by most operators were typically at least 5 inches in diameter. RC hole diameters from drilling by Riverina Gold NL and Barra Resources are unknown. Diamond holes were all HQ or NQ in diameter.

Early RC and diamond hole locations (Riverina Gold NL, Riverina Gold Mines, Greater Pacific Gold NL) were surveyed on an early Riverina local grid which is oriented to true north. The origin for this grid is 10,000N, 10,000E located at the south-west corner of surveyed tenement M30/98. These coordinates were transformed to MGA94 Zone 51 using well-established grid transformation parameters. Drilling by other operators was surveyed by mine surveyors or contractors using DGPS or RTKGPS in either AMG84 Zone 51 or MGA94 Zone 51 coordinates. Surface collars drilled by OBM were all picked up by the mine surveyor in MGA94 Zone 51 coordinates.

Generally shallow RC holes by Riverina Gold NL and Riverina Gold Mines were not down hole surveyed. Other early operators downhole surveyed RC holes by Eastman camera. Diamond drill holes were downhole surveyed by Eastman camera or gyro. Riverina Resources employed Eastman camera, electronic multi-shot or gyro for surveying. Electronic multishot was used by Monarch Gold and north seeking gyro was used by OBM. All grade control holes drilled by OBM are surveyed by the mine surveyor and downhole surveyed by rig north seeking gyro.

UG diamond drill rig alignment is via surveyed collar locations and the DeviAligner tool, downhole surveys via DeviGyro-OX tool. Underground face sample locations measured via laser distometer to known surveyed control points and development surveys via theodolite.

RC sampling protocols for some early operators (Riverina Gold NL., Riverina Gold Mines, Greater Pacific Gold NL, Barminco) are unknown. A riffle splitter was employed by Riverina Gold Mines and ¼ was sent for analysis. Later operators collected samples through a cyclone and split using either a riffle splitter or cone splitter. Barra Resources, Riverina Resources and Monarch Gold submitted 4 m composites for analysis. These were taken using a spear or flour scoop. Anomalous intervals were then re-split using a riffle splitter and submitted for analysis. OBM sampled every meter with a 2-3 kg split taken from a cone splitter. OBM occasionally submitted 4 m composite samples by spearing the 1 m sample piles. If anomalous gold values were returned, the individual 1 m samples from the rig cone splitter were submitted as a separate batch.

Diamond core was generally sampled to geological boundaries and or mineralised intervals. Generally, half core was sampled though Barra Resources Ltd submitted whole core for analysis. Core sampling or resource drilling by Ora Banda was defined by a geological or mineralisation boundary with ½ core submitted for analysis. Frequently underground drill core was whole core sampled. All drill samples were logged by qualified geologists.

Historical assay QAQC protocols used by companies prior to Monarch Gold's ownership (pre-2007) have not been documented in any detail. Monarch Gold submitted Certified Reference Material every 20th sample in RC drilling programs. Duplicate samples were submitted every 25th sample for RC drilling. The protocol adopted by OBM required CRM standards and blanks be inserted every 20 to 25 samples for RC and diamond drilling. The frequency rate of RC field duplicate samples was nominally 1 every 30 m. Underground diamond grade control drilling and face sampling assay submissions include blank and CRMs to monitor laboratory QAQC.

The current resource update follows an extensive UG diamond drill program completed after the previous MRE released in July 2025. An additional 349 UG diamond holes and 924 faces are included in the current MRE. In addition, results from 6 surface diamond holes from the 2025 deep drilling program were received post the 2025 MRE update and are included in the current MRE.

Assay QAQC for the additional drilling was analysed. Assay precision was acceptable, performance of certified reference material was good, and overall results were generally acceptable.

Sample Analysis Methods

Historical assay QAQC protocols used by companies prior to Monarch Gold's ownership (pre-2007) have not been documented in any detail. Monarch Gold submitted Certified Reference Material every 20th sample in RC drilling programs. Duplicate samples were submitted every 25th sample for RC drilling. The protocol adopted by OBM required CRM standards and blanks be inserted every 25 samples for RC and surface diamond drilling. The frequency rate of RC field duplicate samples was nominally 1 every 25 m. All underground diamond drill and face sample submissions include routine CRM and blank insertions at rate of 1:20. Diamond core is sampled to geological intervals with a minimum length of 0.3 m. Initially OBM drilling and face samples were prepared in the SGS on-site sample preparation laboratory and pulps sent to SGS in Kalgoorlie for analysis. A 50 g charge was taken and analysed by fire assay Microwave Plasma-Atomic Emission Spectroscopy (MP-AES). Since early March 2025 all underground grade control and face sampling was crushed in the SGS on-site laboratory and the samples sent to SGS Kalgoorlie for gold analysis by Photon assay method. In April 2025 all samples from surface drilling were crushed at the SGS on-site laboratory and the samples sent to SGS Kalgoorlie for gold analysis by Photon assay method. Transfer of analytical method from fire assay to Photon assay followed a program of comparison assaying whereby Photon assay analysis was done on the crush reject of samples already assayed by fire assay.

ESTIMATION METHODOLOGY

Mineralised domains were interpreted to assay grade thresholds corresponding to geological observations in core and face photographs, and geology logging, including structure. All drilling and face sampling from underground development was used to aid the interpretation. RC, diamond drilling and face sampling assay data was used in the estimation of grades. Sample intervals were manually defined using Leapfrog™ software, on a section-by-section basis. The two dominant mineralised structures, ME1 and MW1 were modelled as a central vein, surrounded by a lower grade shear zone. Assay results were composited to 0.3m, starting from the point where drillholes enter the domains. Residual assay intervals were distributed over the interval. The narrow mineralised domains and minimum sample width of 0.3m led to the adoption of the 0.3m composite.

Previous Riverina MRE's used a 2-dimensional estimation technique where an 'accumulation' variable (gram-metres) and lode width were estimated and the grade back-calculated from the estimated 'accumulation' and width variables. The current MRE uses a traditional estimation of gold grade into a 3-dimensional block model.

Spatial continuity, using Supervisor™ software, of composite gold grades was evaluated using variography and the parameters defined were applied in the estimation process. Search neighbourhoods were defined using Kriging Neighbourhood Analysis implemented in Supervisor™. Top cuts were applied to the composite gold grades on a domain basis in order to reduce the influence of sometimes extreme grades. Control over spread of high grades was further implemented for some lodes by using distance limiting and grade thresholds. Both top-cutting and distance limiting grade thresholds were implemented to control metal risk.

Estimation of gold grades was by ordinary kriging using Leapfrog™ software into a parent block size of 6.4mE x 10mN x 10mRL. The domain wireframes were used to constrain lode volumes using suitable sub-celling. A three-pass search strategy was implemented with successive passes having fewer minimum and maximum samples. Search anisotropy mirrored the variogram anisotropy. Locally variable anisotropy was adopted for the estimation to re-orient the search and variogram according to local lode undulations.

The bulk density values for ore were assigned based on the weathering state of the rock and determined from over 5,684 drill core density measurements. Densities are applied based on several domains, including ore/waste, weathering and lithology. The model has been depleted to account for existing mining, both underground up to 1 April 2026 and previous open pit.

CRITERIA USED FOR CLASSIFICATION

Wireframe solids were constructed to encompass areas considered to adequately fulfil the requirement to be classified as either, Measured, Indicated or Inferred:

- Measured – Near surface areas defined by close spaced RC grade control drilling, or an area between two development drives with significant face sampling
- Indicated – Areas with:
    - drill spacing in long section up to approximately 30mN x 30mRL and with reasonable confidence in the geological interpretation and grade continuity.
    - reasonable estimation quality as defined by the conditional bias slope > 0.5
- Inferred – Areas with:
    - drill spacing in long section in excess of 30mN x 30mRL and where grade continuity is poorer as defined by a lower sample density, even though geological continuity may be apparent.
    - poorer estimation quality as defined by the conditional bias slope > 0.2 and < 0.5

Areas of some lodes, particularly at depth have fairly low/no sample support and were not classified.

CUT-OFF GRADES AND MODIFYING FACTORS

The Mineral Resources have been reported from fresh material at a diluted cut-off of 0.8 g/t Au inside Auto Stope Designer (ASD) derived solids with dimensions of 10mN x 10mRL and a minimum width of 1.6 m. Individual MSO blocks were assessed and removed if above the top of fresh DTM surface and if above the $2400/ oz optimised pit shell from within which the remaining Riverina open pit resources are reported.

ORE RESERVES

Material Assumptions and Outcomes, Criteria for Classification

This ORE for Riverina was derived from technical studies, data and knowledge gained from the recent underground mining, incorporating project-specific costs as well as geotechnical analysis, dilution and recovery parameters and was based on the 2026 MRE current at the time and described in this announcement. Processing parameters were based on test work that has been combined with recent processing performance. Hydrogeological conditions were determined from recent mining at Riverina.

The Riverina Underground Ore Reserve was estimated using a gold price of A$2,500/ oz.

The dilution skin method was employed to reflect the selective mining method proposed for Riverina Underground. Dilution parameters were subjectively determined based on a geotechnical assessment of the expected mining environment. A cut-off grade of 2.5 g/t was applied to determine economic mining envelopes, further spatial optimisation was done to ensure all economic ounces were included.

Mining recovery for the underground Ore Reserve is dependent upon the dimensions and spacing of pillars throughout the orebody. The Riverina mine design assumed 40 m open stopes (along strike) and pillars of 5.0 m by 17.5 m. The 40 m stope strike extents were considered a practical distance over which to successfully operate remote loaders to recover ore from open stopes. 3 m high dilution control sill pillars were designed where stoping extends more than 4 levels down dip on a mineralised lode. The rib and sill pillars equate to 86% mining recovery with both development and stoping activities. Consistent with reconciled performance, an additional 5% stope ore loss was also included for operational losses. The overall mining recovery was estimated to be 83%.

Mining Method

The underground mine design utilises conventional narrow vein up-hole benching using longhole open stoping mining methods. This method is commonly used in the Western Australian Goldfields for this style of mineralisation.

Mining equipment is mechanised, with equipment that includes electric-hydraulic drills for development and production, and rubber tyred loaders and trucks for load and haul activities. Stope production loading incorporates a combination of conventional loading and tele-remote loading for non-entry mining stopes.

Based on the geotechnical assessment, which identified good ground conditions and favourable stress environment, as would be expected at mining depths less than 600mbs, no stope backfill is anticipated.

Cut-off Grades

The estimation of the cut-off grades for the Riverina Underground Ore Reserve were estimated to be 2.5 g/t for production stoping. The cut-off grade calculation was estimated at a gold price of A$2,500/oz, and is inclusive of mining, transport, processing, overheads, sustaining capital and royalties.

A cut-off grade of 1.9 g/t was applied to the underground development based on the incremental cost of developing hauling and processing of the ore. The calculation was estimated at a gold price of A$2,500/oz.

Low Grade insitu material is 0.6 g/t to 1.9 g/t, based on the surface SP cut-off 0.6 g/t where haulage, processing, admin costs are applicable and using a gold price of A$5,000/oz.

Recent Riverina mine contractor costs and OBM budget costings were used.

The standard WA state royalty of 2.5% NSR plus a 1% NSR third party royalty was applied.

Processing Method

The process for treating ore at the DGP is conventional CIL with some gold recovered via a gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. The process plant has a nominal throughput rate of 1.2 Mtpa based on a grind size of 106 µm. The process plant has been successfully operated at this rate with recent improvements made. The processing recovery applied to Riverina Underground was 88% and was based on metallurgical test work. The recovery performance was 92% through Davyhurst plant in FY26 to EOM March-26, processing Riverina and Sand King ores which have an average metallurgical test work recovery of 88%.

Estimation Methodology, and Modifying Factors

Given the narrow vein nature of the mineralisation, the global dilution, inclusive of stoping and ore drive development, was estimated to be 51% of material. Background grades were estimated into the block model and were included in the dilution modelling. Dilution grades varied between zero and 0.7 g/t depending on the nature of the alteration halo. The global average grade of dilution was estimated to be 0.15 g/t. Dilution being all included material less than 0.6 g/t[8].

Delineation of economic stoping areas was completed using Deswik™ software. Mineable “stope” shapes were created to simulate fully diluted stope blocks, as described below. The optimisation field used a cut-off grade of 2.5 g/t. The stope shapes are then depleted by development ore drives and modifying factors are applied in the mine schedule. Scheduled stopes below 2.5 g/t are spatially optimised and incremental stope cut-off grades were used where development is in place and planned to access stopes <2.5 g/t. Spatial optimisation and use of incremental COG of 2.2 g/t ensures all economic ounces are included.

A minimum stope mining width of 1.6 m was applied in the dilution modelling process, with an additional 0.6 m dilution skin applied to all valid stope shapes (0.3 m hanging wall and 0.3 m footwall). Therefore, all stoping analytics have been completed on a minimum mining width including dilution of 2.2 m wide. In addition, a nominal provision for unplanned dilution of 20% at 0 g/t was also included in a scheduling adjustment as a contingency to all stoping panels.

[8] 0.7 g/t represents the surface stockpile cut off for development ore.

Inferred material was not considered in defining the stoping envelopes; however, due to practical mining geometries a small portion of incidental Inferred material was included within the Underground Ore Reserve. This material occurs at the edges of the mining envelope and is estimated at approximately 17 kt at a grade of 1.3g/t, representing 1% of the Riverina Underground Ore Reserve ounces and is not relied upon for economic extraction. The incidental Inferred inventory was not considered material to the economics of the project. The RESCAT for each scheduled task was attributed with the RESCAT of the dominant mass of material above 0.6 g/t.

The economic viability of the Riverina Underground was confirmed using current commercial parameters in a project evaluation cash flow model. This model also considered project phasing, stockpiling, project capital and the effect of fixed costs. The cash flow modelling was based on a gold price of A$3,600/oz. The mine demonstrated a positive net cash flow with acceptable returns. Overall unit mining costs for the underground was estimated to be A$204/t ore, inclusive of sustaining capital.

Mine Design

The Riverina Underground design on which this Ore Reserve was based is shown in Figure 11. The mine entries for the Riverina Underground consists of a main access portal, primary return ventilation rise and an escapeway rise. All entries are located in the fresh rock portion of the existing Riverina pit. The decline is 5.5 m wide x 5.7 m high with a typical gradient of 1:7. Ore drives are designed to be 4.5 m wide x 4.5 m high.

Underground pump stations are in place and have been allowed for in the design with ~100 vertical metres between pump stations. Mine dewatering is further pumped 15 km to a water storage pit with 1,400,000 kl capacity remaining. Dewatering pipelines and pumps are capable of 60 l/s.

Primary ventilation is via a 4.5 m diameter raise bore from underground to the open pit. Return air drives are designed 5 m x 5 m with vertical rises ~6 m x 4 m. The system can meet the demand at various stages including the Ore Reserve design and schedule.

The average floor to floor slope distance between levels is set at 22 m with an average stope panel height of approximately 17.5 m. Stope parameters used in the Riverina mine design are shown in Table 13.

Table 13 - Riverina Stope Parameters

Stoping Parameters		
Sub-Levels	22	m
Stope Width	1.6	m
Dilution FW	0.3	m
Dilution HW	0.3	m
Stope Length	~40	m
Ave Stope Width	2.2	m
Rib Pillar Width	5	m
Sil Pillar thickness	4	m
Sil Pillar frequency	~85	m
COG	2.5	g/t
Schedule Dilution	20%	0 g/t Dilution
Schedule Recovery	95%	

The current ground control management plan provides stope and pillar analysis and guidance in line with the stope parameters used.

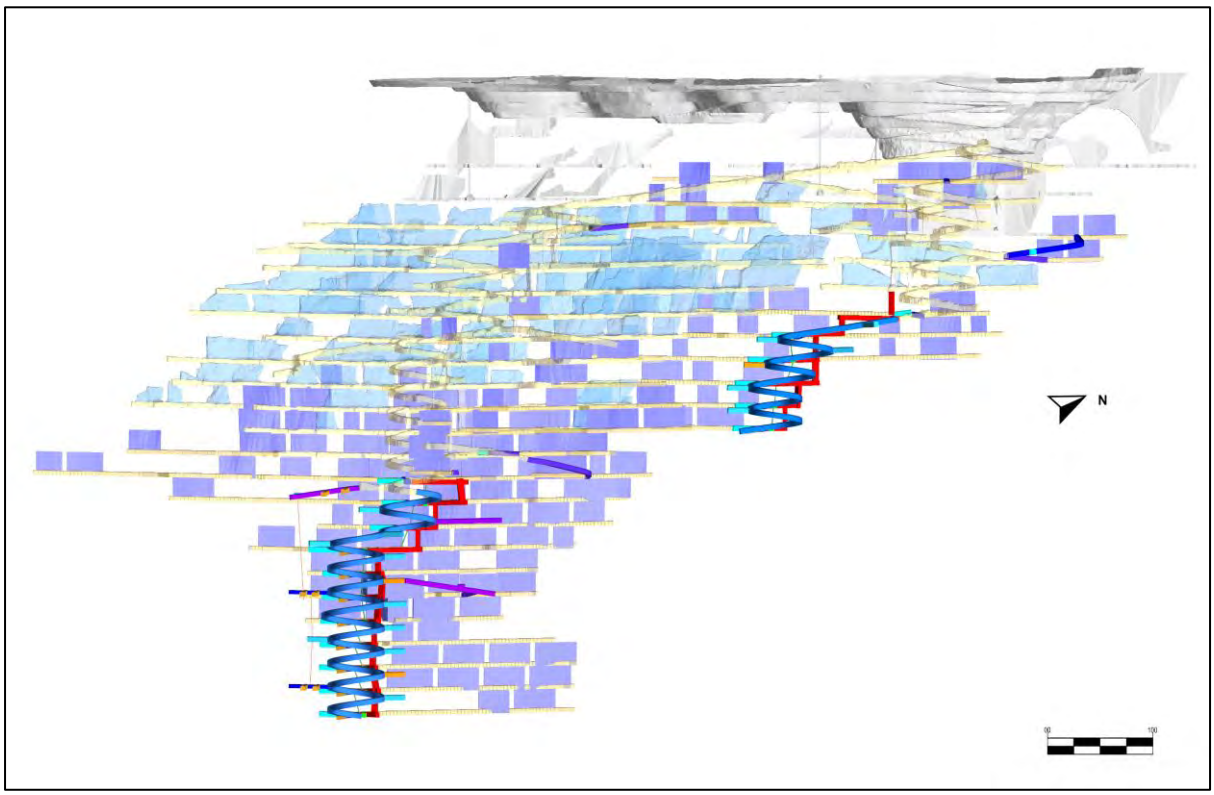

Figure 11 – Long section looking west of Riverina Underground Ore Reserve mine design with existing OBM underground workings (as built yellow drives, blue mined stopes as at 1 April 2026) and future Ore Reserve stoping areas (purple), Riverina pit and historical underground working (light grey)

Riverina Underground Mine Schedule

A mine schedule for the Riverina Underground Ore Reserve was developed, with productivity rate assumption in line with contractor expectations.

The mining sequence assumes top-down retreat mining with no current plans to backfill stopes. The mining equipment resource levels on which the mine schedule was based are shown in Table 14. The ORE schedule was used in the economic assessment.

Table 14 - Riverina mining equipment levels

Equipment		
2x Jumbo	Sandvik DD421	Twin Boom
2x Long Hole Drill	Sandvik DL431	76mm holes
2-3x Loader	Sandvik LH517	17T
2-3x Truck	Sandvik TH663	60T

Economic Assessment

An economic assessment was carried on the Riverina Underground to validate the Ore Reserve. The cash flow was modelled in real terms on a pre-tax basis. Costs, recovery and revenue parameters used were as described above.

Costs were derived from the FY25 budget estimate including contract pricing current at the date of this Ore Reserve. Unit costs for mining were estimated based on fully resourced contracted scope of work.

Mining overheads were based on OBM budget provisions for supervision and technical support, as well as contractor fixed costs, general operating expenses, FIFO flights and accommodation. Dayworks provisions were also included for miscellaneous works during operations as well as closing of the site.

Unit costs for haulage, processing and head office overheads were calculated using the combined project cost model with the Ore Reserve mine schedules and stockpiles.

An allowance for capital has been used in the economic modelling and based on recent actuals and budget forecasts. The allowance covers:

- Additional underground sub stations,
- Power station purchase,
- Primary vent controls, and
- Underground dewatering.

The ORE is based on a feasibility level of accuracy. A gold price of A$3,600/oz was used for financial assessment, and the competent person is satisfied that the mine demonstrated a positive net cash flow with acceptable returns.

Ore Reserve

On the basis of the outcomes of the analysis described above, the estimated economic mining inventory was classified as an Ore Reserve under the 2012 JORC code. All of the ORE was derived from the economic portion of the Measured and Indicated Mineral Resource. Measured Mineral

Resource within the economic mining envelope was classified at Proved Ore Reserve Estimate. Indicated Mineral Resource within the economic mining envelope was classified at Probable Ore Reserve Estimate. Low grade was all classified as Probable Ore Reserve Estimate. The Ore Reserve is shown in Table 15.

Table 15 - Riverina Underground Ore Reserve, as at 1 April 2026

RIVERINA GOLD PROJECT ORE RESERVE ESTIMATE:									
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	103	4.0	13	741	3.6	87	844	3.7	100
LOW GRADE	-	-		208	1.3	9	208	1.3	9
TOTAL	103	4.0	13	**949**	**3.1**	**95**	**1,052**	**3.2**	**108**

ROUND DAM RESOURCE AND RESERVE

SUMMARY

The major MRE update for Round Dam (previous reported as Walhalla) follows an extensive surface drill program at Round Dam that commenced in February 2025. The Round Dam MRE covers the southern half of the 18km Round Dam Trend, from Salmon Gums to Federal Flag North (Figure 12).

A summary of the Round Dam Mineral Resource and Ore Reserve as at 1 April 2026 are shown in Table 16 and Table 17. The maiden Ore reserve for Round Dam is a significant increase to OBM ORE position extending the ORE mine life to over 5years. The series of 5 pits over 3.6 km strike demonstrates consistent grade tenor and lateral continuity within an economic envelope.

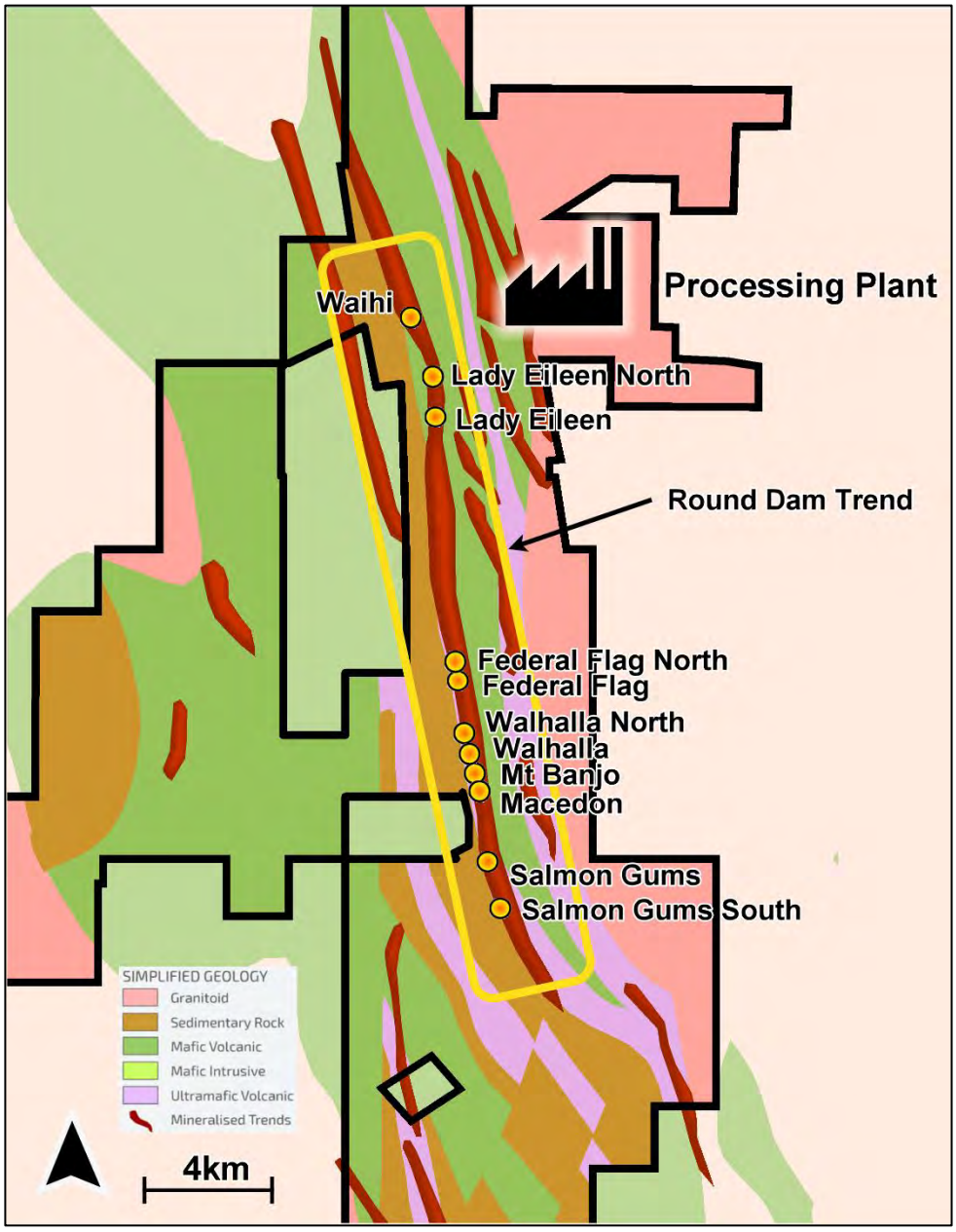

Figure 12 – Deposits along Round Dam Trend

Table 16 – Round Dam Mineral Resource Estimate

ROUND DAM PROJECT MINERAL RESOURCE ESTIMATE[1]:									
	MEASURED		INDICATED		INFERRED		TOTAL MATERIAL		
	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	-	-	-	-	-	-	-	-	-
OPEN PIT	-	-	7,152	1.8	18,199	1.6	25,351	1.6	1,330
TOTAL	-	-	**7,152**	**1.8**	**18,199**	**1.6**	**25,351**	**1.6**	**1,330**

Table 17 – Round Dam Gold Project Ore Reserve Estimate

ROUND DAM PROJECT ORE RESERVE ESTIMATE:									
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
OPEN PIT[2]	-	-	-	3,669	1.9	223	3,669	1.9	223
LOW GRADE[3]	-	-	-	493	0.6	10	493	0.6	10
TOTAL	**-**	**-**	**-**	**4,162**	**1.7**	**233**	**4,162**	**1.7**	**233**

INTRODUCTION

The three historical pits mined at Round Dam from 1990-2008 produced 513 kt @ 1.8 g/t for 29 Koz.

Tenement

The Round Dam gold project is located on the granted mining tenement M30/255, which is 100% owned by Carnegie Gold Pty Ltd, a wholly owned subsidiary of Ora Banda. On 30 October 2023, the Ora Banda Group entered into a binding Farm-In JV Agreement with Davyston Exploration Pty Ltd ("Davyston"), a wholly owned entity of the Wesfarmers Chemicals, Energy & Fertilisers division ("Wesfarmers"). Under the agreement, Davyston acquired an initial 65% rights to all other minerals, except for gold and its byproducts. To date, Davyston has successfully earned into an additional 6%, such that the joint venture currently sits at 71% Davyston and 29% Ora Banda Group. Ora Banda holds the rights to gold and its byproducts over all of the tenements.

There are no known heritage or native title issues within the tenement. The tenement is in good standing with DMPE with no known title risk.

Round Dam pits are entirely on a granted Mining Lease 100% owned by Ora Banda Mining, the designed WRL's footprints are over both Mining and Exploration tenements 100% owned by Ora Banda Mining. OBM is in the process of making an application for a mining lease to facilitate associated mining infrastructure

Permits and Licenses

The company is currently advancing through the regulatory approval phase of the Round Dam Project which seeks the necessary environmental approvals to support its planned mining development. As part of this process, it is undertaking comprehensive baseline studies to collect

[1] Inclusive of Ore Reserve.
[2] The Round Dam open pit Ore Reserve was primarily estimated using a cut-off grade of 0.7 g/t Au based on a gold price of A$3,600/oz.
[3] Low Grade Ore Reserve aligns with stockpiles and was based on A$5,000/oz for a cut-off grade of 0.5 g/t.

environmental data which will form the foundation for impact assessments and management strategies.

This work includes detailed investigations into flora and fauna, water resources, and cultural heritage, alongside ongoing stakeholder engagement. Securing these approvals will represent a key milestone in aligning the project with its development schedule and mine closure planning obligations.

Based on current assessments, no material impediments have been identified; however, approvals remain subject to regulatory processes.

Mine Infrastructure

The Round Dam Project is located 140 km via roads northwest of Kalgoorlie, 15 km to the south of Davyhurst processing plant and 15 km from the Davyhurst village.

The existing features of the Round Dam Gold project consist of three small pits, Federal Flag North, Federal Flag and Walhalla. These pits were mined from 1990 -2008 by various companies including MMC, Croesus and Monarch. There is a well-built haul road from Davyhurst to Round Dam, there are two nearby borefields, Turkey nest, ROM and office pads.

The site contains two waste rock landforms one of which is partially rehabilitated

MINERAL RESOURCES

Mineral Resource Estimation: Summary Information as required under Australian Securities Exchange (ASX) Listing Rule 5.8.1 follows.

GEOLOGY & GEOLOGICAL INTERPRETATION

The Round Dam Trend is located within the Coolgardie Domain of the Kalgoorlie Terrane in the Eastern Goldfields Province of Western Australia. Round Dam mineralisation is hosted within Archaean mafic to ultramafic volcanic rocks and sediments of the Hampton Hill Formation, comprising a fractionated ultramafic–mafic sequence metamorphosed to upper greenschist–lower amphibolite facies. The Round Dam Trend is interpreted as parallel to the Zulieka Shear to the East (Figure 13).

At mine scale, bedding is locally preserved and texturally apparent in flattened pillow basalts. Pillows are well preserved within the komatiitic flows of the ultramafic. Bedding is generally subparallel to foliation, which dips steeply (~70°) toward 265°. However, primary volcanic textures are commonly overprinted by deformation, metamorphism and hydrothermal alteration. Younging is established from east to west through the volcanic progression from primitive ultramafic flows to komatiitic basalts and into more evolved basaltic units.

Litho-geochemistry obtained from 4 Acid digest (ICO-MS finish) along with additional portable X-Ray Fluorescence (pXRF) data provides a reliable method for differentiating volcanic units and confirming stratigraphic position where visual logging alone is insufficient. Elements such as Cr, Ni, Ti, Th, Sc and Zr are especially effective in discriminating between primitive ultramafic flows, komatiitic basalts, mixed Cr basalts and more evolved tholeiitic units. Ba, K, U, Th and Zr are used to identify and classify the meta-sedimentary units.

The Golden Pole Basalt forms a critical upper stratigraphic marker above the fractionated Hampton Hill volcanic sequence and is likely the Gleesons basalt. This unit hosts the Golden Pole mineralisation at Waihi and is also observed underlaying the sequence in the southern portion of the Round Dam Trend and

The package of greenstone is hosted between a felsic volcaniclastic unit to the East (Meta-tuff to meta-lapillistone) and interbedded felsic volcaniclastics (meta-tuff) and shales to the West.

There are multiple pegmatites crosscutting the Round Dam Trend striking in several orientations, including NW-SE (moderate to steep NE dipping) and N-S (shallowly E dipping). Spodumene and lepidolite are observed throughout the pegmatites.

There is one observed post mineralisation (Proterozoic) dolerite dyke cross-cutting the stratigraphy at Round Dam, striking approximately E – W and steeply dipping to the North.

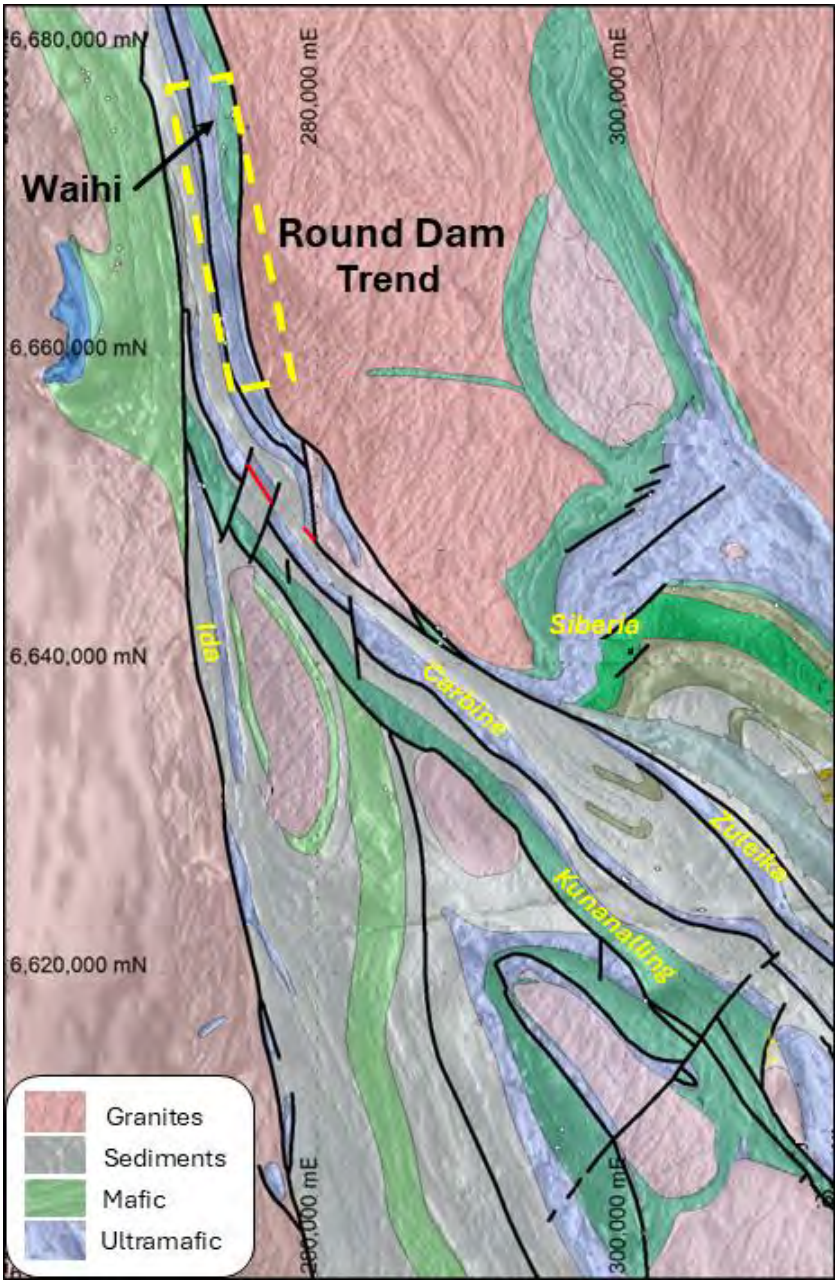

Figure 13 – Regional Geology showing proximity of major regional structures to Round Dam

Structure

The major regional structure proximal to the Round Dam Trend is the Zuleika Shear. This major shear zone is interpreted to be East of the Trend, striking NNW to SSE. To the West of Round Dam is a second major regional structure, the Ida Fault (Figure 6).

Gold mineralization along The Round Dam Trend is associated with shear related folding and shear structures producing boudinaged quartz veins. The plunge of high-grade mineralization ranges from -20^0 to -35^0 to the North. This is derived from the measured fold hinges, lineations and boudinaged quartz veins in both diamond drill core and from mapping within the historical open pits.

The proximity to the Zulieka Shear likely had a great impact on the amount of simple shearing that occurred along the Round Dam Trend. This is observed in the shear jog at Walhalla North, with approximately 100m of West – East offset of the lithology and lodes. High-grade shoots form on either side of the jog.

Other structures observed within the historical open pits at Federal Flag, Walhalla are late crosscutting strike slip faults. These faults offset mineralization at the metre scale. Late faults are sometimes exploited by pegmatites which stope out mineralisation where they intersect the gold-bearing lodes.

Alteration & Mineralisation

There are two main lode styles along the Round Dam Trend, contact lodes and the ultramafic quartz lodes. The contact lodes between the mafic to ultramafic (Lynx Lode) are moderately altered (biotite and silica) and mylonitised. The lode is dominantly hosted within the mafic unit at the contact. Thin veinlets with pyrrhotite, galena and pyrite are common. The contact lodes between the ultramafic unit and the Eastern sedimentary package are strongly silicified within common concordant veining with strong pyrrhotite and arsenopyrite with minor pyrite. Minor biotite and sericite are noted as bands or alteration zones depending on the localized mineralogy of the Eastern sedimentary package. The Grizzly Lode is an ultramafic quartz lode.

Gold mineralisation typically occurs within the sheared and folded quartz veins, within mylonite zones at the sheared contacts of lithological contacts. The lode alteration for the Lynx Lode is extensive and can be over 20m in true thickness, typically biotite-silica-pyrrhotite-pyrite. The alteration within the ultramafic surrounding the Grizzly quartz lodes are less extensive and can range from 1m to 5m of biotite-phlogopite-tremolite-silica, with common pyrrhotite-pyrite-galena. The quartz veins range from thin veinlets (mm scale) to large (up to 5m thick) quartz blowouts. The lodes hosted within the Eastern Meta-Sedimentary Package are veinlets to veins, with 1-2m wide biotite-sericite-silica alteration halos. The sediment hosted lodes have a typical assemblage of pyrrhotite and pyrite+/- arsenopyrite.

Weathering

The weathering profile along the Round Dam Trend is dependent on lithology and the presence and intensity of shearing. Variations in weathering are easily observed within RC chips, diamond core and from the historic open pits along the Trend. The ultramafic unit has a relatively shallow weathering profile with fresh rock within 5m to 15m of surface. The remaining lithologies along the trend are more weathered with fresh rock within 30m - 40m of surface. Transitional rock is approximately 20m – 30m thick.

DRILLING TECHNIQUES

Modern exploration in the Round Dam area began in the early 1980's. Numerous operators have held the tenure since. Although a proportion of drilling data is from previous operators, it is reasonably well documented and to industry standards of the time. In addition, OBM has added significant drilling to the Round Dam deposit. All RC and diamond drilling at the deposit is deemed suitable for resource estimation purposes. Previous explorers include Texas Gulf, West Coast Holdings Pty (Westcoast), Western Mining Corporation (WMC), Aberfoyle/Bardoc, Consolidated Gold (Cons Gold), Davyhurst Project Pty Ltd (DPPL), Croesus, Monarch Gold Ltd, Eastern Goldfields (EGS)/Swan Gold and WESCEF.

Texas Gulf

Texas Gulf drilled short 16m RC holes for laterites. WMC drilled vertical RAB holes. Westcoast drilled RAB holes to a depth of 20m and RC holes to a depth of 40m. Samples were collected through a cyclone, at two metre intervals, riffle split to approximately one kilogram and sent for analysis.

Aberfoyle/Bardoc

Aberfoyle/Bardoc drilled RAB, RC and Diamond holes. RAB and Diamond details generally unknown but RC drilling used 4 and 6 inch diameter face sampling hammer.

Consolidated Gold/DPPL

Cons Gold drilled vertical RAB holes, survey details unknown. Two or four metre composites were collected and sent for analysis.

DPPL RC drilling used a 4.25 to 5.5 inch face hammer with stabilisers. A three-stage riffle split was used to take 4m composite samples. The Round Dam Local grid was used. RC collars were surveyed by licensed surveyors to respective grids. The RC resource holes were downhole surveyed by Eastman single-shot camera. Drilling was predominately inclined at between -50° and -60° towards local grid east (~80° MGA Azi).

Croesus

Croesus RC drilling details unknown but assumed to use face sampling hammers. Various local grids and AMG zone 51 were used. RC holes were routinely collar surveyed and downhole surveyed using Electronic Multishot (EMS), GRYO, Eastman single shot or combination thereof. RAB holes were drilled vertically, RC was inclined at between -50° and -60° towards local grid east (~80° MGA Azi).

Monarch gold

Monarch RC drilling used a 4 inch blade or 5.5 inch diameter RC hammer. Drilling was completed on various local grids and MGA. Holes routinely collar surveyed and RC holes downhole surveyed using EMS, or GYRO at 5m interval average or Eastman single shot (28m interval average). All grade control collars were surveyed by DGPS. Drilling is inclined at between -50° and -60° towards local grid east (~80° MGA Azi). Grade control RC drilled vertically or 50° to 70° toward local grid east.

Eastern Goldfields

EGS/Swan Gold RC drilling was carried out using a face sampling Hammer with 5.25" and 5.125" diameter samples collected under cone splitter. Diamond core was taken as HQ3 to approximately. 40m, then NQ2 to bottom of hole. All core was oriented by spear. Collar locations were surveyed by DGPS and downhole surveys were collected using electronic multishot by the drillers. Subsequent to drilling, the holes were open hole gyro surveyed by ABIMS where possible. The grid system used

is GDA1994 MGA Zone 51. Drilling was inclined at between -50° and -60° towards 80° MGA Azimuth.

Ora Banda Mining

Ora Banda RC drilling was completed using a 5.5 – 5.625 inch diameter face sampling hammer. Some diamond core holes have RC pre-collars. Core diameters include PQ3, HQ3 and NQ2. All core was oriented by Axis instrument. Drill hole collar positions were picked up by an OBM mine surveyor using RTKGPS, subsequent to drilling. All downhole surveys were taken every 10m by Gyro. The grid system used is GDA1994 MGA Zone 51.

Wesfarmers

Wesfarmers (WESCEF) drilling targeted non gold elements, particularly lithium. RC drilling was by the same drill contractor as Ora Banda with identical methods and procedures. Gold sampling was from 4m composites scoop sampled from the 1m sample piles. Composite samples over 0.1g/t were 1m split.

SAMPLING AND SAMPLE ANALYSIS

Historical assay QAQC protocols used by companies prior to Croesus's ownership (pre-2000) have not been documented in any detail.

Croesus

Reverse Circulation (RC) 1m samples collected under cyclone. Composite results greater than 0.1 g/t gold, were riffle split at 1m intervals, where samples were dry, and grab sampled where wet.

Croesus duplicated every 20th sample in the field. Gannet standards and blank samples made by Croesus were submitted with split sample submissions. QAQC analysis of repeats was analysed by Croesus for their drilling completed during 2000. Samples were analysed for Au by 50g Fire Assay/ICPOES at Ultratrace in Perth.

Monarch

RC samples were riffle split and collected at 1m intervals. RAB samples were taken by scoop as 4 metre composites and 1metre end of hole samples. Grade control RC samples were collected as 2.5m or 1m samples either by cone splitter or scoop sample.

Monarch Gold submitted Certified Reference Material every 20th sample in RC drilling programs. Duplicate samples were submitted every 25th sample for RC drilling. RC samples were submitted to ALS laboratory for gold analysis by 50g fire assay. The Laboratory used for RAB samples is uncertain. RAB samples were analysed for gold by Aqua regia with an Atomic Absorption Spectroscopy finish. Grade control samples were submitted to SGS in Kalgoorlie for gold analysis by 50g Fire assay.

Eastern Goldfields

Diamond samples were taken as half core samples, cut by Almonte saw. Sample intervals were selected by geologist and defined by geological boundaries. Minimum sample length is 0.3m, maximum 1.5m. RC samples collected from the cone splitter directly off rig into calico bags. Samples were taken predominately as 1m spilt, with four metre composite samples taken outside of the mineralised zones.

EGS included commercially prepared standard samples and blanks in the sample stream at a rate of 1:10. Swan Gold samples were sent to Bureau Veritas laboratory in Kalgoorlie. The samples were

analysed by Firing a 40g charge followed by AAS finish. EGS samples were sent to Intertek Laboratory in Kalgoorlie for gold analysis by 50g Fire assay/ICP Optical Emission Spectrometry.

Ora Banda Mining

All RC samples were collected into calico bags from a rig mounted cone splitter. Initially four metre composite RC samples were taken outside of mineralised zones, collected using a scoop from the sample piles at the drill site. The one metre cone spilt samples were taken within the expected mineralised zones. Later in the program, entire RC holes were 1m split sampled. Core sample intervals were selected by geologist and defined by geological boundaries with a minimum length of 0.3m.

Ora Banda inserts CRM standards and blanks every 25 samples for RC and surface diamond drilling. The frequency rate of RC field duplicate samples was nominally 1 every 25 m. Several analytical methods and laboratories have been utilised for assaying. Samples from exploration drilling were initially sent to ALS, Perth for pulverising, and assay by 50g fire assay Microwave Plasma-Atomic Emission Spectroscopy (MP-AES). Most resource definition samples were sent to SGS on-site laboratory for crushing and analysis by photon at SGS, Kalgoorlie. Most resource development samples were sent to SGS, Perth for 50g fire assay, AAS finish. Transfer of analytical method from fire assay to Photon assay followed a program of comparison assaying between Photon assay and Fire assay.

Wesfarmers

WESCEF samples sent for gold analysis were submitted by Ora Banda personnel using identical procedures. Samples were prepared at the SGS site lab by crushing and pulverising (Fire Assay) or crushing (photon analysis). Prepared samples were sent to SGS Kalgoorlie for gold analysis by Fire Assay initially and more recently Photon assay.

ESTIMATION METHODOLOGY

Mineralised lodes were generally interpreted on E-W sections and flitches using Leapfrog™ software. Round Dam mineralisation comprises generally 60-70° west dipping, 350° striking parallel lodes. The mineralisation follows along the contacts of the Ultramafic in the HW and FW as well as internally in the Ultramafic. Mineralisation in the HW mafic and FW sediments is present but not well constrained or defined. Interpretation of mineralisation was largely grade and lithology driven from mostly RC drill data. Pit mapping, regional mapping and geophysics were also used. As the lodes are generally contact following, the lithology model was used to assist interpretation consistency along strike.

The resource model is interpreted to a 0.3 g/t cut-off grade guided by presence and intensity of quartz veining, alteration and sulphides as well as contacts between the lithology. A cumulative frequency plot of the all the resource drilling revealed a slight inflection point near 0.3 g/t and this value was taken to represent the boundary between mineralised and un-mineralised material. A minimum of 2 m downhole width above 0.3 g/t defined a potential lode. Internal dilution was sometimes greater than 2 m, but this was accepted given reasonable continuity evident at the 0.3 g/t cut-off. Sometimes lodes were pushed through drill holes with grades below 0.3 g/t to maintain continuity.

Raw assay samples were composited in Leapfrog™ software prior to estimation. Raw samples were assigned to the mineralisation wireframe they fall within. Downhole compositing was completed for each hole, the compositing starting from the point where the hole enters the wireframe. Sampling within the mineralised domains at Round Dam is dominated by 1m RC intervals. Nearly

100% of raw sample data from resource drilling at the Round Dam deposit is sampled at 1m intervals.

Gold grades were estimated in a 3D block model within defined domains using ordinary kriging of top-cut 1m composite samples. Estimation parameters were based on the spatial distribution of data and the results of kriging neighbourhood analysis.

Variography to determine the spatial continuity, was applied to gold composites using Supervisor™ software. A normal scores (gaussian) transform was applied to the data to provide a clearer indication of the ranges of mineralisation as the transformation removes the influence of the highly skewed tail of the population distribution.

The variogram parameters were standardised to a sill of 1 and the modelled variograms were then back transformed into raw space. Spherical structures were used for modelling the variograms. Many ore lodes had insufficient data and or poorly structured variograms. The parameters from modelled ore lodes were applied to these domains based on structural/geological similarity. Search neighbourhoods were defined using Kriging Neighbourhood Analysis implemented in Supervisor™. Top cuts were applied to mineralised domains where appropriate.

Ordinary Kriging was selected as the main method to estimate gold grades for the Round Dam deposit where lodes are characterized by moderate to high CV values. Estimation of gold grade was completed in Leapfrog™ software.

For some of the mineralised zones categorical subdomains were created and estimated with Ordinary kriging. Thresholds for categorical subdomains are chosen from log probability inflections that are representative of the geological understanding of grade populations. Typically, only a single low-grade threshold was chosen to allow separation of lower grade zones from higher grade zones within the lode. High grade sub-domains were estimated separately to the low-grade sub-domains using a hard boundary.

Lodes with a low number of samples or discrete lodes with a low coefficient of variation were interpolated by Inverse Distance Squared (ID^2).

The bulk density values were assigned based on the weathering state of the rock and lithology and determined from over 2,165 drill core density measurements and downhole density measurements calibrated for moisture content.

The model has been depleted to account for existing open pit mining.

CRITERIA USED FOR CLASSIFICATION

The model is classified as indicated and inferred based primarily on drill support, but also considering geological and grade continuity and estimation quality.

Wireframe solids were constructed to encompass areas considered to adequately fulfil the requirement to be classified as either, Measured, Indicated or Inferred:

- Measured – No areas of the current resource attained Measured status.
- Indicated – Areas with drill spacing up to approximately 25m x 25mN up to 25m x 40m along strike and with reasonable confidence in the geological interpretation and grade continuity
- Inferred – Areas with drill spacing up to approximately 50m x 50mN up to 50m x 80m along strike and where grade continuity is poorer as defined by a lower sample density, even though geological continuity may be apparent.

Areas of some lodes, particularly at depth have fairly low or no sample support and were not classified.

CUT-OFF GRADES AND MODIFYING FACTORS

Deswik™ software Auto Stope Designer (ASD) was used to produce solids with dimensions of 5mN x 5mRL and a minimum width of 2.5 m. Diluted grades (ore & waste) derived from the ASD's were used to derive a series of optimised pit shells with contractor derived mining costs, projected processing costs with a processing recovery of 95% and wall angles determined by geotechnical assessment. All classified material (Indicated, Inferred) above 0.3 g/t within the optimised reporting shell was reported as open pit resource.

ORE RESERVES – OPEN PIT

Overview of Assumptions, Outcomes and Criteria for Classification

The Ore Reserve for Round Dam was estimated from the April 1st 2026 Mineral Resource referred to above. Aside from historical mining, no depletion of the Round Dam Mineral Resources was required. The Mineral Resource model was a sub-celled Ordinary Kriged model.

The Ore Reserve is reported as at 1 April 2026.

The Ore Reserve was generated from design studies using current costs estimates, geotechnical parameters and dilution and recovery parameters.

Costs were derived from the FY26 budget process and recent contractor cost estimates specific to the Round Dam Project. Unit costs for ore haulage, processing and site overheads were estimated based on scheduled process plant throughput using material above the economic cut-off grade.

The open pit Ore Reserve was estimated using a cut-off grade derived from a gold price of A$3,600/oz. Low Grade Ore was based on a gold price of A$5,000/oz. There are no existing economic surface stockpiles at Round Dam.

No Measured economic Mineral Resource is defined within the Round Dam mining envelope. All Indicated economic Mineral Resource within the mining envelope was classified as Probable following the application of modifying factors. No downgrading of the Ore Reserve classification was considered necessary.

Dilution parameters were based on mining reconciliations of previous DGP open pit operations. The dilution skin method was used to reflect the selective mining method proposed to be used at DGP.

A weight average process recovery of 95% was used in the estimate. This process recovery was based metallurgical test work of fresh and transitional mineralisation with samples tested from Walhalla to Federal Flag North deposits located within the Round Dam Project.

Geochemical testwork is currently underway for waste rock characterisation. The presence of Arsenic, which often occurs in deposits of this nature, has been detected in isolated areas within the mining envelope. This Ore Reserve assumed that the waste material is of a nature it can be managed and stored using conventional WRL construction and rehabilitation methods such as isolation and encapsulation. These results, along with those of detailed geotechnical, hydrological, hydrogeological and environmental studies, will be considered and incorporated into the mine plan during the next study phase.

The Round Dam open pits are located entirely within a granted Mining Lease owned 100% by Ora Banda Mining. The proposed WRLs extend across Mining and Exploration tenements, also wholly owned by Ora Banda Mining. A mining lease application is currently underway to progress permitting of associated infrastructure.

The majority of agreements for Round Dam Project are in place with key stake holders; however, negotiations with traditional owners as well as the management of lithium pegmatites that are in joint ownership with a third party and are associated with Round Dam are still to be concluded.

Mining Method

The Round Dam deposit will initially be mined by open pit methods using conventional mining methods. Ore will be mined using selective mining methods typically used in the Eastern

Goldfields. Load and haul will be carried out using 120 tonne class excavators and 90 tonne dump trucks. This mining approach was successfully used on other Ora Banda open pit projects.

Drill and blast will be carried out using conventional diesel hydraulic blasthole drills and blasting practices, typical of the West Australian Goldfields. Blasting will be carried out on 7.5 m benches using conventional diesel hydraulic blasthole drills and blasting practices, typical of the West Australian Goldfields. The blast hole diameters will vary between 115 mm and 127 mm depending on pattern geometry and proximity to final walls.

Selective mining of the ore will be in the across strike direction. The process will entail separating the blasted waste from the ore at the hanging wall contact, excavating the ore, then separating the ore from the waste at the footwall contract. Ore mining will be continuously supervised by trained ore spotters in direct contact with the excavator operator.

Processing Method

Ore is treated at the DGP using conventional carbon-in-leach (CIL) with some gold recovered via gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. The process plant currently has a nominal throughput rate of 1.2 Mtpa based on a grind size of 106 µm. Several Round Dam Trend deposits, including Walhalla, Federal Flag and Lady Eileen, have been successfully processed through the Davyhurst processing plant during previous mining episodes with similar metallurgical performance.

Test work on Round Dam ores was conducted in 2026. Based on the process plant design criteria (106 µm, 24 hr leach) recoveries of transitional and fresh rock ranged from 93% to 99% for a 95% average with only 0.5% variation between 150-106 µm. An average of 52% of the gold was recovered by gravity. The overall recovery was estimated to be approximately 95%.

Cut-off Grades

The cut-off grade used to define the economic material within the mining envelope allows for ore haulage, crusher loading, processing, site G&A and corporate overhead contributions. Standard state royalties and third party royalties were included. The cut-off grade for high grade at Round Dam is estimated to be 0.7 g/t. The cut-off grade for Low Grade and Surface stockpiles is estimated to be 0.5 g/t. The low-grade material was considered as a blend material to produce a head grade above the 0.7 g/t cut off.

A gold price of A$3,600 per ounce was used in the high-grade cut-off calculation and whilst a gold price of A$5,000 per ounce was used for the low-grade cut-off calculation.

Estimation Methodology, and Modifying Factors

Dilution modelling for the Round Dam open pit Ore Reserve was completed using Auto Stope Designer (**ASD**) functionality in Deswik™ software. Mineable "stope" shapes are created to simulate practical dig blocks. Dilution skins were added to both hanging wall and footwall of the mineralisation and internal and edge dilution was included resulting from forming practical mineable shapes.

A minimum ore mining width of 1.5 m was applied in the dilution modelling process. A 0.5 m dilution skin was applied to both hanging wall and footwall at Round Dam for all of weathering classifications, resulting in an SMU of 2.5m wide. The average dilution is estimated to be 20% at Round Dam. The dilution parameters were based on a subjective assessment of operational performance at previous DGP pits operated by Ora Banda (e.g. Missouri and Riverina).

The ASD optimisation shapes with an average grade below 0.7 g/t and above 0.5 g/t were classified as Low Grade. This material was considered as blend material for the purpose of the economic analysis for this Ore Reserve. All blended material maintained a head grade above 0.7 g/t.

A diluted resource classification (RESCAT_DIL) was created by assigning the dominant RESCAT code of each SMU dig block. Inferred material was not considered in defining the SMU dig blocks; however, due to practical mining geometries a small portion of incidental Inferred material was included within the Ore Reserve. The incidental Inferred inventory was not considered material to the economics of the project.

Background grades were estimated into the resource block model and were included in the dilution modelling. Dilution grades were estimated to be 0.11 g/t for Round Dam.

Ore loss was applied in the ASD process as a result of the variation between mineralised lode geometry and practical dig block geometry. In addition, a nominal 5% ore loss was applied in the mining schedule, to account for further mining losses occurring through normal operations.

Pit Optimisation

Pit optimisation for the Ore Reserve case was completed using GEOVIA Whittle and the same project inputs used for the PFS optimisation, including mining method and selectivity assumptions, Deswik automated dilution shape (ASD) mining shapes, ore loss assumptions, contractor-derived mining cost basis and Mining Cost Adjustment Factors, ore haulage to the Davyhurst processing facility, processing cost estimates, site and corporate overhead assumptions, metallurgical recovery assumptions, royalties and refining charges, and the preliminary geotechnical slope assumptions applied through Whittle slope sectors and domains.

The selected shells shown in Figure 14 report cash costs of approximately A$3,300/oz.

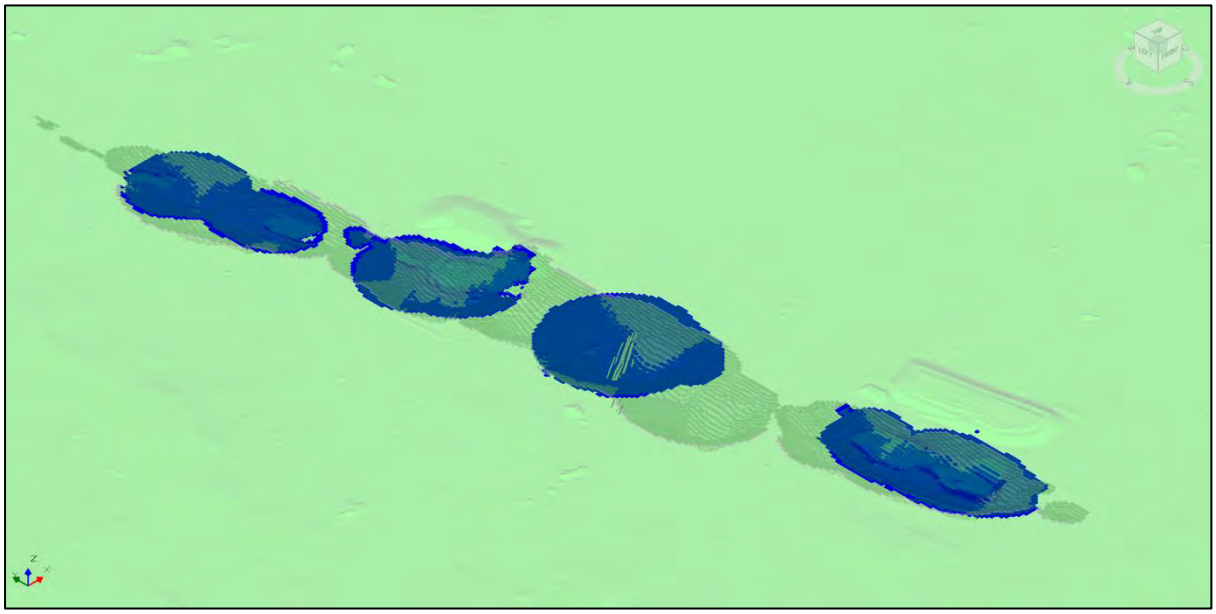

Figure 14 - Round Dam North Block Reserve Case pit shells (blue) shown against PFS pit shells (ghosted)

Pit Design

The pit designs for Round Dam were informed by pit optimisations and assessment of the local conditions and features, as well as geotechnical parameters. The pit optimisation and design were validated against updated cost and revenue inputs for this Ore Reserve estimate.

Five practical pits were designed for the Ore Reserve. From north to south these were: Federal Flag North, Federal Flag, Walhalla North, Walhalla and Mt Banjo. The proposed pits final depth will vary from 65 m to 150 m. The batter angles will vary between 50^0 and 80^0 depending on geotechnical domain and wall orientation. Berms will be between 8 m and 12 m in width, with the batter face heights of 15 m to 30 m. The parameters used were based on geotechnical assessment. The pit ramp widths will be 27 m at a gradient of 1:10 to allow for dual lane travel and 16 m at 1:8 for single lane travel with passing bays at switchbacks and berms. These ramps are intended to accommodate 90t class haul trucks.

The Round Dam pits are shown in Figure 15.

Waste Rock Landform (WRL) designs were prepared for the Round Dam PFS to provide adequate storage for waste mined from the ORE open pits. The designs comprised a Northern, Central and Southern WRL all located to the west of the proposed open pits (Figure 15).

The western WRL locations were selected to avoid sterilising or disturbing potential exploration targets interpreted on the eastern side of the pit corridor. The layout also provided relatively direct waste haulage access from the pit ramp exits.

The WRL designs were based on preliminary landform assumptions of approximately 30 m high, 18 degree final rehabilitation batters and 10 m berms. The designs were prepared as preliminary engineered landforms suitable for mine scheduling and footprint assessment. Further geotechnical, hydrological, geochemical, environmental and closure design review will be required during the next study phase.

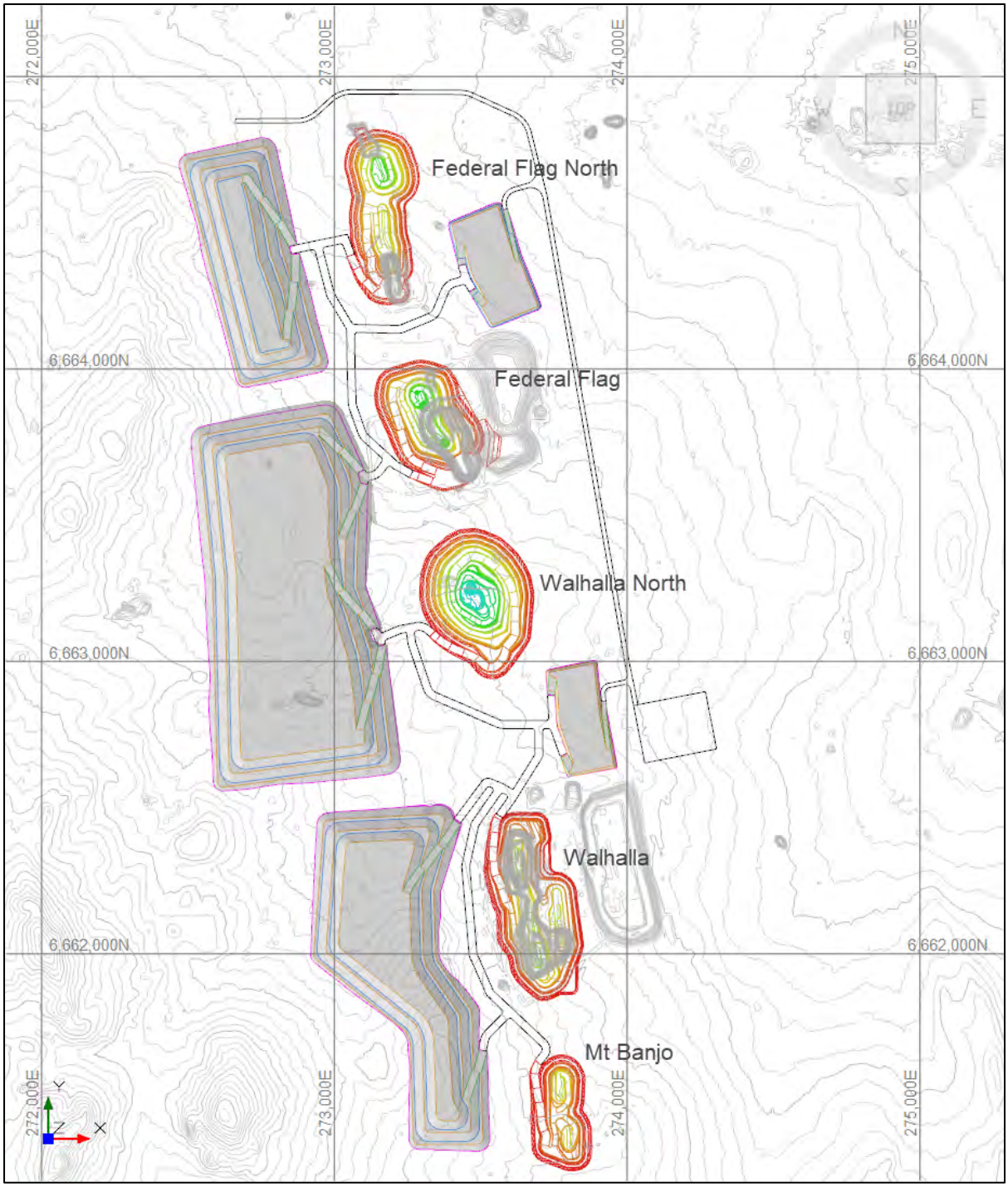

Figure 15 – Round Dam open pit designs showing WRL, MOP and road layout

Geotechnical Design Parameters

The pit wall design parameters used for the Round Dam ORE pit designs were based on the pit design parameter assessment completed in April 2026. The assessment considered previous inspections of existing open pit workings, historical technical reports, and geotechnical assessment work from Waihi, together with subsequent Round Dam-specific geotechnical drilling and logging. The Round Dam-specific work included geotechnical diamond holes drilled between the Federal Flag and Walhalla pits, targeting sedimentary and ultramafic units and lithological boundaries and geotechnical logging of other drillholes.

The geotechnical logging and testing were used to inform rock mass classification by lithology, intact rock properties, discontinuity shear strength and dominant joint sets for basalt, sediment and ultramafic units. Laboratory testing indicated that the ultramafic material was weaker than the sedimentary unit and had lower discontinuity shear strength, making it more prone to sliding. The weathered material properties were variable, with a wide range of measured cohesion and friction values.

The pit wall parameters recommended for the Round Dam design are summarised in Table 18. The parameters include separate treatment of oxide, transitional, fresh basalt / sediment and fresh ultramafic material. Fresh ultramafic material was separated by wall orientation, with lower batter angles applied to the east wall exposure.

Table 18 -Pit Design Parameters by Material Domain

Material / domain	Batter height	Berm width	Batter angle
Oxide	15 m	8 m	50°
Transitional	15 m	8 m	55°
Fresh basalt and sediments	30 m	12 m	80°
Fresh ultramafic – east wall	30 m	12 m	60° to 65°
Fresh ultramafic – north / south walls	30 m	12 m	70°
Geotechnical berm below Transitional material	-	15 m	-

The updated geotechnical assessment concluded that the original preliminary pit design parameters were generally appropriate but recommended a reduced batter angle for fresh ultramafic material on east wall exposures. For these areas, the batter angle should be limited to not more than 65°, with consideration of a 60° batter angle where conditions warrant. A geotechnical berm not less than 15 m wide was recommended at the base of the transitional zone. These parameters were adopted for this Ore Reserve estimate.

The geotechnical design basis remained appropriate for PFS-level mine design but was not considered final for execution. The assessment noted that the available dataset was relatively small compared with the planned extent of the Round Dam open pits. Additional geotechnical drilling, logging, laboratory testing, hydrogeological review, structural interpretation and slope design assessment will be required during the next study phase. A costs allowance for this is included in the economic modelling.

Open Pit Mine Schedule

The project comprises the Federal Flag North, Federal Flag, Walhalla North, Walhalla and Mt Banjo pits. The pits will be mined over a period of approximately 45 months or approximately 4 years using the productivity rates shown in Table 19. The mining schedule is shown in Figure 16.

Pit sequencing prioritises 1 Walhalla North, 2 Federal Flag, 3 Federal Flag North, 4 Walhalla, 5 Mt Banjo.

The mine specific cash flow modelling was based on a gold price of A$3,600/oz. The Round Dam ORE study indicates positive net cash flow outcomes with acceptable returns.

Table 19 - Schedule dig rates

Productivity Rates	
Instantaneous Dig Rate	120t class Excavator
Oxide	500 tph
Trans	350 tph
Fresh	250 tph
Mechanical availability, weather and effective dig hours are further applied	

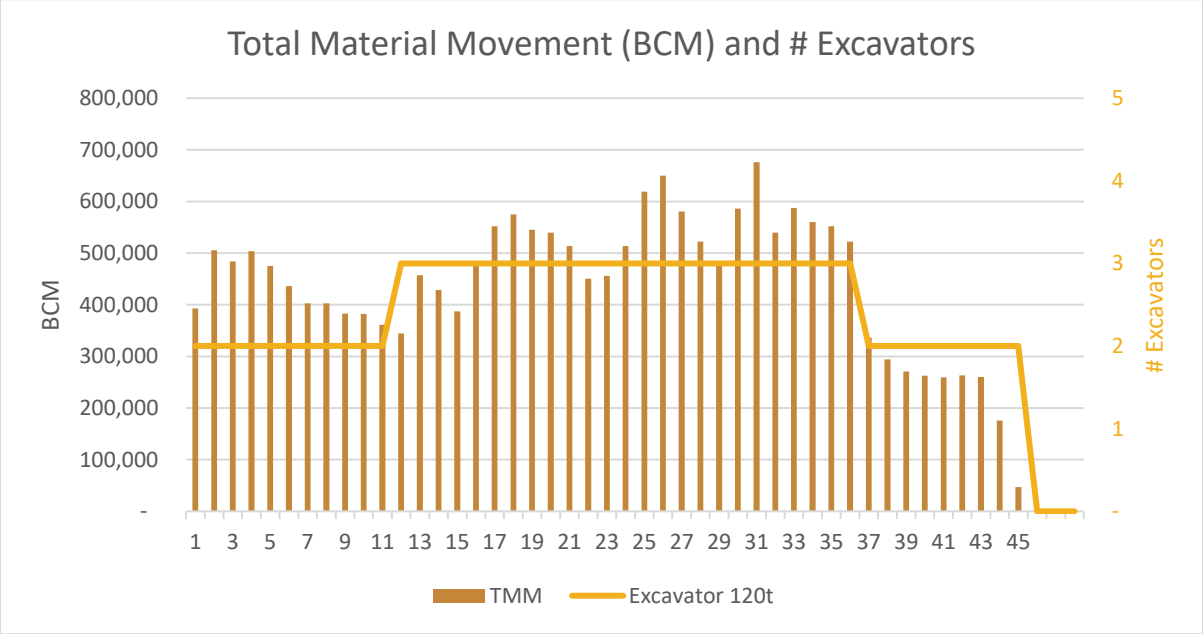

Figure 16 - Schedule # Excavator and TMM's

WAIHI RESOURCE AND RESERVE

SUMMARY

The Waihi Gold Project is a high grade open pit and underground Ore Reserve within 4 km of the Davyhurst processing facility. Waihi offers a high grade option in the longer-term schedule extending mine life. Waihi underground is a material change for the project which has resulted in the addition of 101 Koz and the removal of the Waihi North open pit, -10 Koz. Cost changes have been considered, and the Open Pit Ore Reserve has been estimated using a gold price of A$3,600/oz for the economic analysis representing an increase of A$1,600/oz from previous years Ore Reserve due to a reduction of material mined and tender contract prices.

A summary of the Waihi Mineral Resource and Ore Reserve estimates as at 1 April 2026, are shown in Table 20 and Table 21.

Table 20 - Waihi Gold Project Mineral Resource Estimate

WAIHI GOLD PROJECT MINERAL RESOURCE ESTIMATE[12]:									
	MEASURED		INDICATED		INFERRED		TOTAL MATERIAL		
	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	-	-	3,833	2.2	3,207	1.9	7,040	2.1	466
OPEN PIT	-	-	224	2.3	1	1.3	225	2.3	16
TOTAL	**-**	**-**	**4,057**	**2.2**	**3,208**	**1.9**	**7,265**	**2.1**	**482**

Table 21 - Waihi Gold Project Ore Reserve Estimate

WAIHI UNDERGROUND GOLD PROJECT ORE RESERVE ESTIMATE:									
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	-	-	-	825	3.8	101	825	3.8	101
Inc Golden Pole	-	-	-	*254*	*5.0*	*41*	*254*	*5.0*	*41*
OPEN PIT	-	-	-	200	2.1	14	200	2.1	14
LOW GRADE[13]	-	-	-	157	1.1	6	157	1.1	6
TOTAL	**-**	**-**	**-**	**1,182**	**3.2**	**120**	**1,182**	**3.2**	**120**

[12] Inclusive of Ore Reserve
13 Insitu material contained in both open pit and underground.

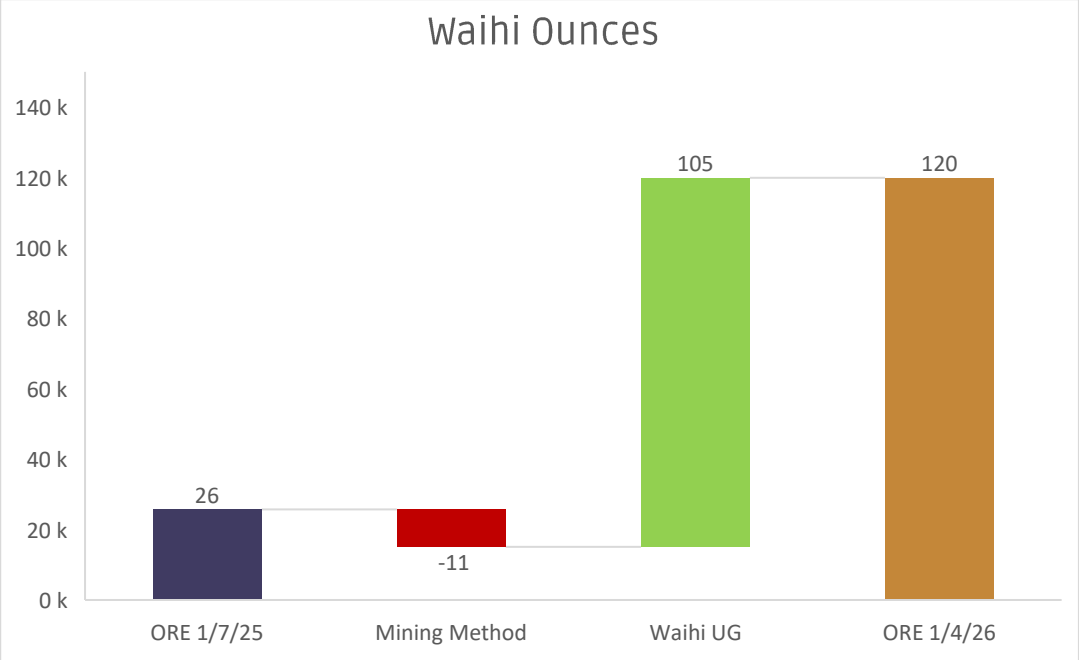

Figure 17 - Waihi ORE Oz change

INTRODUCTION

Tenement

The Waihi Gold Project is located on the granted mining tenement M30/255, which is 100% owned by Carnegie Gold Pty Ltd, a wholly owned subsidiary of Ora Banda. On 30 October 2023, the Ora Banda Group entered into a binding Farm-In JV Agreement with Davyston Exploration Pty Ltd ("Davyston"), a wholly owned entity of the Wesfarmers Chemicals, Energy & Fertilisers division ("Wesfarmers"). Under the agreement, Davyston acquired an initial 65% rights to all other minerals, except for gold and its byproducts. To date, Davyston has successfully earned into an additional 6%, such that the joint venture currently sits at 71% Davyston and 29% Ora Banda Group. Ora Banda holds the rights to gold and its byproducts over all of the tenements.

There are no known heritage or native title issues within the tenement. The tenement is in good standing with DMPE with no known title risk.

Permits and License

The required environmental approvals to operate the Waihi open pit mine are in place. The project remains compliant with all the current permitting requirements, and as such they remain in full force.

- Waihi Gold Operations Mining Proposal and Mine Closure plan (Reg Id 120936).
- GWL 180490 (3)
- Clearing permit 8882-2

The MDCP addendum for Waihi underground mine and infrastructure has been submitted for approval. The regulator is familiar with the project with the approval expected to be received prior to planned commencement.

Mine Infrastructure

Waihi Gold Project is located 120 km northwest of Kalgoorlie, 3.5 km to the west of Davyhurst processing plant and 5 km from the Davyhurst village and 120 km northwest of Kalgoorlie.

The existing features of the Waihi project consists of 3 adjoining in-pit tailings storages over the historic Waihi and Golden Pole underground mines. These underground mines were developed in the early 1900's and the open pits were mined from mid 1980's to late 1990's by various companies. The pits mined in the mid 1980's were later filled with tailings from the Davyhurst plant in the 2000's. There is an approved pipeline corridor and haul road from Davyhurst to Waihi.

The site contains a rehabilitated waste rock landform and a smaller legacy waste rock landform along with ROM pads and various access and haul roads. The rehabilitated waste rock landform is under post closure monitoring.

Key Changes from ORE 1-7-25

The Waihi open pit ORE has reduced to a single Central Pit due to the underground ORE design being the preferred method of mining for the North/Homeward bound orebody.

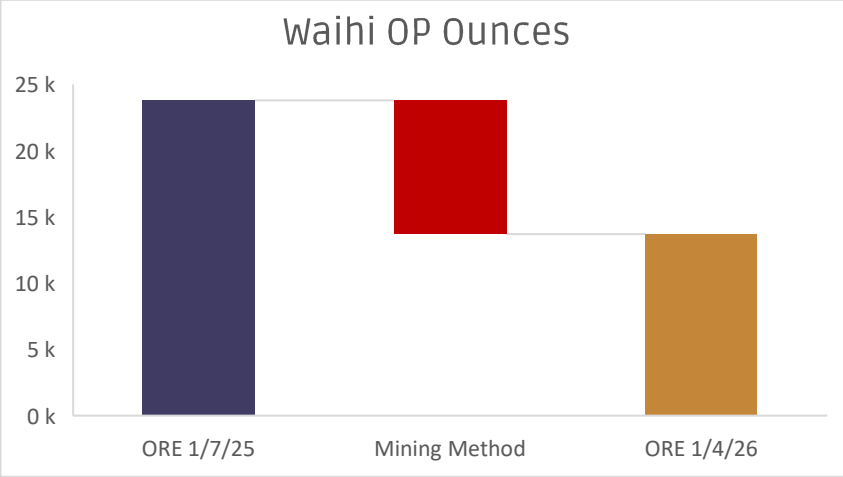

Figure 18 - Waihi OP ORE Oz change

Figure 19 - Waihi Existing Surface Features 1 APR-26

MINERAL RESOURCES

Mineral Resource Estimation: Summary Information as required under Australian Securities Exchange (ASX) Listing Rule 5.8.1 follows.

GEOLOGY & GEOLOGICAL INTERPRETATION

Lithology

Waihi and Golden Pole are the northern-most exploited gold deposits in a chain of deposits which stretch at least 14 km to the south along the Round Dam trend. Waihi and Golden Pole are located within the Coolgardie Domain of the Kalgoorlie Terrane, Eastern Goldfields Province, Western Australia. The deposit is hosted within Archaean mafic to ultramafic volcanic rocks of the Hampton Hill Formation, comprising a fractionated ultramafic to mafic volcanic sequence. The variation from ultramafic to more evolved basaltic rocks is interpreted to result from differences

in mantle melting and magma composition over time. The package is metamorphosed from upper greenschist to lower amphibolite facies.

Younging is established from east to west and defined by volcanic progression of the fractionated Hampton Hills formation transitioning from primitive in the east to more evolved basaltic flows on the west. Triple junction margins in less deformed pillow basalts provide additional younging indicators.

The Golden Pole Basalt forms a key upper stratigraphic marker above the Hampton Hills volcanic sequence. This unit is interpreted to correlate with the Gleesons Basalt, which is regionally overlain by sulphidic carbonaceous to graphitic shales, potentially equivalent to the Centenary Shale.

Lithogeochemistry obtained from portable X-Ray Fluorescence (pXRF) provides a reliable method for differentiating volcanic units and confirming stratigraphic position where visual logging alone is insufficient or difficult due to metamorphic and hydrothermal alteration. Elements such as Cr, Ni, Ti, and Zr are especially effective in discriminating ultramafic flows, komatiitic basalts, mixed chrome basalts and more evolved tholeiitic units. Lithologies in the area strike just west of N-S, and dip steeply to the west (>75°). Structurally Waihi has undergone a multitude of shortening events with rock fabrics displaying crenulations and a pervasive west dipping foliation.

All units are intruded by late-stage lepidolite bearing pegmatite dykes.

Structure

Regionally, Waihi is situated between the Zuleika Shear and the Ida Fault and therefore in the northern portion of Coolgardie Domain. The greenstone belt in this area is constricted by surrounding granitoids, resulting in higher metamorphic grades (upper greenschist to lower amphibolite). Across the district, mineralised trends and stratigraphy south of Waihi are predominantly north-south striking. At Waihi, however, the sequence deviates from this orientation to NNW and is interpreted to represent a regional flexure within the Round Dam trend.

The Waihi deposit exhibits a spaced to penetrative foliation with an overall orientation of -70° towards 256°, however, this orientation can rotate to -70° towards 270° and is concordant to sub-parallel to bedding with the orientation of bedding supported by pXRF data.

Across Waihi, mineralisation in the 320° to 330° orientation hosts the most metal and often the best grades. Mineralisation in this orientation includes Homeward bound (lithological contact), Waihi South (lithological contact) and Golden Pole (structural-shear control). The Homeward Bound lodes are positioned on the lithological contact between the ultramafic to the east and tholeiitic basalt to the west, striking ~330°. All lodes within this pit are orientated 330◦ which mirrors the attitude of the lithological contact and grade plunges 50° towards 330°. Mineralisation at Waihi South is strongly lithologically controlled. Structural interpretation suggests a dip-slip flexure that may localise the high-grade shoot. At Golden Pole (GP), lodes begin in the south tracing a lithological boundary of low-to-high-zirconium before deviating and taking a 330° orientation. Mineralisation in Waihi Central and North is associated with NNW striking (350°), steep west dipping shears

Key structural characteristics include:

- Shears are subvertical to steep west dipping and strike ~320° to ~350°.
- Shears exploit lithology, diffract in out of contacts creating anastomosing geometries
- Where shears intersect lithological contacts high grade shoots can develop (-40 towards 330°)
- Local flexures or irregularities along lithological boundaries may focus fluids also providing high-grade shoots (local folding?).
- Foliation dips ~-70° toward ~256°.

Alteration & Mineralisation

The principal mineralised zones are characterised by biotite alteration related to potassic metasomatism (Biotite – Silica – Feldspar – Actinolite). This alteration is focused within the ductile shear zones and forms biotite-rich schistose units containing disseminated sulphides dominated by pyrrhotite with accessory chalcopyrite and trace arsenopyrite. Pyrite occurs locally and appears to have a strong spatial association with gold mineralisation. Petrographic relationships suggest pyrite formed during a later stage of sulphide development, possibly reflecting increased sulphur fugacity or minor oxidation during continued fluid–rock interaction.

Shear zones also acted as conduits for high-temperature metamorphogenic fluids that produced distinctive calc-silicate alteration assemblages comprising diopside, tremolite–actinolite and minor microcline. These calc-silicate assemblages locally overprint earlier biotite-altered units and are associated with elevated temperature fluid–rock interaction. Ductile shear zones potentially acted as long-lived structural conduits that enabled repeated pulses of metamorphic fluids to circulate through the host rocks and contribute to the development and remobilisation of gold mineralisation.

Scheelite is observed along the Golden Pole line of lode and displays a strong correlation with high-grade gold mineralisation as do the margins between calc-silicate and biotite alteration zones, suggesting that these alteration boundaries acted as favourable sites for fluid focusing and gold precipitation.

Weathering

The weathering profile in the area is poorly developed with much of the area covered by thin soils, or fresh sub-cropping amphibolite. In the old Waihi Pit saprolite and weathered bedrock occur to a maximum depth of approximately 25m within the exposed ore zones. In the Homeward bound pit weathering is negligible. Depth to fresh rock increases to the West over the mafic and sediment lithologies. The east is dominated by more ultramafic lithologies with a corresponding shallower weathering profile.

DRILLING TECHNIQUES

Modern exploration at Waihi commenced in the early 1980s by WMC and Billiton Australia and was followed by numerous operators who held the tenure at various periods since. Although a significant proportion of drilling data is from previous operators, it is generally well documented and to industry standards of the time. In addition, OBM has added significant drilling to the Waihi deposit. All RC and diamond drilling at the deposit is deemed suitable for resource estimation purposes. Previous operators include WMC, Billiton, Consolidated Exploration (Consex), Consolidated Gold (Consgold), Croesus and Eastern Goldfields Ltd. (EGS).

Billiton Australia

RAB holes were closely spaced or overlapping for exploration and mapping in areas of poor outcrop. RC drilling was completed in areas of known mineralisation, principally to obtain reliable samples. Diamond drilling was done in areas which required a better geological understanding and where RC drilling proved to be too slow due to hard ground. RC drilling was by Aquadrill, ACDC and Stanley who all employed roller/blade and hammer drill bits. Diamond drilling was by Aquadrill, Stanley and Wallis. All drilling was NQ core size.

Geology logging was predominantly qualitative noting RQD, lithology, mineralisation, alteration, weathering, veining and fracturing. Percentage quartz was noted.

Western Mining Corporation

Reverse Circulation drilling was completed by a Schramm rig. Drill lines were established by tape and compass from a previously surveyed AMG baseline transecting the lease.

Geology logging was predominantly descriptive, percentage quartz was noted.

Consolidated Exploration

RC drilling with 11.4cm rods and 19.9cm button bits. Sample collection was via a crossover sump located 1m up the rods from the hammer cutting face. Drilled on local grids (possibly truncated AMG84, zone 51). Holes appear to have been surveyed using AMG zone 51 grid at a later stage. Numerous vertical holes not down-hole surveyed. Downhole surveys when performed were by undocumented method with a 9m interval average.

Lithological logging was qualitative for lithology, colour, alteration and grainsize (at times). Quantitative logging of quartz mineralisation was sometimes done.

Cons Gold/DPPL

Reverse Circulation drilling was done by various drilling contractors. Boosters and auxiliary compressors were required to penetrate the hard ground. Hole diameter varied between 4.25 inch and 5.5 inch, depending on contractor. Stabilisers were used to control hole direction. A face sampling hammer was used. Diamond drilling was done by Strata Drilling using a Longyear 44 rig. Hole diameters were NQ though HQ triple tube was used for geotechnical drilling at Waihi. Core was oriented and geologically logged and photographed. Intervals of shearing or alteration were cut using a diamond saw and half core submitted to the laboratory. RAB drilling was done by Bostech to blade refusal.

All drill collars were surveyed by licensed surveyors. RC resource holes were downhole surveyed by either wireline multishot camera, Eastman single shot camera using an aluminium barrel to minimise magnetic interference, or electronic gyro compass.

Logged geology included lithology, colour, oxidation, alteration, with grainsize, texture and structure (diamond drilling). Quantitative logging of Quartz veining was done. Logging was entered directly into HPLX200 data loggers.

Croesus

All RC drilling was by either Drillcorp or Drilltorque. Hole diameters were not recorded. Collars were picked up by DGPS or Theodolite. WHRC series RC holes were downhole surveyed every 10m by Electronic multishot or other unrecorded method. WSRC series holes were not down hole surveyed.

Qualitative logging of lithology, colour, grainsize, alteration, oxidation, texture, structures and regolith was done. Quartz veining and mineral intensity was logged quantitatively.

Eastern Goldfields/Ora Banda Mining

All RC holes were 5-inch diameter, drilled using a face sampling hammer with samples collected under cone splitter. Diamond coring generally started with HQ3 coring to approx. 40m, then NQ2 to bottom of hole. Early core (2016 and 2019) was oriented by reflex instrument 2025 drill core was oriented by an axis instrument. 2016 and 2019 drill hole collar positions are picked up using a Trimble DGPS subsequent to drilling by a licensed surveyor. Drill collars from 2023 and 2025 programs were picked up by the mine surveyors using RTKGPS. Drill-hole downhole surveys of 2016 and 2019 holes were recorded every 30m using a reflex digital downhole camera. Some RC holes were not down-hole surveyed if they were short. Later RC and DD holes were downhole surveyed by north seeking gyro (reflex). Diamond drill recoveries are recorded as a percentage calculated from

measured core against downhole drilled intervals (core blocks). RC sample weights as received by the laboratory are recorded and monitored.

Qualitative logging of lithology, colour, oxidation, grainsize, texture, structure, hardness and regolith was completed. Quantitative logging estimates were made of quartz veining, sulphide and alteration percentages. Core was photographed.

SAMPLING AND SAMPLE ANALYSIS

Billiton

RAB samples were collected every metre but 2m composites were despatched for assay. RC samples were collected and assayed every metre. The assay method employed is unknown but is assumed to be Aqua Regia digest. The sample submissions included standards and field duplicates, but no information is currently available for assessment.

Consolidated Exploration

RC samples were collected from a standard cyclone and split through a 3-way riffle splitter to obtain a 2-3kg sample. Samples were collected every metre and submitted at 1 metre intervals or as 2m composites. Where composite gold grades were >1 g/t the individual samples were resubmitted for analysis. All samples were weighed before splitting to monitor sample recovery and bias. A 3-metre plastic pipe was inserted into the cyclone vent to minimise sample loss and the drill hole was partially pressurised to maximise sample recovery. The cyclone was washed at the end of each hole or if water was intersected.

All samples were analysed by Genalysis. RAB 1m samples were usually dispatched as 3m composites but occasionally as 1m samples. RC composite 2m samples were hammer milled, mixed and split to 200g then pulverised to 200 mesh size. 1m samples were single stage mix and ground to 200 mesh. Phase 1 drilling was analysed for gold by standard wet chemical multi acid digestion and AAS. The second phase samples were pre-roasted. Any results of >1g/t Au or samples in proximity to ore grade intersections were re-assayed by fire assay using a 50g charge. Genalysis carried out check assays using either wet chemical, pre-roast or fire assay techniques.

Consolidated Gold/DPPL

RAB 1m samples were composited to 4m using a PVC pipe as a spear. RC samples were collected at 1m intervals of the cyclone and homogenised by a 3-stage riffle splitter. Intervals of 2-3 kg weight showing alteration or shearing were submitted as 1m samples to either ALS of Kalgoorlie or Amdel of Kalgoorlie. Remaining intervals were composited to 4m. Any composite returning >0.19 g/t Au was resubmitted as individual samples. Sample preparation was by jaw crushing (if necessary) followed by total sample pulverising using a mixer mill. A quartz blank was pulverised between each sample to minimise carry over. All assaying was by fire assay, 50g charge. For infill drilling, standards supplied by Garnet Laboratories were routinely submitted to monitor assay accuracy. Cons Gold also undertook checks on the assay quality by:

- submitting field duplicate samples every twentieth sample
- Umpire laboratory checks
- Screen fire assay of selected high grade samples.

Croesus

RC drill samples were collected in large plastic retention bags below a free-standing cyclone at 1m intervals, with analytical samples initially formed by composite sampling over 5m intervals. Composite samples were formed by spear sampling. A 50mm diameter plastic pipe was pushed through the drill cuttings in the sample retention bag to the base of the bag and removed carefully

with the contents of the pipe containing a representation of the retained metre. Wet RC drill samples were thoroughly mixed in the sample retention bag and 'scoop' sampled to form a composite sample. Five metre composite analytical samples, returning values greater than 0.1g/t gold, were riffle split at 1m intervals, were samples where dry, and grab sampled where wet.

All RC composite and 1m split samples were analysed for gold (Fire assay/ICP Optical Spectrometry) by Ultratrace Laboratories in Perth. The analytical samples were dried, crushed and split to obtain a sample less than 3.5kg, and then fine pulverised prior to a 50gm charge being collected and analysed. Every 20th composite and split sample was duplicated in the field and submitted to monitor laboratory precision.

Assay standards supplied by Gannet Laboratories and uncertified blanks were also submitted with every batch of 1m split samples, as a more precise form of quality control.

Eastern Goldfields/Ora Banda Mining

RC samples were submitted as individual samples taken onsite from the cone splitter. The core sample intervals were selected by a geologist and defined by geological boundaries. Half-core samples were cut by saw. Samples from 2016, 2017, 2019 and 2023 were dried, crushed, split, pulverised and a 50gm charge taken for analysis by an accredited laboratory (Intertek Genalysis, SGS or Nagrom). The 2025 drill program samples were crushed on-site in Orbis crushers and a ~400g sample split into a jar for photon analysis at SGS laboratories in Kalgoorlie or Perth. Field duplicates, blanks and standards were submitted for QAQC analysis from all drill programs.

ESTIMATION METHODOLOGY

The resource model is interpreted to a 0.4 g/t cut-off grade guided by presence and intensity of quartz veining, alteration and sulphides. Extensive use was made of core photographs to aid lode interpretation. The 0.4 g/t value is indicative of the onset of mineralisation at the margins of shear zones. A cumulative frequency plot of the all the resource drilling assays revealed a slight inflection point near 0.4 g/t and this value was taken to represent the boundary between mineralised and un-mineralised material. A minimum of 2 m downhole width above 0.4 g/t defined a potential lode. Internal dilution was sometimes greater than 2m, but this was accepted given reasonable continuity evident at the 0.4 g/t cut-off. Sometimes lodes were pushed through drill holes with grades below 0.4 g/t in order to maintain continuity. Where several consecutive sample intervals of ~0.4 g/t were present on the margins of mineralisation, the outer samples were omitted from the lode interpretation. Lodes were generally interpreted on E-W sections and flitches using Leapfrog™ software.

Raw assay samples were composited in Micromine™ software prior to estimation. Raw samples were assigned to the mineralisation wireframe they fall within. Downhole compositing was completed for each hole, the compositing starting from the point where the hole enters the wireframe. A minimum composite length of 0.30m was accepted as this was the minimum sample width from recent diamond drill program. Any residuals (<0.30 m) were distributed across the lode interval. Only composite samples within wire framed mineralisation domains were used in the estimation.

The plunge is moderate (39º) towards the north and is consistent with observed geological structures (fold hinges and boudin necks) in diamond core and field mapping. Selected lodes with high variability and high maximum grades were selected for top cutting to reduce the influence of the high grade composites.

Selected lodes with high coefficient of Variation (CV) and high maximum grades were selected for top cutting to reduce the influence of the high grade composites. Top cutting was generally applied

using Micromine™ top-cutting tools to domains with a COV of >1.7 and values were determined by disintegration analysis of the probability curve and visual inspection of the histogram.

Variography to determine the spatial continuity, was applied to gold composites using Supervisor™ software. The principal axes of anisotropy were determined using variogram fans based on the normal scores transformed data. Downhole normal scores variograms were modelled to determine the normal scores nugget effect. The variogram parameters were standardised to a sill of 1 and the modelled variograms were then back transformed into raw space. Spherical structures were used for modelling the variograms. Maximum continuity for Waihi Main lodes is in a plane striking roughly 327° and dipping steeply west. The plunge is moderate (40°) towards the north. The moderate northerly plunge is consistent with geological observations in diamond core.

Block model block sizes are 4mE x 10mN x 10mRL with sub-celling to 0.5mE x 1.0mN x 1.0mRL. Supervisor™ software was used for Kriging Neighbourhood Analysis (KNA) to assist with defining the estimation neighbourhood. Parameters defined by KNA were optimal block size and search distances, minimum samples and discretisation. Maximum and minimum samples were set at 16 and 6 respectively. Search parameters, to be used in the primary search were at or greater than the maximum range of the modelled variogram. Estimation was completed in 3 passes with an expanded search and reduced minimum samples for each successive pass. Dynamic anisotropy (DA) was applied to the domain estimation. DA changes the local search orientation to mirror local changes in lode orientation. Micromine™ software was used for the Estimate.

Distance thresholds were applied to selected lodes to control the influence of high grade composites at larger distances from the block being estimated. Clamping reduces the grade of high grade composites if over a specified search distance from the block being estimated.

Density readings were taken from diamond core samples using the Archimedes method. A total of 1,716 readings were collected and results were applied according to oxidation state and lithology.

CRITERIA USED FOR CLASSIFICATION

Existing mining at Waihi has confirmed steep west dipping to sub vertical north-west striking mineralised lodes. Where lodes are defined by two or fewer drillholes, they have been classified as inferred.

- Measured – No areas of the current resource attained Measured status.
- Indicated – Areas with drill spacing up to approximately 30m x 30mN with reasonable confidence in the geological interpretation and grade continuity
- Inferred – Areas with drill spacing up to approximately 60m x 60mN along strike and where grade continuity is poorer as defined by a lower sample density, even though geological continuity may be apparent.

Areas of some lodes, particularly at depth have fairly low/no sample support and were not classified.

CUT-OFF GRADES AND MODIFYING FACTORS

The Waihi Underground Mineral Resource is a diluted resource reported at a diluted cut-off grade of 0.8 g/t within Auto Stope Designer (ASD) solids with 10mN x 10mRL dimensions and minimum 1.6 m width. A portion of Waihi is intended to be mined by open pit methods. All stope shapes within

the open pit design were excluded from the Underground report (Figure 20). All fresh material within MSO shapes outside the planned open pit design are included in the Underground report. All Indicated and Inferred material within the pit design and above a cut-off grade of 0.5 g/t is included in the Open Pit report.

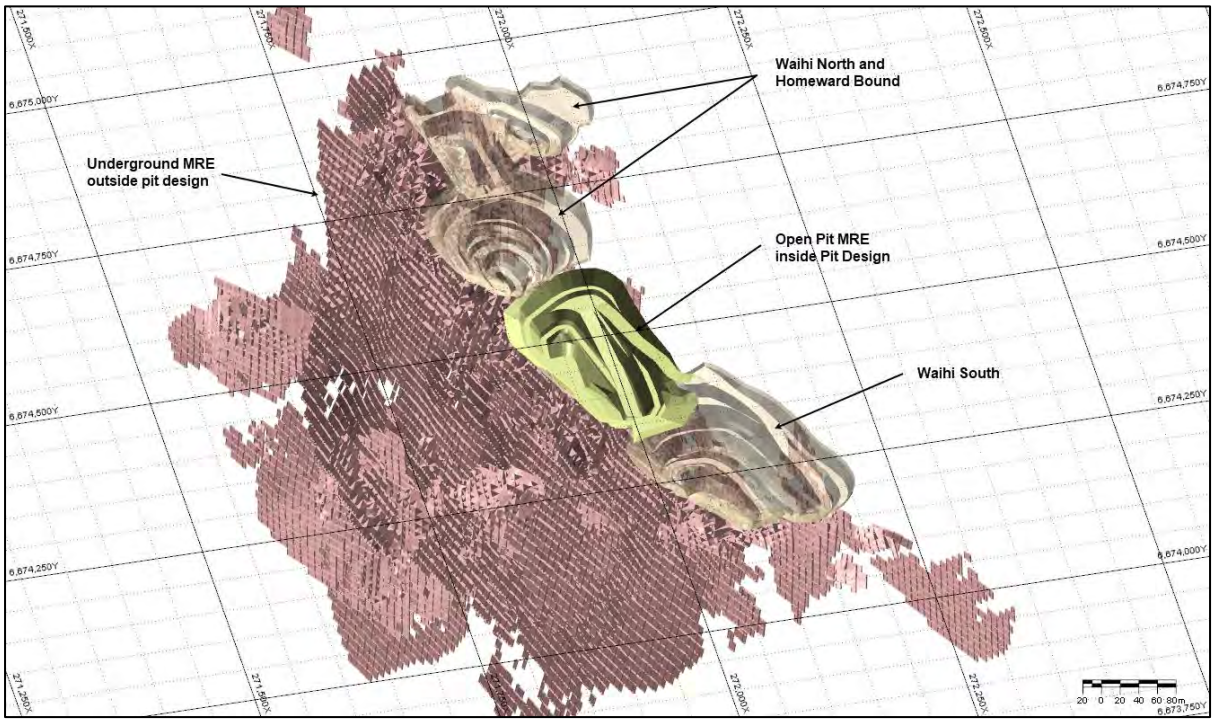

Figure 20. ASD solids outside open pit design included in Underground Mineral Resource Reporting

PROCESSING METHOD

The process for treating ore at the DGP is conventional CIL with some gold recovered via a gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. Waihi gold recoveries from fresh material average 90%.

ORE RESERVES – UNDERGROUND

Material Assumptions and Outcomes, Criteria for Classification

The Ore Reserve was derived from technical studies incorporating project-specific costs as well as geotechnical analysis, dilution and recovery parameters and is based on the current 2026 MRE. Processing parameters were based on test work combined with historical processing recoveries. Hydrogeological conditions were determined from historic mining of the Waihi pits and Golden Pole underground, as well as information obtained from extensive Resource drilling.

Costs were derived from the FY26 budget estimate including contract pricing from OBM's operating underground mines current at the date of this Ore Reserve. Unit costs for haulage, processing, site administration and head office overheads were calculated using the combined project cost model with the Ore Reserve mine schedules and stockpiles.

The Waihi Underground Ore Reserve was estimated using a gold price of A$2,500/oz.

The dilution skin method was employed to reflect the selective mining method proposed for Waihi Underground. Dilution parameters were based on a geotechnical assessment of the expected mining environment and nearby operating mine experience. A cut-off grade of 2.2 g/t was applied to determine economic mining envelopes using Deswik™ ASD. Costs derived from the FY26 budget including contract pricing from OBM's operating underground mines current at the date of this Ore Reserve were used to validate the Ore Reserve cut-off grades.

Mining extraction ratios for the underground Ore Reserve is dependent upon the dimensions and spacing of pillars throughout the orebody. The Waihi mine design assumes 40 m open stopes (along strike) and pillars of 5 m by 17.5 m. The 40 m stope strike extents are considered a practical distance over which to successfully operate remote loaders to recover ore from open stopes. There are isolated areas with six stopes > 7.5m wide, stope strikes are limited to no more than 25m and ribs of 10m. Sill pillars have been considered via a stope recovery of 72% where stoping extends more than 4 levels down dip on a mineralised lode. A 5% stope ore loss was also included for operational losses. A weighted average extraction ratio is estimated to be 82% across the Waihi underground.

Mining Method

The underground mine design is premised on a conventional longhole open stoping mining method, commonly used in the Western Australian Goldfields.

Mining equipment will be mechanised, with equipment to include electric-hydraulic drills for development and production, and rubber tyred loaders and trucks for load and haul activities. Production loading will incorporate conventional and tele-remote loading for non-entry mining stopes.

Based on the geotechnical assessment, which identified favourable ground conditions and low stress environment, as would be expected at the shallow mining depths of no more than 220mbs, no stope backfill is contemplated.

Cut-off Grades

The Waihi Underground cut-off grade was calculated to be 2.2 g/t for production stoping ore. The cut-off grade calculation was estimated at a gold price of A$2,500/oz, and is inclusive of mining, transport, processing, overheads, sustaining capital and royalties.

A cut-off grade of 1.7 g/t was applied to the underground development based on the incremental cost of developing hauling and processing of the ore. The calculation was estimated at a gold price of A$2,500/oz.

Low Grade insitu material is 0.5 g/t to 1.7 g/t, based on the surface SP cut-off where haulage, processing, admin costs are applicable and using a gold price of A$5,000/oz.

OBM underground operating mine contractor costs and OBM budget costings were used.

The WA state royalty of 2.5% NSR plus a 1% NSR Private company royalty apply.

Processing Method

The process for treating ore at the DGP is conventional CIL with some gold recovered via gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. The process plant has a nominal throughput rate of 1.2 Mtpa based on a grind size of 106 µm. The process plant has been successfully operated at this rate with recent improvements made. The processing recovery applied to Waihi Underground was 90% and was based on metallurgical test work. The recovery performance was 92% through Davyhurst plant in FY26 to EOM

March-26 processing Riverina and Sand King ores which have an average metallurgical test work recovery of 88%.

Estimation Methodology, and Modifying Factors

Given the nature of the mineralisation, the global dilution, inclusive of stoping and ore drive development, equates to 29% of material. Background grades were estimated into the block model and were included in the dilution modelling. Dilution grades varied between zero and 0.5 g/t depending on the nature of the alteration halo. The global average grade of dilution was estimated to be 0.14 g/t. Dilution being all included material less than 0.5 g/t.

Delineation of economic stoping areas was completed using Deswik™ software. Mineable "stope" shapes were created to simulate fully diluted stope blocks. The stope shapes are then depleted by development ore drives and modifying factors are applied in the mine schedule. Stope selection was optimised using a cut-off grade of 2.2 g/t.

A minimum stope mining width of 1.6 m was applied in the dilution modelling process, with an additional 0.6 m dilution skin applied to all valid stope shapes (0.3 m hanging wall and 0.3 m footwall). In addition, a nominal provision for unplanned dilution of 20% @ 0 g/t for stopes < 3.5m wide (57 stopes) and 10% @ 0 g/t for stopes >3.5m wide (37 stopes) was also included as a contingency to all stoping panels.

Inferred material was not considered in defining the stoping envelopes; however, due to practical mining geometries a small portion of incidental Inferred material is included within the Underground Ore Reserve. This material occurs at the edges of the mining envelope and is estimated at approximately 17 kt at a grade of 4.6 g/t without application of modifying factors and represents 2% of the Waihi Underground Ore Reserve ounces and is not relied upon for economic extraction. The incidental Inferred inventory was not considered material to the economics of the project. The RESCAT for each scheduled task was attributed with the RESCAT of the dominant mass of material above 0.5 g/t with all tasks being Indicated Material.

The economic viability of the Waihi Underground was confirmed using current commercial parameters in a project evaluation cash flow model inside the greater multiple mine company model. This model also considered project phasing, stockpiling, sustaining capital and the effect of fixed costs. The cash flow modelling was based on a gold price of A$3,600/oz. Based on the assumptions outlined in this report, the mine indicates positive net cash flow outcomes. After the mine is operating in commercial production the overall unit mining costs for the underground was estimated to be A$193/t ore, inclusive of sustaining capital.

Mine Design

The mine design for the Waihi Underground on which this Ore Reserve was based is shown in Figure 21. The mine entries consists of main access portals to Golden Pole/Waihi (west) and to Homeward Bound (east) with a primary ventilation portal and a surface return air rise in the east. All portals are located in the interpreted fresh rock portion of the existing Waihi pit.

The primary ventilation is via a vent portal to the Waihi open pit for the western decline and via a surface raisebore for the eastern decline. Return air drives are designed 5 m x 5 m with vertical rises ~6 m x 4 m. The system can meet the demand at various stages of mine life including the Ore Reserve design and schedule.

Underground pump stations are in place and have been allowed for in the design. Mine dewatering is further pumped 600 m to a water settlement with 8,500 kl capacity. A 3.5km pipeline to the

processing plant and 1.5km pipeline to a nearby pit also offer water storage capacity. Dewatering pipelines are capable of 40 l/s and pumps to suit demand.

The decline design is 5.5 m wide x 5.7 m high with a typical gradient of 1:7. Ore drives are designed to be 4.5 m wide x 4.5 m high. The average floor to floor slope distance between levels is set at 22 metres, with an average stope panel height of approximately 17.5 metres. Stope parameters used in the Waihi mine design are shown in Table 22.

The Waihi Underground Geotechnical Report provides stope and pilar analysis and guidance in line with the stope parameters used. Crown pillars have been designed no less than 10m for stopes <5m thick and 15m crown pillars for stopes >5m thick. The 15m crown pillars have drill drive from which rockmass classification can be determined and suitable ground support can be installed if required.

Table 22 - Waihi stope parameters

Stoping Parameters		
Sub-Levels	22	m
Min Stope Width	1.6	m
Dilution FW	0.3	m
Dilution HW	0.3	m
Stope Length	~40	m
Ave Stope Width	3.6	m
Rib Pillar Width	5-10	m
Sil Pillar Recovery	72	%
Sil Pillar frequency	~88	m
COG	2.2	g/t
Schedule Dilution	10-20%	0g/t Dilution
Schedule Recovery	95%	

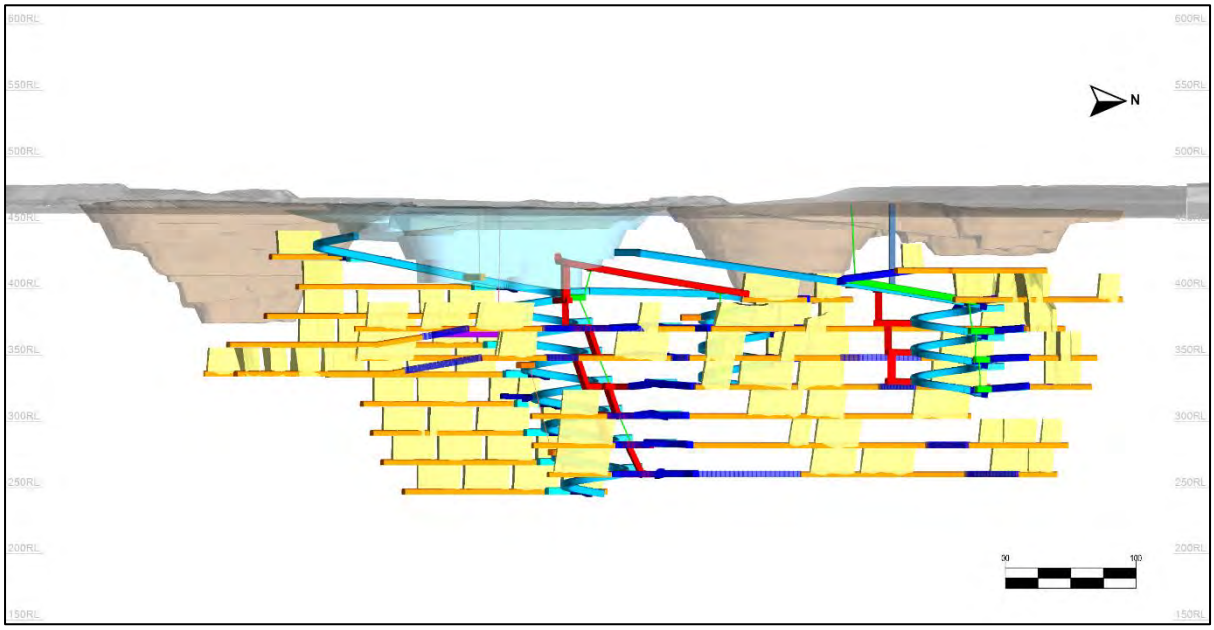

Figure 21 - Waihi Underground Ore Reserve mine design with Waihi pits (looking west)

Waihi Underground Mine Schedule

A mine schedule for the Waihi Underground Ore Reserve was developed, with productivity rate assumption in line with contractor expectations.

The mining sequence assumes top-down echelon mining with no current plans to backfill stopes.

The primary mining equipment levels on which the mine schedule was based are shown in Table 23. The ORE schedule was used in the economic assessment.

Table 23 - Waihi primary mining equipment levels

Equipment		
2x Jumbo	Sandvik DD421	Twin Boom
2x Long Hole Drill	Sandvik DL431	76+89mm holes
3-2x Loader	Sandvik LH517	17T
2-3x Truck	Sandvik TH663	60T

Economic Assessment

An economic assessment was carried on the Waihi Underground to validate the Ore Reserve Financials. The cash flow was modelled in real terms on a pre-tax basis. Recovery and revenue parameters used were as described above.

Costs were derived from the FY26 budget estimate, the Waihi FID and contract pricing from OBM's operating underground mines current at the date of this Ore Reserve.

Mining overheads were based on OBM budget provisions for supervision and technical support, as well as contractor fixed costs, general operating expenses, FIFO flights and accommodation. Dayworks provisions were also included for miscellaneous works during operations as well as closing of the site.

Unit costs for haulage, processing, site administration and head office overheads were calculated using the combined project cost model with the Ore Reserve mine schedules and stockpiles.

An allowance for capital has been used in the economic modelling and based on recent actuals and FID planning. The allowance covers:

- Various surface infrastructure and buildings,
- Surface Power station, UG sub stations with HV cabling,
- Portal façade works,
- Dewatering and mine water pipeline and pump stations,
- Escapeway ladders,
- Primary ventilation fans controls and concrete works,
- Surface magazine and access.

The Waihi Open pit is establishing offices, changerooms some workshops, ROM, laydowns, WRL and mine haul roads and accesses.

The ORE is based on a feasibility level of accuracy. A gold price of A$3,600/oz was used for financial assessment, and the competent person is satisfied based on the assumptions outlined in this report, the mine indicates positive net cash flow outcomes

Ore Reserve

On the basis of the outcomes of the analysis described above, the estimated economic mining inventory was classified as an Ore Reserve under the 2012 JORC code. All of the Ore Reserve Estimate was derived from the economic portion of the Measured & Indicated Mineral Resource. Measured Mineral Resource within the economic mining envelope was classified at Proved Ore Reserve Estimate. Indicated Mineral Resource within the economic mining envelope was classified at Probable Ore Reserve Estimate. Low grade was all classified as Probable Ore Reserve Estimate. The Ore Reserve is shown in Table 24.

Table 24 - Waihi Underground Ore Reserve, as at 1 April 2026

WAIHI UNDERGROUND GOLD PROJECT ORE RESERVE ESTIMATE:									
	PROVED			PROBABLE			TOTAL MATERIAL		
	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)	('000t)	(g/t Au)	('000oz.)
UNDERGROUND	-	-	-	825	3.8	101	825	3.8	101
Inc Golden Pole	-	-	-	*254*	*5.0*	*41*	*254*	*5.0*	*41*
LOW GRADE[14]	-	-	-	116	1.1	4	116	1.1	4
TOTAL	**-**	**-**	**-**	**941**	**3.5**	**105**	**941**	**3.5**	**105**

ORE RESERVES – OPEN PIT

Overview of Assumptions, Outcomes and Criteria for Classification

The Ore Reserve was estimated from the Mineral Resource estimates prepared in July 2025 and were current at the time. Aside from historical mining there has been no mining of the Waihi Mineral Resource as at the date of this Ore Reserve; hence, no depletion of the Waihi Mineral Resources was required. The Mineral Resource model was a sub-celled Ordinary Kriged model.

The Ore Reserve is reported as at 1 April 2026.

The Ore Reserve was generated from design studies using current costs, geotechnical parameters and dilution and recovery parameters.

Costs were derived from the FY26 budget process and recent tendered contract pricing specific to the Waihi open pit. Unit costs for haulage, processing and site overheads were estimated based on scheduled process plant throughput using material above the economic cut-off grade.

The open pit Ore Reserve was estimated using a cut-off grade derived from a gold price of A$2,400/oz. Low Grade Ore and Stockpiles were incorporated based on a gold price of A$3,400/oz. There are no existing economic surface stockpiles at Waihi.

No Measured economic Mineral Resource occurs within the Waihi mining envelope. All Indicated economic Mineral Resource within the mining envelope was classified as Probable within the Waihi open pit Ore Reserve following the application of modifying factors. No downgrading of the Ore Reserve classification was considered necessary.

14 Insitu material

Dilution parameters were based on mining reconciliations of previous DGP open pit operations. The dilution skin method was used to reflect the selective mining method proposed to be used at DGP.

A weight average process recovery of 90% was used in the estimate. This process recovery was based on metallurgical test work for oxide, transition and fresh mineralisation.

Mining Method

The upper portion of the Waihi deposit will be mined using conventional open pit methods. Ore will be mined using selective mining techniques typically used in the Eastern Goldfields. Load and haul will be carried out by 120 tonne class excavators and 90 tonne dump trucks. This mining approach was successfully used for the load and haul of ore and waste on other Ora Banda open pit projects. Drill and blast will be carried out using conventional diesel hydraulic blasthole drills and blasting practices, typical of the West Australian Goldfields.

Selective mining of the ore will be in the across strike direction. The process will entail separating the blasted waste from the ore at the hanging wall contact, excavating the ore, then separating the ore from the waste at the footwall contract. Ore mining will be continuously supervised by trained ore spotters in direct contact with excavator the operator.

A key nuance of mining the Waihi pit is the excavation and storage of the existing in-pit tailings. The tailings will be mined by conventional load and haul fleet in combination with low ground pressure dozer (swamp dozer). Surface storage will be developed using a sequence of placing tails and waste rock to complete a landform whereby the tailings are fully encapsulated.

Processing Method

Ore is treated at the DGP using conventional carbon-in-leach (CIL) with some gold recovered via gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. The process plant currently has a nominal throughput rate of 1.2 Mtpa based on a grind size of 106 µm.

Test work on Waihi ores was conducted during the feasibility study in 2020. The test work showed the material to be similar in nature to ores already treated through the Davyhurst process plant. Based on the process plant design criteria (106 µm, 24 hr leach) recoveries between oxide, transition and fresh ranged from 94%, 92% and 90% respectively. An average of 57% of the gold was recovered through gravity. The overall recovery was estimated to be approximately 90% due to 93% of the ounces from fresh rock material.

Cut-off Grades

The cut-off grade used to define the economic material within the mining envelope allows for ore haulage, crusher loading, processing, site G&A and corporate overhead contributions. Standard state royalties and third party royalties were included. The cut-off grade for high grade at Waihi is estimated to be 1.2 g/t. The cut-off grade for Low Grade and Surface stockpiles is estimated to be 0.8 g/t.

A gold price of A$2,400 per ounce was used in the high grade cut-off calculation and using A$3,400 for low grade cut-off calculation.

Estimation Methodology, and Modifying Factors

Dilution modelling for the Waihi open pit Ore Reserve was completed using Auto Stope Designer (**ASD**) functionality in Deswik™ software. Mineable "stope" shapes are created to simulate practical dig blocks. Dilution skins were added to both hanging wall and footwall of the mineralisation and internal and edge dilution was included resulting from forming practical mineable shapes.

A minimum ore mining width of 1.5 m was applied in the dilution modelling process. A 0.5 m dilution skin was applied to both hanging wall and footwall at Waihi for all of weathering classifications, resulting in an SMU of 2.5m wide. The average dilution is estimated to be 27% at Waihi. The dilution parameters were based on a subjective assessment of operational performance at previous DGP pits operated by Ora Banda (e.g. Missouri and Riverina).

The ASD optimisation shapes with an average grade below 1.2 g/t and above 0.8 g/t were classified as Low Grade.

Background grades were estimated into the resource block model and were included in the dilution modelling. Dilution grades were estimated to be 0.16 g/t for Waihi.

Ore loss was applied in the ASD process as a result of the variation between mineralised lode geometry and practical dig block geometry. In addition, a nominal 5% ore loss was applied in the mining schedule, to account for further mining losses occurring through normal operations.

Pit Optimisation

Pit optimisations using Whittle or similar software were carried out to inform pit design and was considered still to be a reasonable representation of the economic envelope at the revised input parameters.

Validation of Waihi's economics was based on the ultimate pit achieving the target cash costs described above (A$3,000 per ounce).

Pit Design

The pit design for Waihi was informed by previous pit optimisations and assessment of the local conditions and features, as well as current geotechnical parameters. The pit optimisation and design were validated against updated cost and revenue inputs for this Ore Reserve estimate.

The proposed pit cutback final depth will be approximately 65 m. The batter angles will vary between 50^0 and 85^0 (excluding tailings). Berms will be between 5 m and 7 m in width, with the batter face heights of 15 m to 25 m. The parameters used were based on geotechnical assessment. Detailed tailings geotechnical test work and modelling was done to determine the excavation geometry in the in situ tailings. Based on the study results, the stable overall slope angles of in the in situ tailings were designed to be no more than 9.5°. The pit ramp width will be single lane 15 m wide ramp to accommodate Komatsu HD-785 trucks or similar. Passing bays will be located at switch backs and berms.

The Waihi Central Pit is shown in Figure 22.

Geotechnical test work and modelling was carried out on the relocation and storage of the in situ in-pit tailings. From this analysis, a detailed methodology for constructing stable Waste Rock Landforms (WRL) was developed whereby the majority of mined tailings are stored on top of the existing in-pit tailings and then encapsulated with co-mingled tailings and fresh rock. The proposed WRL has been approved by the regulator (Waihi Mining Proposal Reg ID 120936).

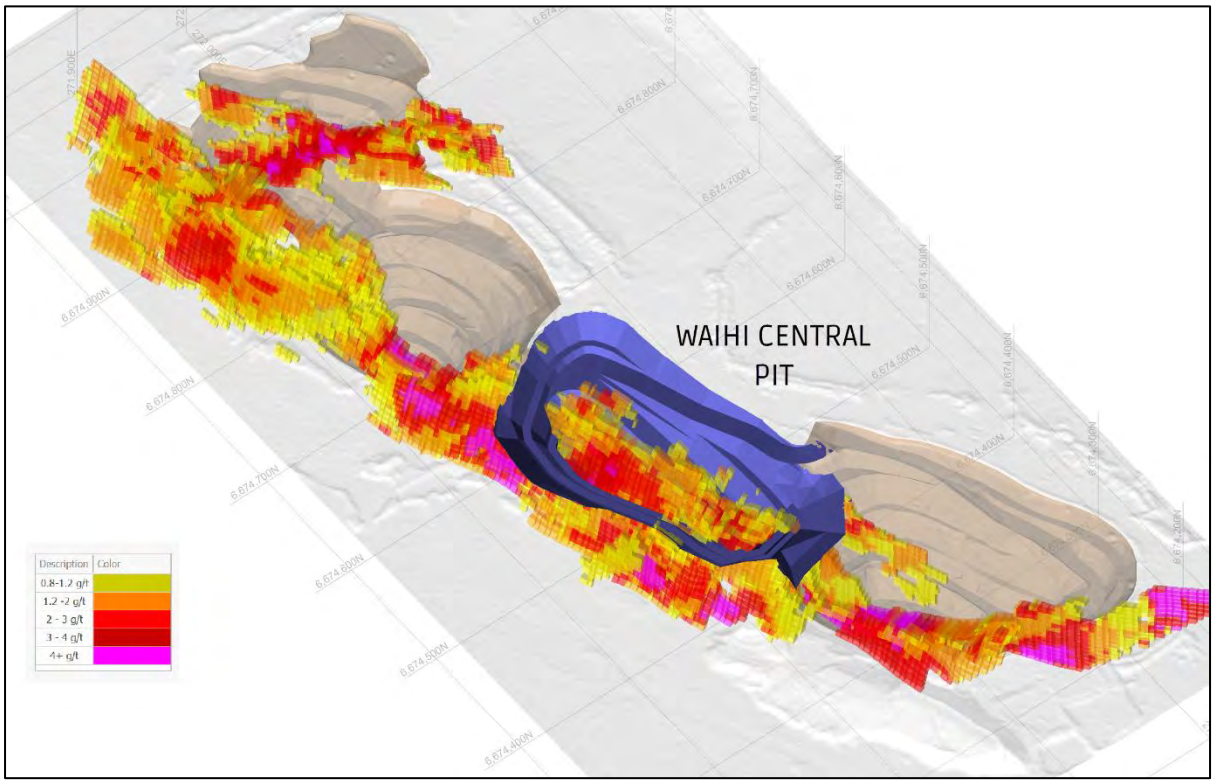

Figure 22 - Waihi open pit designs showing diluted block model >0.8 g/t

Open Pit Mine Schedule

The Waihi historic pits are currently backfilled with tailings from an earlier mining episode. The removal and disposal of tails formed part of the operational considerations and costing. The Central pit tailings are scheduled to be mined and placed on top of the north and south tailings filled pits. The sequencing is alongside the in situ rock ensuring excavators and trucks operate on competent ground with swamp dozers pushing the tailings material. Management of the tailings handling, deposition and sequencing will be an important consideration for the project. The Waihi pit will be mined over a period of approximately eight months.

The mine specific cash flow modelling was based on a gold price of A$3,600/oz. Based on the assumptions outlined in this report, the Waihi Open Pit indicates positive net cash flow outcomes.

STOCKPILES

Stockpile inventories consist of ROM stocks and low-grade stocks mined under ownership of Ora Banda as of 1 April 2026 and above the economic cut-off grade (Table 25). The cut-off grades vary based on location and allows for ore haulage, crusher loading, processing, site G&A and corporate overhead contributions. The costs to treat these stockpiles was estimated to be A$89 per tonne or less, depending on distance from the process plant. Recoveries used were based on metallurgical test results of the source deposit. All stockpiles listed in Table 25 is above a cut-off grade of 0.5 g/t.

Table 25 - Ore Reserve stockpiles

Location	Stockpile ID	Grade Bin	Material Type	Dry Tonnes	Grade	Ounces
Davyhurst	DH-HG	HG	Fresh	1,605	4.60	237
Davyhurst	DH-MG	MG	Fresh	5,114	2.30	378
Davyhurst	DH-LG	LG	Fresh	3,154	1.05	106
Davyhurst	FOS A	MG	Crushed	11,218	2.59	933
Davyhurst	FOS C	LG	Crushed	4,769	1.30	199
Davyhurst	FOS D1	MW	Crushed	2,254	0.68	49
Davyhurst	SC	MW	Crushed	89,713	0.54	1,558
Riverina	RV-HG1	HG	Fresh	13,403	3.98	1,716
Riverina	RV-MG1	MG	Fresh	1,201	2.03	78
Riverina	RV-LG1	LG	Fresh	1,696	1.53	83
Riverina	RV-MW	MW	Fresh	24,731	0.72	573
Riverina	RV-OP1	MW	Oxide	169,268	0.76	4,136
Riverina	RV-OP2	MW	Fresh	56,423	0.76	1,379
Siberia	SK-HG	HG	Fresh	2,458	9.06	367
Siberia	SK-MG	MG	Fresh	707	5.42	65
Siberia	SK-LG	LG	Fresh	1,937	1.24	77
Siberia	SK-MW	MW	Fresh	18,981	0.64	391
Siberia	MS-MW	MW	Fresh	190,974	0.77	4,729
Sub Total			Fresh	322,385	1.0	10,181
Sub Total			Oxide	169,268	0.8	4,136
Sub Total			Crushed	107,954	0.8	2,739
Total				**599,607**	**0.9**	**17,056**

This announcement was authorised for release to the ASX by the Ora Banda Board of Directors. For further information about Ora Banda and its projects please visit the Company's website at www.orabandamining.com.au.

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APPENDIX - JORC CODE, 2012 EDITION –REPORT TEMPLATE

Section 1 Sampling Techniques and Data – Riverina

Information for historical (Pre Ora Banda Mining Limited from 1980's to 2010) drilling and sampling has been extensively viewed and validated where possible. Information pertaining to historical QAQC procedures and data is incomplete but of a sufficient quality and detail to allow drilling and assay data to be used for resource estimations. Further Ora Banda Mining Limited has undertaken extensive infill and confirmation drilling which confirm historical drill results. Sections 1 and 2 describe the work undertaken by Ora Banda Mining Limited and only refer to historical information where appropriate and/or available.

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample retrospectivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (ego 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information*	• Croesus Mining N.L; All samples were dried, crushed and split to obtain a sample less than 3.5kg, and finely pulverised prior to a 50gm charge being collected for analysis by fire assay. • Monarch Gold Mining Company Ltd; Industry standard work. RC samples collected and sent to certified laboratories for crushing, pulverising and assay by fire assay (RC) and aqua regia (RAB). • Pancontinental Mining Ltd; Samples (>2kg) were crushed to 1mm, 1kg split taken and pulverised to 90% minus 20 mesh from which a 50gm aliquot was taken for assay by aqua regia or fire assay. • Consolidated Gold N.L/DPPL (Davyhurst Project PTY LTD); Industry standard work, RAB samples crushed, pulverised and a 50g charge taken for fire assay. 200gm soil samples oven dried, and pulverised, 50g charge taken for aqua regia assay. • Riverina Resources Pty Ltd; Industry standard work. RAB samples taken every metre, composited to 4m using a spear. Samples crushed, pulverised and 50g charge taken for fire assay. RC four metre composite samples were collected using a sample spear. RC and diamond samples crushed, pulverised and 50g charge taken for fire assay and/or 4 acid digest. Any gold anomalous 4m composite samples were re-sampled over 1m intervals using a riffle splitter and also sent to Kalgoorlie Assay Laboratory for gold analysis by 50g fire assay. • Barra Resources Ltd; Industry standard work. The entirety of each hole was sampled. Each RC and RAB hole was initially sampled by 4m composites using a spear or scoop. To obtain a representative sample, the entire 1m sample was split using a riffle splitter into a calico bag. Whole diamond core samples for ore zones were sampled. Entire samples were pulverised before splitting and a 50g charge taken for fire assay. • Greater Pacific Gold; Core sampling method unknown, assumed to be cut half core. RC sampling method unknown. Analysis method unknown. However, work completed by accredited laboratories, Analabs and Genalysis. • Carpentaria Exploration Company Pty Ltd; Samples were collected over 1m intervals. 1m, 2m and 4m composite samples taken depending on the rock type. Composite samples were collected using a sample spear. About 2kg samples were despatched for analysis. Samples crushed, pulverised and a 50g charge taken for fire assay. • Malanti Pty Ltd; Industry standard work. 1m samples were collected via a cyclone and passed through a triple splitter giving a 12.5% split of about 2kg. A trowel was used to scoop the samples for composites over 4m and 6m intervals. Samples for assay were then taken with composite intervals based on geology. Many of the single splits were selected for assay in the first instance. Samples packed in poly weave bags were freighted for analysis. Sample crushed, pulverised and a 50g charge taken for fire assay. • Riverina Gold Mines NL; Industry standard work, Composited RAB and 1m RC samples assayed by laboratory. Samples crushed, pulverised and a 50g charge taken for aqua regia analysis. • Riverina Gold NL; RAB samples were bulked at 2m intervals. RC holes were sampled at 1m intervals. Diamond core samples were taken at geological boundaries, sample method unknown. All samples crushed, pulverised and a charge taken for fire assay (Au) and perchloric acid digest/AAS for other elements.

		• Ora Banda Mining Limited (OBM) - 1m RC samples using face sampling hammer with samples collected under cone splitter. 4m composite RC samples collected using a PVC spear from the sample piles at the drill site. For drilling up to April 2020, RC samples were dispatched for pulverising and 50g charge Fire Assay. For drillholes RVRC20036 to RVRC20104 inclusive, 1m and 4m composite samples were dispatched to the lab, crushed to a nominal 3mm, split to 500 grams and analysed by Photon Assay method at MinAnalytical in Kalgoorlie. 4m composite samples with gold values greater than 0.2 g/t Au were re-sampled as 1m split samples and submitted to the lab for Photon Assay analysis. Half-core samples, cut by automated core saw. Core sample intervals selected by geologist and defined by geological boundaries. Samples are crushed, pulverized and a 40g charge is analysed by Fire Assay. For all drilling since 2022, - 1m RC samples using face sampling hammer with samples collected under cone splitter. 4m composite RC samples were taken outside of mineralised zone, collected using a scoop from the sample piles at the drill site. 1m cone spilt samples were taken within the expected mineralised zones. Core sample intervals selected by geologist and defined by geological boundaries. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay. From 7 March 2025 surface drill samples were analysed by ~400g photon analysis by SGS, Perth, following preparation at the on-site SGS laboratory. Underground diamond drilling - Core sample intervals selected by geologist and defined by geological boundaries. Samples are generally sawn half core but some intervals are whole core. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay. From 10 March 2025 underground samples were analysed by ~400g photon analysis by SGS, Perth after being crushed at the on-site SGS laboratory. Underground face sample (rock chips by hammer) intervals selected by geologist and defined by geological boundaries.
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Croesus Mining N.L; Auger samples were drilled by Prodrill Pty Ltd using Toyota mounted auger rig. RAB holes were drilled by either Kennedy, or Arronika or Challenge Drilling of Kalgoorlie. Challenge drilling employed a custom built RAB/AC rig. RC holes were drilled by Ausdrill Pty Ltd and diamond holes were drilled by Sandersons. Core was oriented. • Monarch Gold Mining Company Ltd; Aircore and RAB holes were drilled by Challenge Drilling. All RC holes were drilled by Kennedy Drilling Contractors with $5^{1/2}$" hammer. • Pancontinental Mining Ltd; Drilling was undertaken by Davies Drilling of Kalgoorlie using a Schramn T64 rig. • Consolidated Gold N.L/DPPL; Auger samples were collected using a power auger fitted to a 4WD vehicle. RAB drilling was undertaken by Bostech Drilling Pty Ltd. • Riverina Resources Pty Ltd; RC holes drilled with $5^{1/4}$" hammer. Unknown diamond core diameter. • Barra Resources Ltd; Holes were drilled by Resource Drilling Pty Ltd using a Schramm 450 drill rig. • Greater Pacific Gold; Schramm RC Rig with face sampling hammer, $5^{1/8}$" diameter. NQ core, Edson Rig • Carpentaria Exploration Company Pty Ltd; RC drilling by Robinson contractors. Face sampling hammer used. • Malanti Pty Ltd; Holes were drilled by Redmond Drilling of Kalgoorlie using a truck mounted Schramm rig with a compressor rated at 900 cfm 350 psi. • Riverina Gold Mines NL; Vacuum holes were drilled by G & B Drilling using a Toyota Landcruiser mounted Edsom vacuum rig fitted with a 2 inch (5.08cm) diameter blade. RAB holes were drilled by PJ and RM Kennedy using a Hydro RAB 50 drill rig mounted on a 4 wheel Hino truck with 600 cfm/200 PSI air capacity. A 51/4 inch hammer and blade were used. RC holes were drilled by either Civil Resources Ltd using an Ingersoll Rand T4W heavy duty percussion rig fitted with a 900 cfm at 350 PSI air compressor and a 51/4 inch (13,34cm diameter) RC hollow hammer or by Swick Drilling using an Ingersoll Rand TH 60 reverse circulation drill rig with 750 cfm/350 PSI air capacity and a 51/4 inch RC hollow hammer or by B. Stockwell of Murray Black's Spec Mining Services using a rig mounted on an 8 x 4 Mercedes. • Riverina Gold NL; RC hole were drilled by Green Drilling using Schramm T66 rig. Diamond holes were drilled by Longyear. Diamond holes were sometimes drilled with a RC pre-collar, HQ core and a NQ2 core drilled. • Ora Banda Mining Limited (OBM) – 5.25 to 5.5 inch diameter RC holes using face sampling hammer with samples collected under cone splitter. HQ and HQ3 coring to approx. 40m, then NQ2 to BOH. Metallurgical and geotechnical core holes drilled using HQ3 exclusively. All core oriented by reflex instrument. All core drilled in 2022 was orientated by Axis instrument. Underground diamond drilling – NQ2 coring with standard tubing (triple tubing for geotechnical), all core is oriented by Axis Champ Ori tool, rig alignment via DeviAligner tool, downhole surveys via DeviGyro-Ox tool.

Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• Auger, RAB and RC drill recoveries were not recoded by Croesus Mining N.L, Monarch Gold Mining Company Ltd, Pancontinental Mining Ltd, Consolidated Gold N.L/DPPL, Riverina Resources Pty Ltd, Barra Resources Ltd, Carpentaria Exploration Company Pty Ltd, Malanti Pty Ltd, Riverina Gold Mines NL or Riverina Gold Mines NL. However Monarch, in a Riverina resource report state that "Good recoveries for RMRC series RC drilling were observed. Minor water was encountered in 27 of the RMRC series drillholes" • Diamond Core recoveries are very high due to the competent ground. Any core recovery issues are noted on core blocks and logged. • Ora Banda Mining Limited (OBM - Diamond drill recoveries are recorded as a percentage calculated from measured core against downhole drilled intervals (core blocks). Underground diamond drilling – Diamond drill recoveries are recorded as a percentage calculated from measured core against metre marks and noted core loss blocks from driller's rod counts. Underground face sampling domains marked up, with chip samples taken along the sample line per domain to reduce sampling bias. • There is no known relationship between sample recovery and grade.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Croesus Mining N.L; RAB drill logs were recorded both on paper and later electronically by a Casiopia datalogger. Diamond core was geologically, geotechnically and magnetic susceptibility logged. Qualitative: alteration, colour, contact, grainsize, joint, matrix, texture, rock type, mineral, structure, sulphide, percent sulphide, vein type, percent vein, weathering. Quantitative; percent sulphide, percent vein. Diamond core was photographed. • Monarch Gold Mining Company Ltd; Qualitative: lithology, mineralisation code, alteration, vein code, sulphide code. Quantitative; percent mineralisation, alteration intensity, percent vein, percent sulphide. • Pancontinental Mining Ltd; All drill data was recorded on computer forms and the lithological descriptions were produced by Control Data' Bordata program. Qualitative: colour, weathering, minerals, grainsize, rock, structure, alteration. Quantitative: alteration intensity. • Consolidated Gold N.L/DPPL; Holes were logged at 1m intervals using a standard logging sheet directly onto a palmtop logger. Qualitative: colour, weathering, minerals, grainsize, rock, structure, alteration. Quantitative: alteration intensity. • Riverina Resources Pty Ltd; Qualitative: lithology, minerals, oxidation, colour, grain, texture, texture intensity, alteration, sulphide, comments. Quantitative: alteration intensity, percent sulphide, percent quartz veins. • Barra Resources Ltd; Each meter from all RC drillholes was washed, sieved and collected in chip trays and stored at the Barminco First Hit Mine office. These rock chips were geologically logged using the Barminco Pty Ltd geological logging codes. This data was manually recorded on logging sheets or captured digitally using a HP Jornada hand held computer utilising the Micromine Field Marshall program and entered into a digital database at the Barminco First Hit Mine office. Each diamond drillholes was recovered according to the driller's core blocks and metre marked. The core was logged to the centimetre, and samples were marked up accordingly. The core was geologically logged using the Barminco Pty Ltd geological logging codes. This data was manually recorded on logging sheets in the field and entered into a digital database at the Barminco First Hit Mine office. Qualitative: qualifier, lithology, mineralisation, alteration, grain size, texture, colour, oxidation. Quantitative; percentage of quartz and sulphide. Core was photographed. • Greater Pacific Gold; Qualitative logging of lithology, oxidation, alteration and veining. • Carpentaria Exploration Company Pty Ltd; Qualitative: description. Quantitative; percent oxidation, percent quartz, percent pyrite. • Malanti Pty Ltd; Qualitative: description. Quantitative; percent quartz. Logged on a metre basis. • Riverina Gold Mines NL; Qualitative for Vacuum holes: colour, grain size, alteration minerals, rock type, structure, vein type, sulphides, oxidation and comments. Quantitative for Vacuum holes; percent veins, percent sulphides. Qualitative for RAB holes and RC holes from RV110 to RV295: colour, grain size, alteration minerals, rock type, fabric, vein type, sulphides, oxidation and comments. Quantitative RAB holes and RC holes from RV110 to RV295; percent veins, percent sulphides. Qualitative for RC holes from RV296 to RV350: geology, oxidation, colour and description. Quantitative for RC holes from RV296 to RV350; percent quartz. • Riverina Gold NL; Qualitative: RQD, lithology, mineralisation, alteration, weathering, veining, fracturing. Quantitative: percent quartz. • Ora Banda Mining Limited (OBM - Field logging was conducted using Geobank Mobile™ software on Panasonic Toughbook CF-31 ruggedized laptop computers. Qualitative logging: Lithology, colour, oxidation, grainsize, texture, structure, hardness, regolith. Quantitative: estimates are made of quartz veining, sulphide and alteration percentages. Core photographed both wet and dry. Magnetic susceptibility and RQD were also recorded for core holes. Underground diamond drilling – Qualitative logging: Lithology, texture, alteration, mineralisation/sulphides, structure, veining. Quantitative: estimates are made of veining, sulphide and

		alteration percentages, RQD measurements, core density measurements, core recovery per metre, fractures per metre. Core photographed both wet and dry. Underground face sampling domain logging of lithology, veining, alteration, mineralisation/sulphides with each face mapped and photographed • All holes were geologically logged in their entirety to a level of detail to support mineral resource estimation.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Croesus Mining N.L; Auger samples were taken from an average depth of 1.5m to 2m. RAB and Aircore samples were collected in buckets below a free standing cyclone and laid out at 1m intervals in rows of tens adjacent to the drill collar. Composite analytical samples (~3.5kg) were initially collected over 5m intervals for each hole and a 1m bottom of hole analytical sample. Analytical composite samples were formed by taking a representative scoop through each 1m drill sample. RC drill samples were collected in large plastic retention bags below a freestanding cyclone at 1m intervals, with analytical samples initially formed by composite sampling over 5m intervals. Where samples were dry, analytical composites were formed by spear sampling, using a 50mm diameter plastic pipe pushed through the drill cuttings in the sample retention bag to the base of the bag. The pipe is removed carefully with the contents of the pipe containing a representation of the retained metre. Wet RC drill samples where thoroughly mixed in the sample retention bag and 'scoop' sampled to form a 5m composite sample. HQ diamond core was cut into halves and sampled on geological boundaries, to a minimum of 20cm samples or on a metre basis on site. The diamond core was cut using a diamond saw, with half core being submitted to the laboratory for analysis and the other stored. Field samples were taken for RAB, RC and diamond core samples at a rate of 1 in 20. Composite analytical samples returning values greater than 0.1 g/t Au were re-sampled at 1m intervals. • Monarch Gold Mining Company Ltd; Drillhole samples were collected at 4m and 3m composite intervals. All samples at ALS Kalgoorlie were sorted, dried, split via a riffle splitter using the standard splitting procedure laboratory Method Code SPL-21, pulverised in a ring mill using a standard low chrome steel ring set to >85% passing 75 micron. If sample was >3 kg it was split prior to pulverising and the remainder retained or discarded. A 250g representative split sample was taken, the remaining residue sample stored and a 50gm sample charge was taken for analysis. All samples at Ultra Trace Pty Ltd were sorted, dried, a 2.5 – 3kg sample was pulverized using a vibrating disc, was split into a 200-300g subsample and the residue sample stored. A 40grm charge was taken for analysis. Composite samples returning anomalous values were sampled at 1m intervals using a scoop. For both RC and RAB drilling a duplicate sample was collected at every 25th sample, and a standard sample was submitted every 20th sample. • Pancontinental Mining Ltd; RC samples were collected in plastic bags directly from the cyclone at 1m intervals, split twice through a sample splitter before splitting off a 2kg sample for analysis. Samples were crushed to 1mm, 1kg split taken and pulverised to 90% minus 20 mesh from which a 50gm aliquot was taken. Field samples were taken at a rate of 1 in 10 and results show a good correlation with the original values. Samples sent to SGS were dried, jaw and roll crushed, split and pulverised in a chromium steel mill. • Consolidated Gold N.L/DPPL; Auger samples were collected at a nominal depth of 1.5m or blade refusal. Approximately 200gm of material was placed into pre-numbered paper geochemical bags. Sample numbers were entered into a datalogger linked to the GPS unit to ensure accuracy. RAB samples were collected a 1m intervals and used to create a 4m composite sample. Samples were oven dried, pulverised in a single stage grinding bowl until about 90% of the material passed 75 micron. A 50gm split sample was taken for analysis. Composite samples returning values greater than 0.19 Au g/t were sampled at 1m intervals. • Riverina Resources Pty Ltd; Auger soil samples were collected from a depth of 1.8m or blade refusal. RAB and RC 4m composites were taken using a sample spear. Samples were dried, crushed, split, pulverised and a 50gm charge taken. Composite samples returning anomalous gold values were sampled at 1m intervals using a sample spear. • Barra Resources Ltd; Every metre of the drilling was collected through a cyclone into a large green plastic bag and lined up in rows near the hole in rows of 20. The entirety of each hole was sampled. Each hole was initially sampled by 4m composites using a spear or scoop. Once each hole was logged, intervals considered to be geologically significant were re-sampled at 1m intervals. To obtain a representative sample, the entire 1m sample was split using a riffle splitter into a calico bag. Whole diamond core samples for ore zones were sampled. Samples greater than 2.5kg were riffle split to <2.5kg using a Jones riffle splitter. The entire sample was then pulverised in a Labtechnics LM5 to better than 85% passing 75 microns. A 50gm pulp was taken for assaying in appropriately numbered satchels. Composite samples that returned gold assays greater than 0.1 g/t Au and that had not been previously sampled at 1m intervals, were re-sampled at 1m intervals. In addition, any highly anomalous 1m samples were also sampled again to confirm their assay results. • Greater Pacific Gold; Sample preparation for RC and core sample unknown.

		• Carpentaria Exploration Company Pty Ltd; Samples were collected over 1m intervals. 2m and 4m composite samples were collected using a sample spear. About 2kg samples were despatched for analysis. Samples were dried, crushed, split, pulverised and a charge taken for analysis. • Malanti Pty Ltd; 1m samples were collected in plastic bags via a cyclone and passed through a triple splitter giving a 12.5% split of about 2kg which was placed in a calico bag and marked with the drillhole number and interval sampled. The 87.5% was returned to the similarly numbered large plastic bag and laid in rows on site. A trowel was used to scoop the samples for composites over 4m and 6m intervals. Samples for assay were then taken with composite intervals based on geology. Many of the single splits were selected for assay in the first instance. Samples packed in poly weave bags were freighted for analysis. Samples were dried, crushed, split, pulverised and a 50gm charge taken. RC Samples with anomalous composite assays were split and submitted for analysis. • Riverina Gold Mines NL; Vacuum hole samples were collected every metre and split. RAB samples were taken every metre through a cyclone and riffle split to a quarter and composited to 4m intervals. RC samples were taken every metre through a cyclone after being riffle split to a quarter and some composited to 4m. The residue remained on site in plastic bags whilst the quarter split was sent for analysis. For vacuum holes RVV70 to RVV125, a 30grm was taken. RC samples from holes RV110 to RV164 and vacuum hole samples were dried, crushed to nominal 3mm and a 1,000 gram split was taken for pulverising until 90% passed minus 75 microns. A 25grm charge was taken. RC samples from holes RV230 to RV350 were totally pulverised and a 50 grm charge taken. 4m RAB composite samples returning anomalous values greater than 0.1 g/t Au were sampled at 1m intervals. • Riverina Gold NL; RAB samples were bulked at 2m intervals. RC holes were sampled at 1m intervals. Diamond core samples were taken at geological boundaries. Samples were crushed, split, pulverised and a charge taken for analysis. • Ora Banda Mining Limited (OBM) – RC samples were submitted either as individual 1m samples taken onsite from cone splitter or as 4m composite samples speared from the onsite drill sample piles. Half core samples, cut by saw. Core sample intervals selected by geologist and defined by geological boundaries. For drilling up to April 2020, RC samples were dried, crushed, split, pulverised and a 50gm charge taken. For drillholes RVRC20036 to RVRC20104 inclusive, 1m and 4m composite samples were dispatched to the lab, crushed to a nominal 3mm, split to 500 grams and analysed by Photon Assay method at MinAnalytical in Kalgoorlie. 4m composite samples with gold values greater than 0.2 g/t Au were re-sampled as 1m split samples and submitted to the lab for Photon Assay analysis. For all drilling from 2022, RC samples were submitted either as individual samples taken from the onsite cone splitter or as four metres composite samples taken by metal scoop. Core sample intervals selected by geologist and defined by geological boundaries, cut by saw and submitted as half core. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10). From 10 March 2025 samples were analysed by ~400g photon analysis by SGS. Field duplicates, blanks and standards were submitted for QAQC analysis. Underground diamond drilling – Core sample intervals selected by geologist and defined by geological boundaries, selected holes cut by saw and submitted as half core and remainder of holes are whole-core sampled. Initially all UG samples were dispatched to the SGS laboratory at the Davyhurst site for crushing and pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10). From early March 2025 all underground grade control and face sampling was crushed in the SGS on-site laboratory and the samples sent to SGS Kalgoorlie for gold analysis by Photon assay method. Flushes, blanks and standards were submitted for QAQC analysis. Underground face samples as per diamond drilling, including field duplicates, rock chip samples taken via hammer sampling per geology domain. • Repeat assays were undertaken on pulp samples at the discretion of the laboratory.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*	• Croesus Mining N.L; Auger samples were sent to Ultratrace Laboratories, Perth, to be assayed for gold using the Aqua Regia method with a detection limit of 1ppb. RAB, aircore, RC and diamond samples were sent to Ultratrace Laboratories in Perth to be analysed for gold using Fire assay/ICP Optical Spectrometry. Diamond core check samples were analysed at Genalysis of Perth. Some diamond core samples were also analysed for platinum and palladium by fire assay. • Monarch Gold Mining Company Ltd; RC samples were sent to ALS Kalgoorlie to be analysed gold by fire assay (lab code Au-AA26). This was completed using a 50grm sample charge that was fused with a lead concentrate using the laboratory digestion method FA-Fusion and digested and analysed by Atomic Absorption Spectroscopy against matrix matched standard. RC samples were also sent to Ultra Trace Pty Ltd, Canning Vale Western Australia for gold analysis by lead collection fire assay. Samples were also analysed for palladium and platinum. The Quality control at ALS involved 84 pot fire assay system. The number and position of quality control blanks, laboratory standards and repeats were determined by the batch size. Three repeat samples were generally at position 10,

	• *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	30, 50 of a batch and the control blanks (one blank) at the start of a batch of 84 samples. The laboratory standards were inserted randomly and usually two certified internal standards were analysed with a batch, but it was at the discretion of the 'run builder' as to how many standards to add to the batch and where to place them in the run. QAQC at Ultra Trace Pty Ltd was undertaken for every 27th sample. At random, two repeat samples were chosen, one laboratory standard was inserted and one check sample was taken. The check sample was chosen if the first pass of fire assay shows anomalous value. • Pancontinental Mining Ltd; Samples were sent to Genalysis Laboratory Services Pty Ltd in Perth to be analysed for gold with a detection limit of 0.01 ppm. They were also analysed for gold at SGS laboratory using aqua regia with AAS finish. A number of samples with an assay greater than 0.2 ppm were re-assayed by fire assay. Laboratory standards indicated reasonable accuracy. • Consolidated Gold N.L/DPPL; Auger samples were submitted to ALS Pty Ltd in Perth to be analysed for gold to a detection limit of 0.001ppm using ALS's PM2005 graphite furnace/AAS technique. Samples were also analysed for calcium, magnesium and arsenic using ALS's IC205 technique. RAB samples were submitted to Minlab Pty Ltd Kalgoorlie to be analysed for gold by fire. Some samples were also sent to Amdel Laboratories Ltd Kalgoorlie for gold analysis by fire assay method FAI. • Riverina Resources Pty Ltd; Auger soil samples were sent to Ultra Trace in Perth to be analysed for gold and arsenic using an aqua regia digest and determination by ICP-MS. RC samples were submitted to Kalgoorlie Assay Laboratory for gold analysis by 50gm fire assay. Samples from holes GNRC012 to GNRC020 were also sent Kalgoorlie Assay Laboratory for gold and nickel analysis using a four-acid digest and gold analysis by 50g fire assay. Martin Zone samples were to Kalgoorlie Assay Laboratories to be assayed Ni, Co, Cr, Cu, Mg, Mn, Fe, S, As, Al, Ca, and Zn using a four acid digest with ICP-OES finish and for Au using a 50gm fire assay digest with flame AAS finish. Some samples were also sent to Ultra Trace in Perth for analysis. 312 end of hole RAB samples from the Forehand Prospect were sent to AusSpec International in Sydney for HyChips spectral analysis developed by AusSpec International and CSIRO capable of analysing dry samples stored in chip trays at a rate of at least 1,600 per day. This was undertaken to identify alteration minerals, weathered clays, Fe oxides, and weathering intensity as well as sample mineralogy including mineral crystallinity and mineral composition. (Results are in appendix 4 of Riverina Project Combined ATR 2006.pdf). Down Hole Electro-Magnetic (DHEM) surveys were conducted in RC drillholes GNRC001, GNRC003 and GNRC004 and three diamond drillholes. These surveys were completed by Outer Rim Exploration Services using a Crone Pulse EM probe. (Southern Geoscience Consultants were contracted to plan the DHEM surveys and interpret the results). • Barra Resources Ltd; Auger samples were sent to Ultra Trace Analytical Laboratories in Perth to be analysed for gold and arsenic. Gold was determined by Aqua Regia with ICP-Mass Spectrometry to a detection limit of 0.2ppb. All RC pulp samples were sent to Kalgoorlie Assay Laboratories or Australian Laboratory Services Pty Ltd (ALS) in Kalgoorlie for gold analysis. Gold analysis was completed using the 50gm fire assay technique with an AAS finish to a detection limit of 0.01ppm. Each was weighed and data captured, with the charge then intimately mixed with flux. Mixed sample and flux were fused in a ceramic crucible at 1100^{o} C in a reducing furnace. Molten mass was then poured into moulds and allowed to cool. Lead button removed and placed in a cupellation furnace. The resultant dore bead was parted and digested, being made up to volume with distilled water. The analyte solution was aspirated against known calibrating standards using AAS. All diamond core sample pulps were sent to Leonora Laverton Assay Laboratory Pty Ltd to be assayed for gold by fire with an AAS finish to a detection limit of 0.01ppm Au. Some drillhole samples were analysed for gold (Fire assay/ICP Optical Spectrometry) by Ultratrace Laboratories in Perth. • Greater Pacific Gold; 1m RC samples submitted to Analabs for Au, Ag, Cu, Pb, Zn, As and Ni analysis. Core samples submitted to Genalysis for Au, Ag, Cu, Pb, Zn, As and Ni analysis. Ore zone samples submitted to Minlab for re-assay. Screen fire assay performed on ore zone pulps. • Carpentaria Exploration Company Pty Ltd; Samples were sent to Australian Assay Laboratories Group in Leonora to be analysed for gold with a detection limit of 0.01 g/t Au by fire assay. Repeat assays undertaken for about 1 sample in 20. Field duplicates and standards routinely submitted with assay batches. • Malanti Pty Ltd; RC samples from RRC1 to RRC7 holes were sent to Aminya Laboratories Pty Ltd, Ballarat, Victoria, to be analysed for gold by fire assay with a detection limit of 0.01 g/t Au. RC samples from holes RRC8 to RRC12 submitted to Minesite Reference Laboratories, Wangara, Western Australia to be analysed for gold by Fire Assay of 50g charge (code FA50) with a 0.01ppm lower detection limit. About 1 in 20 assays was either a repeat or duplicate. • Riverina Gold Mines NL; RC samples from holes RV110 to RV164 and vacuum hole samples were sent to Leonora Laverton Assay Laboratory Pty Ltd, Leonora, to be analysed for gold. The charge was dissolved in aqua-regia/solvent digest with a double ketone backwash and then assayed using AAS techniques with a detection limit of 0.02ppm. RC samples from holes RV230 to RV350, vacuum samples from holes RVV126 to RVV204 and RAB composite samples were sent to Multilab Pty Ltd in Kalgoorlie to be analysed for gold.

		The 50grm samples were digested in aqua regia and assayed by AAS techniques with a detection limit of 0.01ppm. Other RC samples were sent to Minlab in Perth to be analysed for gold using the aqua regia digest and AAS finish. For vacuum and RAB samples, about 1 in 10 assays was a repeat. For RC holes from RV110 to RV164 and vacuum holes, at least 10 percent of a bulk order was repeated as a laboratory duplicate for quality control. • Riverina Gold NL; RAB samples were analysed for gold, silver, arsenic, lead, zinc, copper and nickel. RC samples were despatched to Genalysis to be analysed for gold by Aqua Regia/ AAS method. Diamond samples were set to Analabs in Kalgoorlie to be analysed for gold by fire with fusion AAA, copper, lead and silver by ASS with perchloric acid digestion and, arsenic by ASS with vapour generation and density using an air pycnometer. • Ora Banda Mining Limited (OBM) – Up to April 2020, all samples were sent to an accredited laboratory (Nagrom Laboratories in Perth, Intertek-Genalysis in Kalgoorlie or SGS in Kalgoorlie). The samples have been analysed by firing a 50gm portion of the sample. This is the classical fire assay process and will give total separation of gold. An ICPOES finish is used. Commercially prepared standard samples and blanks are inserted in the sample stream at a rate of 1:12. Sizing results (percentage of pulverised sample passing a 75$_{\mu}$m mesh) are undertaken on approximately 1 in 40 samples. The accuracy (standards) and precision (repeats) of assaying are acceptable. For drillholes RVRC20036 to RVRC20104, 1m and 4m composite RC samples were sent to MinAnalytical Laboratory Services in Kalgoorlie. Sample prep involves drying and a -3mm crush, of which 500 grams is linear split into assay jars for analysis. Samples are analysed by the PhotonAssay method which utilises gamma radiation to excite the nucleus of the target atoms (gold). The excited nucleus then emits a characteristic photon, which is counted to determine the abundance of gold in the sample. For all drilling in 2022, All samples were sent to the accredited onsite SGS laboratory at Davyhurst for sample preparation. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) with MP-AES finish. Commercially prepared standard samples and blanks are inserted in the sample stream at an average rate of 1:25. Sizing results (percentage of pulverised sample passing a 75$_{\mu}$m mesh) are undertaken on approximately 1 in 20 samples. The accuracy (standards) and precision (repeats) of assaying are acceptable. Standards and blanks were inserted into the sample stream at a rate of approximately 1:12. Duplicates were submitted at a rate of approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are acceptable. Underground diamond drilling – All samples pre-April 2025 were sent to the accredited onsite SGS laboratory at Davyhurst for sample preparation. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) with MP-AES finish or ~400g Photon analysis. Commercially prepared standard samples and blanks are inserted in the sample stream at an average rate of 1:20. Sizing results (percentage of pulverised sample passing a 75$_{\mu}$m mesh) are undertaken on approximately 1 in 20 samples. The accuracy (standards) and precision (repeats) of assaying are acceptable. The accuracy (standards) and precision (repeats) of assaying are acceptable. Face samples assayed as per diamond core, including a field duplicate per face. From April 2025 all face sample, and UG diamond samples were assayed by PhotonAssay analysis. From March 2024 surface RC and diamond samples were analysed by PhotonAssay. Samples are crushed at the SGS onsite laboratory using dedicated Orbis crushers and analysed at SGS Kalgoorlie. • Fire assay is considered a total technique, Aqua Regia is considered partial. The PhotonAssay method is considered a total technique and is non-destructive.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• Holes are not deliberately twinned. • Monarch Gold Mining Company Ltd; Geological and sample data was logged digitally and .csv or .xls files imported into Datashed SQL database with in-built validation. Samples bags were put into numbered plastic bags and then cable tied. Samples collected daily from site by laboratory. • OBM - Geological and sample data logged directly into field computer at the drill rig or core yard using Field Marshall or Geobank Mobile. Data is transferred to Perth via email or through a shared server and imported into Geobank SQL database by the database administrator (DBA). Assay files are received in .csv format and loaded directly into the database by the DBA. Hardcopy and/or digital copies of data are kept for reference if necessary. • Data entry, verification and storage protocols for remaining operators is unknown. • No adjustments have been made to assay data.
Location of data points	• *Accuracy and quality of surveys used to locate drillholes (collar and down-hole surveys),*	• Croesus Mining N.L; All drilling was located using a Trimble/Omnistar DGPS with an accuracy of plus or minus 1m. Down hole surveys were either as planned or taken using electronic multi shot camera. The gird system used is AGD 1984 AMG Zone 51.

	trenches, mine workings and other locations used in Mineral Resource estimation. • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• Monarch Gold Mining Company Ltd; The collar co-ordinates of aircore and RAB holes and RC holes RMRC001 to RMRC085 were surveyed using GPS. The co-ordinates of holes RMRC086 to RMRC177 were surveyed using the RTKGPS. All surveying was undertaken by staff of Monarch Gold Mining Company Ltd. Down hole surveys were undertaken every 5m by Ausmine using electronic multi-shot (EMS). The gird system used is GDA94 MGA Zone 51. • Pancontinental Mining Ltd; RC drilling at Mulwarrie was surveyed by McGay Surveys. The grid system used is AMG Zone 51. RAB drilling at Riverina South – holes drilled on local Riverina grid and transformed to MGA using 2 point transformation. Holes were not routinely downhole surveyed. • Consolidated Gold N.L/DPPL; Auger holes located on AMG grid. Some RAB holes were drilled on an AMG grid installed by Kingston Surveys Pty Ltd of Kalgoorlie. Each 40m grid peg had an accurate (plus or minus 10 cm) northing, easting and elevation position. Other RAB holes drilled on local grid. Holes located using compass and hip chain from surveyed baselines. The grid system used is AMG Zone 51. RAB holes not down hole surveyed. • Riverina Resources Pty Ltd; Collar co-ordinates were surveyed using a DGPS. Collar azimuth and inclination were recorded. Downhole surveys for most GNRC holes were by single shot and on rare occasions by gyro. Diamond holes surveyed by electronic multishot. The gird system used is AGD 1984 AMG Zone 51. • Barra Resources Ltd; Collar co-ordinates for northings, eastings and elevation have been recorded. Collar azimuth and inclination were recorded. Drillhole collar data was collected by the First Hit mine surveyor and down hole data was collected by the drilling company and passed onto the supervising geologist. The gird system used is AGD84 Zone 51. • Greater Pacific Gold; Collars surveyed on Riverina local Mine grid. 2 point grid transformation translates coordinates into MGA91 zone 51. Holes downhole surveyed by gyro (Ace Drilling). • Carpentaria Exploration Company Pty Ltd; A local Riverina South grid was employed to record collar coordinates. Holes were not downhole surveyed. Local co-ordinates were transferred to the AMG and MGA grids using a 2-point transformation. • Malanti Pty Ltd; Collar locations of re-sampled RAB holes were noted using a GPS. Holes were not downhole surveyed. Two grid systems were employed; a local Riverina grid and AGD 1996 AMG Zone 51. Local co-ordinates were transferred to the AMG and MGA grids using a 2-point transformation. • Riverina Gold Mines NL; Collar co-ordinates for northings and eastings and have been recorded. Collar inclination was recorded. The grid used was the Riverina grid which is oriented to true north. The origin for this grid is 10,000N, 10,000E located at the south west corner of surveyed M30/98. • Riverina Gold NL; For diamond holes, down hole surveys were either assumed or taken using an Eastman camera or gyro. Diamond hole locations surveyed on Riverina local grid. RC and RAB holes located on surveyed Riverina local grid. • Topography has been surveyed by recent operators. Collar elevations are consistent with surrounding holes and the natural surface elevation. • Ora Banda Mining Limited (OBM) (RC, DD) MGA94, zone 51. Drillhole collar positions were picked up by a contract surveyor using RTKGPS subsequent to drilling. Drill-hole, downhole surveys are recorded every 30m using a reflex digital downhole camera. Some RC holes not surveyed if holes short and/or drilling an early stage exploration project. Diamond drillholes completed in 2019 and 2020 by OBM were surveyed using a Gyro tool. For all drilling in 2022 Drillhole collar positions were picked up by an OBM mining surveyor using RTKGPS subsequent to drilling. All downhole surveys were taken every 10m by Gyro. Underground diamond drilling – diamond drilling collar locations picked up by mine surveyors via theodolite and known survey control points. UG diamond drill rig alignment via surveyed collar locations and DeviAligner tool, downhole surveys via DeviGyro-Ox tool. Underground face sample locations measured via laser distometer to known surveyed control points and development surveys via theodolite. The underground mine is established on a local (mine grid) with no rotation and false (+2000m) RL. The grid and transformation parameters to MGA94, zone 51 were established by OBM surveyors. All development, drill collars and face sampling are surveyed in mine grid.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the*	• Exploration results are reported for single holes only. • Drillhole spacing is adequate for the current resources reported externally. (Examples are discussed below) • Croesus Mining N.L; Auger samples were collected to infill a 250m x 100m grid, Riverina South RAB samples were collected to infill a 400m x 80m grid and Sunraysia RC drilling was completed on a 40m x 200m grid.

	Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. • *Whether sample compositing has been applied.*	• Monarch Gold Mining Company Ltd; RAB holes were drilled on 200m x 40m grids and RC holes were drilled on a 20m x 20m and 40m x 20m grids. • Riverina Resources Pty Ltd; Auger soil sampling program was taken over 50m x 50m, 50m x 100m and 50m x 200m spaced grids, Silver Tongue RAB and RC holes were drilled on 25m x 25m, 25m x 50m and 50mx 50m spaced grids and Corporate James RAB holes were drilled on 50m x 100m and 25m x 100m spaced grids. • Barra Resources Ltd; Auger soil sampling program was taken over 50m x 50m, 50m x 100m and 50m x 200m spaced grids, Silver Tongue RAB and RC holes were drilled on 25m x 25m, 25m x 50m and 50m x 50m spaced grids, Corporate James RAB holes were drilled on 50m x 100m and 25m x 100m spaced grids, Forehand RAB and RC holes were drilled on 50m x 100m, 50m x 50m or 25m x 50m spaced grids and Cactus RC holes were drilled on 10m x 10m, 20m x 20m and 40m x50m spaced grids. • Ora Banda Mining Limited (OBM) – underground diamond drilling – initial spacing for grade control purposes was 20m x 20m, since reduced to 20m x 10m to assist with grade delineation. Underground face samples are taken each 3m/4m ore development cut. • Drill intercepts are length weighted, 1.0g/t lower cut-off, not top-cut, maximum 2m internal dilution.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Drilling was oriented at 90º to the strike of mineralisation and inclined at 60º. Examples are discussed below. • Croesus Mining N.L; Holes were either vertical or inclined at 60º and oriented towards the west. • Monarch Gold Mining Company Ltd; Holes were inclined at 60o and oriented towards the west. • Consolidated Gold N.L/DPPL; Holes were inclined at 60º and oriented towards either the west or east. • Riverina Resources Pty Ltd; Holes were inclined at 60º and oriented towards either the west or east. • Barra Resources Ltd; Holes were either vertical or inclined at 60º and oriented towards the west. • Greater Pacific Gold; Holes drilled to the east inclined at -58 to -60. Suitable for sub vertical N-S striking mineralisation. • Carpentaria Exploration Company Pty Ltd; Holes were inclined at 60º and oriented towards either the west or east. • Malanti Pty Ltd; Holes were inclined at 60º and oriented towards either the west or east. • Riverina Gold Mines NL; Vacuum holes from RVV1 to RVV69 and from RVV126 to RVV204 were drilled vertically. Vacuum holes from RVV70 to RVV125 were inclined at 60º and oriented either east or west. RAB and RC holes were inclined at 60º and oriented either east or west. • Riverina Gold NL; RC holes were inclined at 60º and oriented either east or west. • Ora Banda Mining Limited (OBM) – RC drilling is predominately inclined at between -50 and -60 degrees towards the west. Drilling inclined to the east is only done when lodes are deemed to be vertical or if local landforms prevent access. Underground diamond drilling – collared from decline cuddies in sub-horizontal and inclined fans cutting across sub-vertical lodes, holes are designed to optimise intersection angles and reduce bias for Main Lode East and West. Some bias is present for the Murchison lodes, given their close proximity to the drill cuddies and this impact is mitigated through detailed wall/backs mapping of Murchison lode intersections in underground workings and future targeted grade control drilling.
Sample security	• *The measures taken to ensure sample security.*	• Unknown for all drilling except for the following; • Barra Resources Ltd. Samples received at the laboratory were logged in ALS Chemex's unique sample tracking system. A barcode was attached to the original sample bag. The label was then scanned and the weight of sample recorded together with information such as date, time, equipment used and operator name. • Monarch; Sample calicos were put into numbered plastic bags and cable tied. Any samples that going to SGS were collected daily by the lab. Samples sent to ALS were placed into sample crates and sent via courier on a weekly basis. • OBM - Samples were bagged, tied and stored in a secure yard on site. Once submitted to the laboratories they are stored in cages within a secure fenced compound. Samples are tracked through the laboratory via their LIMS.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• OBM has reviewed historic digital data and compared it to hardcopy and digital (Wamex) records, noting that no issues were found. • OBM sampling procedures are currently being reviewed by external consultants.

Section 1 Sampling Techniques and Data – Sand King

Information for historical (Pre Ora Banda Mining Limited from 1980's to 2010) drilling and sampling has been extensively viewed and validated where possible. Information pertaining to historical QAQC procedures and data is incomplete but of a sufficient quality and detail to allow drilling and assay data to be used for resource estimations. Further Ora Banda Mining Limited has undertaken extensive infill and confirmation drilling which confirm historical drill results. Sections 1 and 2 describe the work undertaken by Ora Banda Mining Limited and only refer to historical information where appropriate and/or available.

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.*	• Goldfields Group; Auger holes were drilled to a maximum depth of 1.5m. RC samples were routinely collected at 1m intervals. Diamond drill core samples were taken at geological boundaries and sawn in half. Samples pulverised at laboratory. • Monarch Gold Mining Company Ltd; RAB samples were collected at 2m and 4m composites via a scoop method at 1m intervals. RC samples were collected at 1m, 2m to 5m intervals. 1m samples were riffle split. • WMC; In early drilling by WMC, samples were "panned' for visible gold. Percussion samples were collected at 1m intervals, split in the field. Diamond core samples were cut in half or quartered. • Gilt Edged Mining NL; All RAB and RC holes were collected through a cyclone and sampled at 1m intervals, pipe or spear sampled, composited over 5m intervals. The composite samples weighing about 3kg were despatched for analysis. 5m composites with assays greater than 0.2 g/t Au were resampled by riffle-splitting the whole of each 1m sample down to about 3kg prior to being despatched for analysis. • Siberia Mining Corporation Ltd; RAB samples were collected at 1m intervals from the drillhole collar using a plastic bucket and laid on the ground. A scoop sample was taken from each sample to form a 5m composite. RC samples were collected at 1m intervals and passed through a cyclone and split using a two tiered, 75:25 riffle splitter. The split sample (approximately 2-3kg) was stored in a drawn calico bag, which was then placed next to the split sample reject (approximately 10-15kg), which was contained in UV resistant PVC bags. A representative scoop sample was then taken from each split sample reject bags to form a 4m composite sample. Diamond half core sampled at 1m intervals. • Ora Banda Mining; RC samples were routinely collected at 1m intervals and cone split. RC samples are collected at 1m intervals in calico bags directly from a cone splitter. Sample size of at least 2kg is targeted. Surface diamond drilling core sample intervals selected by geologist, defined by geological boundaries and half core sampled. Underground diamond core is whole core sampled. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay. Underground face sample (rock chips by hammer) intervals selected by geologist and defined by geological boundaries. From March 2025 samples were analysed by ~400g photon analysis by SGS.
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Goldfields Group; Auger holes were using an auger rig on the back of a Toyota Landcruiser from Snap Drilling. RC holes were drilled by Western Diamond Drillers using a Schramm Rig. Diamond holes were drilled by Mundy Drilling services using a KL1200 rig. Diamond holes were oriented. • Monarch Gold Mining Company Ltd; RC holes were drilled by Kennedy Drilling using a 4 inch blade. • WMC; RC percussion holes were drilled using a Schram Rig. RC holes were drilled using blades and hammer. The RC drilling diameter is unknown. Diamond drillholes for NQ core were drilled and reduced to BQ core at depth if necessary. Some diamond holes commenced with a percussion pre-collar. Diamond core generally not oriented. • Gilt Edged Mining NL; RC holes were drilled by either Sing Drilling or McKay Drilling. Both Kalgoorlie companies used a booster and auxiliary compressor. The RC drilling diameter is unknown. • Siberia Mining Corporation Ltd; RAB holes were drilled by ProDrill Pty Ltd of Kalgoorlie using an open hole RAB drill rig. All holes were drilled dry. RC holes were drilled by Premium Drilling Pty Ltd of Kalgoorlie using a 350/750 Schram RC drill rig and a 5.25" face sampling hammer. An auxiliary booster was used on holes deeper than 75m. • EGL; RC drilling using 5.25 inch face sampling hammer. PQ, HQ and NQ diamond core. PQ drilled from surface until fresh rock encountered, then changed to NQ for geotechnical holes. Resource holes drilled HQ from surface to fresh rock, then changed to NQ. • Ora Banda Mining Limited – 5.5 – 5.625 inch diameter RC holes using face sampling hammer with samples collected under cone splitter.

Criteria	JORC Code explanation	Commentary
		Core holes have RC pre-collars, then NQ_2, HQ_3 or PQ_3 coring to BOH. All core oriented by Axis instrument. RC grade control rig is 5.5 inch diameter hammer with samples collected from a rig mounted cone splitter into calico bags which are submitted for assay. GC Drilling was carried out by Australian Surface Drill Contractors, Rock on Ground, Orlando Drilling and JDC Drilling. Underground diamond drilling – NQ2 coring with standard tubing (triple tubing for geotechnical), all core is oriented by Axis Champ Ori tool, rig alignment via DeviAligner tool, downhole surveys via DeviGyro-Ox tool.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• Quantitative auger, RAB and RC drill recoveries were not recoded by Goldfields Group, Monarch Gold Mining Company Ltd, WMC, Gilt Edged Mining NL, Siberia Mining Corporation, Maitland Mining NL, Newcrest Mining Ltd, Julia Mines NL, Placer Dome Asia Pacific Ltd, Goongarrie Gold Pty Ltd, Australian Consolidated Equities Ltd, Centaur Mining and Exploration Ltd, EGL, Britannia Gold NL, Glengarry Resources NL, Sundowner Minerals NL and Gutnick Resources NL. • EGL - Diamond drill recoveries are recorded as a percentage calculated from measured core against downhole drilled intervals (core blocks). RC sample recoveries not recorded. • Ora Banda Mining Limited – RC drilling recoveries, including Grade control RC were recorded on a pre metre basis based on sample size. Diamond Core recoveries are very high due to the competent ground. Any core recovery issues are noted on core blocks and logged. Diamond drill recoveries are recorded as a percentage calculated from measured core against downhole drilled intervals (core blocks). • There is no known relationship between sample recovery and grade.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Goldfields Group; Qualitative: colour, oxidation, hardness, shearing, texture, grain size, rock, alteration, minerals and Quantitative: alteration intensity, mineralisation intensity, structure intensity, vein percent. • Monarch Gold Mining Company Ltd; Qualitative: colour, oxidation, hardness, shearing, texture, grain size, rock, alteration, minerals. Quantitative: alteration intensity, mineralisation intensity, structure intensity, vein percent. • WMC; RC and diamond logging describes the dominant and minor rock types, mineralisation, oxidation, alteration, texture, vein type and basic structure. Quantitative values assigned to amounts of sulphides, alteration and veining. • Gilt Edged Mining NL; Qualitative: rock code, alteration, sulphides, weathering. • Siberia Mining Corporation Ltd; Qualitative: alteration, colour, lithology, oxidation, mineralogy, vein style, vein assemblage, remarks. Quantitative: mineralisation intensity. • EGL; Qualitative: alteration, colour, grain size, lithology, oxidation, mineralogy, structure, texture, vein style, vein assemblage, remarks. Quantitative: mineralisation intensity, vein percent. • Ora Banda Mining Limited – Field logging was conducted using Geobank MobileTM software on Panasonic Toughbook CF-31 ruggedized laptop computers. Qualitative logging: Lithology, colour, oxidation, grainsize, texture, structure, hardness, regolith. Quantitative: estimates are made of quartz veining, sulphide and alteration percentages. Core photographed both wet and dry. Magnetic susceptibility and RQD were also recorded for core holes. Underground face sampling domain logging of lithology, veining, alteration, mineralisation/sulphides with each face mapped and photographed. • All holes were geologically logged in their entirety to a level of detail to support mineral resource estimation
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Goldfields Group; RC samples were routinely collected at 1m intervals and riffle split. Diamond drill core samples were taken at geological boundaries and sawn in half. RC and diamond samples were dried, crushed, split, pulverised and a 50 gm charge taken. All sampling of resource drilling incorporated a system of standards and blanks to keep strict control on assay reliability. • Monarch Gold Mining Company Ltd; RAB samples were collected at 1m intervals and 2m and 4m composites taken via a scoop method. RC samples were collected at 1m, 2m and 5m intervals. 1m samples were riffle split. Samples were prepared with a single stage mix and grind from which an assay charge was taken Composite samples with assays greater than 0.2 g/t Au were split at 1m intervals and re-analysed. Field duplicate samples were taken and analysed every 20 samples. Blanks and standards were routinely submitted with assay batches to evaluate sample preparation and assay accuracy. • WMC; In early drilling by WMC, samples were "panned' for visible gold. Percussion samples were collected at 1m intervals, split in the field. Diamond core samples were cut in half or quartered. Samples were dried in fan forced ovens at 80°C for paper packets and 140°C for samples in calico bags, sieved using a nylon mesh. Oversize samples crushed in Jacques jaw crusher to produce -6mm sample, split employing either a rotary or riffle splitter and pulverised using Tema Swing mills prior to analysis, except for soil and stream sediment samples finer than 80 mesh. A 25grm charge was taken for assaying. • Gilt Edged Mining NL; All RAB and RC holes were collected through a cyclone and sampled at 1m intervals, pipe or spear sampled, composited over 5m intervals. The composite samples weighing about 3kg were despatched for analysis. 5m composites with assays greater than 0.2 g/t Au were resampled by riffle-splitting the whole of each 1m sample down to about 3kg prior to being despatched for analysis. Samples were despatched to MinLab in Kalgoorlie where they were dried, pulverised to a nominal 90% minus 200 mesh (75

Criteria	JORC Code explanation	Commentary
		microns) and a 25 gm aliquot taken to be analysed for gold. Comprehensive QA/QC and check sampling reports were produced. Umpire assay checks were completed using a second laboratory (Genalysis). • Siberia Mining Corporation Ltd; RAB samples were collected at 1m intervals from the drillhole using a plastic bucket and laid on the ground. A scoop sample was taken from each sample to form a 5m composite. RC samples were collected at 1m intervals and passed through a cyclone and split using a two teared, 75:25 riffle splitter. The split sample (approximately 2-3kg) was stored in a drawn calico bag, which was then placed next to the split sample reject (approximately 10-15kg), which was contained in UV resistant PVC bags. A representative scoop sample was then taken from each split sample reject bags to form a 4m composite sample. Diamond half core was sampled at 1m intervals. Samples were dried, crushed, split, pulverised until 80% passed minus 75 microns and a 50 gm charge taken. Field duplicates were submitted. Composites with assays greater than 0.2 g/t Au were re-assayed using individual 1m re-split samples. • EGL & Swan Gold; RC samples were routinely collected at 1m intervals from a cone splitter and submitted for analysis. Samples were crushed, pulverised and a 50gm charge taken for analysis. Field duplicates, blanks and standards were submitted for QAQC analysis. Diamond core in sampled at 1m intervals or to zones of geological interest. Core samples are sawn in half. Minimum sample length in NQ core or 0.3m. • Ora Banda Mining Limited – RC samples were submitted as individual 1m split samples (cone splitter) or composited to 4m by PVC spear. Half-core samples, cut by automated core saw. Core sample intervals selected by geologist and defined by geological and/or mineralisation boundaries. RC samples were dried, crushed, split, pulverised and a 50gm charge taken. Field duplicates, blanks and standards were submitted for QAQC analysis. Grade control samples are prepared in the SGS on-site laboratory or at the SGS Kalgoorlie laboratory. GC samples are dried, crushed, split, pulverised and a 50gm charge taken for fire assay. Core sample intervals selected by geologist and defined by geological boundaries, cut by saw and submitted as half core. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) MP-AES finish. Field duplicates, blanks and standards were submitted for QAQC analysis. Underground core sample intervals selected by geologist and defined by geological boundaries and whole-core sampled. Whole core samples dried, crushed, split and pulverised at the SGS site laboratory. Prepared samples despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) MP-AES finish. From March 2025 samples were analysed by ~400g photon analysis by SGS. Underground face samples as per diamond drilling, including field duplicates, rock chip samples taken via hammer sampling per geology domain. Face samples submitted to SGS Kalgoorlie for`400g photon analysis.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	• Goldfields Group; Auger samples were set to Analabs (Welshpool) to be assayed for gold to 1ppb by graphite furnace P605 and arsenic to 1ppm by aqua regia hydride H605. RC samples were submitted to Australian Laboratory Services (ALS) in Kalgoorlie for gold and arsenic analysis. Fire assay methods were used for gold analysis with 50gm charge, detection limit of 0.01ppm Au, while Aqua Regia methods, with detection limits of 5ppm As, were used for arsenic analysis. Diamond drill core samples were despatched to Genalysis in Kalgoorlie and analysed for gold using 50gm fire assay to 0.01ppm. A system of standards and blanks were incorporated in all sample despatches to keep a strict control on assay reliability. QA/QC re-assaying of mineralised RC intersections and interpreted structures was undertaken later in the reporting period. • Monarch Gold Mining Company Ltd; Samples submitted to ALS for 50g Fire Assay with AAS finish. Samples were also analysed at Ultratrace for gold, palladium and platinum. Submitted field duplicates, blanks and standards for QAQC analysis. • WMC; All samples were sent to WMC Exploration Division Kalgoorlie Laboratory to be analysed for gold using wet method, aqua regia leach, reading by AAS; a 25gm sample was digested with aqua regia, the gold extracted using aliquot DIBK and the solvent backwashed. The gold concentration was determined by Atomic Absorption. • Gilt Edged Mining NL; All samples were submitted to Minlab of Kalgoorlie to be assayed for gold; 5m composites were analysed by aqua regia/AAS with a detection limit of 0.01ppm and 1m samples assayed by Fire/AAS with a detection limit of 0.01ppm. Certified reference material standards were employed. Duplicate samples, analytical standards, and check analyses at a second laboratory were used to monitor analytical quality. • Siberia Mining Corporation Ltd; All samples were submitted to SGS Analabs in Kalgoorlie to be assayed for gold using 50gm Fire Assay with detection limit at 0.01ppm Au and for sulphur. Samples were also analysed at Ultratrace. Standards and repeats (1 in 20) were used during the first phase drilling campaign to provide a reference to the internal lab standards. There was a strong correlation between standard (client) and laboratory results. Repeats of composite samples showed no problems with technique or dependability with the laboratory.

Criteria	JORC Code explanation	Commentary
		• EGL& Swan; Samples were sent to Intertek Assay Laboratories to be analysed for gold by 50gm fire assay. Certified reference material standards were employed for a gold range of 0.32 to 48.55ppm. Blanks were also employed. Satisfactory results were obtained for both. Field duplicates were routinely taken from RC sampling. • Ora Banda Mining Limited - All samples were sent to the accredited onsite SGS laboratory at Davyhurst for sample preparation. Prepared drill samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) with MP-AES finish. Face samples submitted to SGS Kalgoorlie for ~400g photon assay. Commercially prepared standard samples and blanks are inserted in the sample stream at an average rate of 1:25. Sizing results (percentage of pulverised sample passing a 75μm mesh) are undertaken on approximately 1 in 20 samples. The accuracy (standards) and precision (repeats) of assaying are acceptable. Standards and blanks (barren basalt) were inserted into the sample stream at a rate of approximately 1:12. Duplicates were submitted at a rate of approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are acceptable. Face samples assayed as per diamond core, including a field duplicate per face.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• Selected drill intersections from WMC, Goldfields and Siberia Mining Corporation diamond core have been inspected by EGL/OBM geologists. Some WMC holes have been re-logged by EGL geologists and mineralisation identified at the reported intervals. • Drill intersections from WMC and Goldfields diamond core were inspected by Siberia Mining Corporation geologists in 2005 and mineralization was visible in core at the expected intervals. Mineralisation widths and styles are very comparable with NQ2 drilling by SMC in 2004. • Holes are not deliberately twinned. • WMC; Hand written geology logs and assays were digitally captured. • EGL; Data has been verified by reviewing original drill and assay logs. Print outs of computerized sample intervals and assays generated by WMC were used to verify the intercepts reported. Geological and sample data logged directly into field computer at the core yard. Data is transferred to Perth via email and imported into GBIS SQL database by the database administrator (DBA). Assay files are received in .csv format and loaded directly into the database by the DBA. Hardcopy and/or digital copies of data are kept for reference if necessary. • Monarch Gold Mining Company Ltd; Geological and sample data was logged digitally and .csv or .xls files imported into Datashed SQL database with in-built validation. • Ora Banda Mining Limited - Geological and sample data logged directly into field computer (Panasonic Toughbook CF-31) at the core yard or at the drill rig using Geobank Mobile. Data is exported from the logging computer, copied onto the company servers and imported into Geobank SQL database by the database administrator (DBA). Assay files are received in .csv format and loaded directly into the database by the DBA. Hardcopy and/or digital copies of data are kept for reference if necessary. • Data entry, verification and storage protocols for remaining operators is unknown. • No adjustments have been made to assay data.
Location of data points	• *Accuracy and quality of surveys used to locate drillholes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• Goldfields Group; Collar co-ordinates for RC and DD holes, including elevation were surveyed with DGPS. RAB holes were located with GPS. Downhole surveys were taken every 10m for RC and DD holes, method unknown. RAB holes not downhole surveyed. The gird system used is AGD 1984 AMG Zone 51. • Monarch Gold Mining Company Ltd; Drillhole collars were surveyed by Spectrum Surveys of Kalgoorlie using RTK GPS. Downhole surveys were undertaken by electronic multiple shot (EMS) or Eastman single shot. The gird system used is GDA1994 MGA Zone 51. • WMC; Drillhole collars were surveyed by Electronic Distance Meter (EDM) theodolite by the Kalgoorlie Gold Operations' mine surveyor. Holes also surveyed using theodolite by McGay Surveys as well as by WMC mine surveyors. WMC RC holes were generally not downhole surveyed. Diamond holes down hole surveyed by Eastman single shot camera or multishot approximately every 30m. The gird system used is AGD 1984 AMG Zone 51. • Gilt Edged Mining NL; Contract surveyors were engaged for siting of drillholes prior to drilling, pick-up of accurate drillhole co-ordinates after drilling and down-hole plunge and azimuth readings. All holes drilled after 1998 were picked up by Fugro Survey Pty Ltd of Kalgoorlie using differential GPS. The gird system used is AGD 1984 AMG Zone 51. • Siberia Mining Corporation Ltd; Collar co-ordinates for northings, eastings and elevation were recorded by Fugro Spatial Solutions Pty Ltd. The grid system used is AGD 1984 AMG Zone 51. Diamond holes were down hole surveyed by gyro. RC holes generally not downhole surveyed. If surveyed, then done by Digital electronic multishot (DEMS) • EGL and Swan; Collar locations were surveyed by DGPS and downhole surveys were collected using electronic multishot by the drillers. Subsequent to drilling holes were open hole gyro surveyed by ABIMS where possible. The gird system used is GDA1994 MGA Zone 51. • Ora Banda Mining Limited (RC, DD) MGA94, zone 51. Holes are picked up using RTK GPS the mine surveyors. Drill-hole downhole surveys are recorded using an Axis digital tool. Surface grade control holes are all surveyed by the mine surveyors by RTKGPS. Grade control holes are

Criteria	JORC Code explanation	Commentary
		all downhole surveyed with north seeking gyro. Underground diamond drilling – diamond drilling collar locations picked up by mine surveyors via theodolite and known survey control points. UG diamond drill rig alignment via surveyed collar locations and DeviAligner tool, downhole surveys via DeviGyro-Ox tool. Underground face sample locations measured via laser distometer to known surveyed control points and development surveys via theodolite. The underground mine is established on a local (mine grid) with 60° rotation (0° mine grid = 60° MGA) and false (+4000m) RL. The grid and transformation parameters to MGA94, zone 51 were established by OBM surveyors. All development, drill collars and face sampling are surveyed in mine grid. • At close of mining in January 2024, OBM mine surveyors surveyed the Sand King pit area. Topographical control is considered adequate for resource modelling
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• Drilling is predominantly on a 20mN X 20mRL grid, increasing to 40mN X 40mRL at depth. Surface grade control drilling was carried out on a nominal 5m X 5m grid. Underground grade control drilling is at a nominal 10m X 10m spacing when targeting the major "Big Dog" lodes. Underground face samples are taken each 3m/4m ore development cut. • At Sand King the data spacing and distribution is sufficient to establish geological and grade continuity to support the definition of Mineral Resource and classifications as defined under the JORC 2012 code. • Composites of drill intercepts are length weighted, 1g/t lower cut-off, not top-cut, maximum 2m internal dilution. • Samples are composited to 1m for resource calculations.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• At Sand King resource drilling is predominantly inclined to the south, optimal for the predominantly ENE (060°) striking, north dipping mineralisation. UG diamond drilling is from cuddy's in fan patterns which does lead to less than optimal intersection angles of the outermost holes. • It is not known whether there is any introduced sample bias due to drill orientation.
Sample security	• *The measures taken to ensure sample security.*	• Unknown for earlier operators. • EGL – Samples are bagged, tied and in a secure yard on site. Once submitted to the laboratories they are stored in cages within a secure fenced compound. Samples are tracked through the laboratory via their LIMS. • Monarch - Pre-numbered sample bags were put into numbered plastic bags. These numbers were written on the submission forms which were checked by the geologist. Plastic bags were then securely cable tied and placed in a secure location. Samples were then picked up by the Lab in Kalgoorlie or deliver to Perth via courier. A work order conformation was emailed to Monarch personnel for each sample submission once samples were received by the Laboratory. • Ora Banda Mining Limited - Samples were collected on the day of drilling and bagged into cable tied polyweave bags. Polyweave bags are stored into bulka bags on pallets in a secure yard on-site. Once submitted to the laboratories they are stored in cages within a secure fenced compound. Samples are tracked through the laboratory via their LIMS.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• Digital data from the SQL database has been reviewed by OBM and is consistent with hard copy and digital WAMEX data. • Siberia Mining Corporation conducted a due diligence on the data and core in 2005 and were "comfortable with the quality and integrity of the data". Digital data has been reviewed and is consistent with hard copy data. • Monarch Gold Mining Company Ltd; Monthly QAQC reports were produced to monitor accuracy and precision. • OBM audits core logging and sampling on a weekly basis, checking for logging of lithology, alteration & sulphides is to mine standard. The relationship between sulphide % and gold grades is monitored. Sample intervals < minimum length is monitored

Section 1 Sampling Techniques and Data – Round Dam

Information for historical (Pre Ora Banda Mining Limited from 1980's to 2010) drilling and sampling has been extensively viewed and validated where possible. Information pertaining to historical QAQC procedures and data is incomplete but of a sufficient quality and detail to allow drilling and assay data to be used for resource estimations.

Further Ora Banda Mining Limited has undertaken extensive infill and confirmation drilling which confirm historical drill results. Sections 1 and 2 describe the work undertaken by Ora Banda Mining Limited and only refer to historical information where appropriate and/or available.

Criteria	JORC Code Explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.*	• Aberfoyle/Bardoc - Reverse Circulation (RC) and Rotary Air Blast (RAB) sampling methods generally unknown however usually collected as 1m samples and composited to 2 to 4m samples when outside mineralised zones. RC drilling between 4 and 6 inch diameter hammers with use of face sampling hammer known from 1992 onwards. Pre-1990 Rotary Air Blast (RAB) holes generally sampled on 2-3m intervals and composited to 6m. • Cons Gold (Consolidated Gold) – Reverse Circulation (RC) 1m samples where alteration is visible. Remainder of hole composited to 4m. 2 to 3 kg samples sent to laboratory for crushing, pulverising and 50g Fire Assay. NQ diamond except for geotechnical purposes (HQ triple) • Croesus – Reverse Circulation (RC) 1m samples collected under cyclone. 5m comps assayed for gold by 50g Fire assay. NQ diamond except for geotechnical purposes (HQ triple) • DPPL (Davyhurst Project Pty. Ltd.)- 4.25 to 5.5 inch Reverse Circulation (RC) drilling with face hammer. Potential mineralisation sampled and assayed on a metre basis otherwise 4m composites. NQ diamond except for geotechnical purposes (HQ triple) • EGS (Eastern Goldfields)- Reverse Circulation (RC) samples collected from the riffle splitter directly off tig into calico bags. Splitter maintained on level site to ensure sample representivity. 1m samples are pulverised and a 40g charge is analysed by Fire Assay • Monarch - Riffle split Reverse Circulation (RC) samples were collected at 1m intervals and despatched for analysis by pulverisation and fire assay. Selected Rotary Air Blast (RAB) 2m-4m scoop composites and 1m intervals were despatched for analysis. Not all intervals were sampled. SRK holes were Reverse Circulation (RC) and were 4m composites of 1m samples • Swan Gold Diamond - Half core samples, cut by saw. Samples intervals selected by geologist and defined by geological boundaries. Minimum sample length is 0.3m, maximum 1.5m. Core is aligned and measured by tape, comparing back to down hole core blocks, consistent with industry practice. Samples are pulverized and a 40g charge is analysed by Fire Assay. 1m Reverse Circulation (RC): 5.125 inch face sampling hammer with samples collected under cone splitter • Texas Gulf – sampling methods unknown • West Coast Holdings – Rotary Air Blast (RAB) drilling 2m intervals were passed though riffle splitter for approximately 1kg sample. • WMC - Reverse Circulation (RC) Sampling on 1m basis • WESCEF - 1m RC samples using face sampling hammer with samples collected under cone splitter. All pegmatite, felsic rocks, and altered/veined intervals are sampled, and a 10m buffer either side of these intervals are also sampled. Li-pegmatite specific standards, and field duplicates (taken via the rig-mounted cone splitter during drilling) are both inserted at a rate of one every 25 samples. For gold assay sample piles scoop sampled into 4m comps by OBM personnel. Samples prepped in SGS site lab by either pulverising (Fire Assay) or crushed using orbis crusher (Photon Assay). Samples analysed at SGS, Kalgoorlie or SGS Perth. Splits take where composite grade >0.1g/t. For elements other than gold, samples submitted to ALS for multielement analysis by 3 suites: ME-ICP89, ME-MS89L and ME-ICP61. For gold assays samples. Ora Banda Mining Limited (OBM) - 1m RC samples using face sampling hammer with samples collected under cone splitter. 4m composite RC samples were taken outside of mineralised zone, collected using a scoop from the sample piles at the drill site. 1m cone spilt samples were taken within the expected mineralised zones. Core sample intervals selected by geologist and defined by geological boundaries. Several analytical methods and laboratories have been utilised for assaying. Samples from exploration drilling were initially sent to ALS, Perth for pulverising, and assay by 50g fire assay Microwave Plasma-Atomic Emission Spectroscopy (MP-AES). Most resource definition samples were sent to SGS on-site laboratory for crushing and analysis by photon at SGS, Kalgoorlie. A small number of samples were sent to SGS, Perth for 50g fire assay, AAS finish. •

Criteria	JORC Code Explanation	Commentary
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Aberfoyle/Bardoc - RC, RAB and Diamond details unknown however NQ diamond known to be used. RC drilling with use of face sampling hammer known from 1992 onwards. • ConsGold – NQ diamond, RAB and RC. 4.25 to 5.5 inch RC drilling with stabilisers and face sampling hammers. • Croesus – Diamond holes NQ2 diameter. RC details unknown but assumed to be face sampling hammers • DPPL - NQ and RC. RC drilling with stabilisers and face sampling hammers. • EGS - NQ and RC. RC drilling using Face sampling Hammer, 5.25" diameter • Monarch - RC samples were collected by Kennedy Drilling using a 4 inch blade. 5.5 inch diameter RC drilling • Swan Gold "HQ3 to approx. 40m, then NQ2 to BOH. All core oriented by spear RC: 5.125 inch face sampling hammer" • Texas Gulf – RC hammer type unknown • West Coast Holdings – Bit, roller and open hole hammer used for RAB drilling. • WMC - RC and RAB drilling details unknown • WESCEF - 5.5 – 5.625 inch diameter RC holes using face sampling hammer with samples collected from a rig mounted cone splitter into calico bags which are submitted for assay at ALS. • Ora Banda Mining Limited (OBM) – 5.5 – 5.625 inch diameter RC holes using face sampling hammer with samples collected from a rig mounted cone splitter into calico bags which are submitted for assay. Some core holes have RC pre-collars, then NQ2, HQ3 or PQ3 coring to BOH. All core oriented by Axis instrument. Drilling was carried out by contractors Top Drill Pty Ltd.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• RC drill recoveries were not recorded by Aberfoyle/Bardoc, Consolidated Gold, Croesus, DPPL, EGS, Monarch, Texas Gulf, West coast holdings or WMC • Swan - Diamond drill recoveries are recorded as a percentage calculated from measured core against downhole drilled intervals (core blocks). • WESCEF - RC sample recoveries are approximated based on the size of the bulk sample and recorded in drill log tables. Sample weights are determined by the laboratory. • OBM - RC sample recoveries are approximated based on the size of the bulk sample and recorded in drill log tables. Sample weights are determined by the laboratory. Diamond drill recoveries are recorded as a percentage calculated from measured core against downhole drilled intervals (core blocks).
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Aberfoyle/Bardoc - Qualitative: lithology, colour, grainsize, structures, alteration. Quantitative: Quartz mineralisation • Consolidated Gold/ DPPL - Qualitative: lithology, colour, oxidation, alteration, with grainsize, texture and structure often recorded in diamond drilling. Quantitative: Quartz veining. Core photographed • Croesus - Most holes photographed, geologically logged and geotechnical and magnetic susceptibility measurements were taken. Qualitative: Lithology, colour, grainsize, alteration, oxidation, texture, structures, regolith. Quantitative: Quartz veining • EGS - Qualitative: Lithology, colour, oxidation, grainsize, texture, structure, hardness, regolith. Quantitative: estimates are made of quartz veining, sulphide and alteration percentages. Core photographed • Monarch - Qualitative: lithology, colour, oxidation, grainsize, texture, structure, hardness, regolith. Quantitative: estimates are made of quartz veining, sulphide percentages. Core photographed • Swan - Qualitative: lithology, colour, oxidation, grainsize, texture, structure, regolith. Quantitative: estimates are made of quartz veining, sulphide and alteration percentages. • Texas Gulf - Qualitative: lithology, oxidation • West coast holdings - Qualitative: colour, oxidation, lithology, alteration Quantitative: Quartz, Iron • WMC RC: Qualitative: Lithology, Colour, Grainsize, Alteration and oxidation. Some logging detail was lost during translation from one logging system to another. This has been rectified by referring back to original logs. • WESCEF - Holes are geologically logged in their entirety. • OBM - Field logging was conducted using Geobank MobileTM software on Panasonic Toughbook CF-31 ruggedized laptop computers. Qualitative: Lithology, colour, oxidation, grainsize, texture, structure, hardness, regolith. Quantitative: estimates are made of quartz

Criteria	JORC Code Explanation	Commentary
		veining, sulphide and alteration percentages. Core photographed wet and dry. Magnetic susceptibility recorded for core holes. Bulk density measurements taken at regular intervals for core holes (determined by Archimedes Principle). Downhole density measurements also acquired from selected holes, principally for additional data from oxide and transitional material.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Aberfoyle/Bardoc – Diamond core sawn in half. RC and RAB samples with variable compositing lengths and often 1m samples. Method unknown before 1992, but thereafter riffle split to approximately 2kg samples. RC and RAB was usually prepared by single stage mixer and grind. Diamond, when known was jaw crushed and ring milled for a 50g charge fire assay. Duplicate studies undertaken at times, usually with good correlation. • Consgold RC Samples collected via cyclone at 1m intervals and passed through 3 stage riffle splitter. A 2-3kg fraction was calico bagged for analysis, the residue collected in plastic bags and stored on site. Potentially mineralised zones were sampled at 1m intervals, the remainder composited to 4m by unknown method. Composite samples returning >0.19g/t were re submitted at 1m intervals. Samples underwent mixermill preparation (2-3kg) by Amdel Laboratories. RAB 4m composite samples using PVC spear. Samples returning >0.19g/t were re submitted at 1m intervals Diamond drill samples were sawn into half core. One half was jaw crushed, then pulverised using a labtechnics mill. A quartz blank was pulverised between each sample to avoid contamination. Field duplicates at 1 in 20 frequency from residues submitted. • Croesus RC - 1m samples collected under cyclone. 5m comps, spear sampled with 50mm PVC pipe. Wet RC drill samples were thoroughly mixed in the sample retention bag and scoop sampled to form a composite sample. 3-5kg five metre composite analytical samples, returning values greater than 0.1g/t gold, were riffle split at 1m intervals, were samples where dry, and grab sampled where wet. Diamond tails were cut to half core and sampled based on geological boundaries and identified prospective zones. Samples size varied from 0.2m to1m. Core samples were sent to Ultratrace Laboratories of Perth • DPPL – RC 3 stage riffle split then 4m compositing. RAB 4m composite samples using PVC spear. BOTH RC and RAB composites returning >0.19ppm Au re-submitted as 1m samples. Duplicates at 1 in 20 frequency from residues submitted. • EGS - Riffle split into calico bags. Wet or moist samples are noted during sampling • Monarch - RC samples were collected at 4m or 1m composites intervals and despatched for analysis. Samples were riffle split and prepared with single stage mix and grinding. Duplicates are taken 1 in 25 when taking 1m splits straight from the rig. When doing re-splits on composite results 1 in 20 duplicate with occasional triplicates (about 1 every 50 re-splits) • Swan - Core was cut with Almonte diamond saw and half core sampled. • Texas Gulf - Whole metres placed in plastic sacks and were then split to approximately 500g samples. Split method unknown. Samples crushed, disc pulverized then split to 250g. Petrographic study completed by Mintek Services. • West Coast Holdings - 2m intervals with passed though riffle splitter for approximately 1kg sample. • WMC - RC Sampling on 1m basis, methods undocumented. Assay by aqua regia method, unknown laboratory. • WESCEF - RC samples for non gold elements were submitted as individual 1m samples taken from the onsite cone splitter. 4m comp samples taken from 1m sample piles for gold assay. Samples submitted for gold analysis with OBM routine blanks and standards for monitoring lab performance. OBM - RC samples were submitted either as individual samples taken from the onsite cone splitter or as four metres composite samples taken by metal scoop. Core sample intervals selected by geologist and defined by geological boundaries, cut by saw and submitted as half core. Several analytical methods and laboratories have been utilised for assaying. Samples from exploration drilling were initially sent to ALS, Perth for pulverising, and assay by 50g fire assay Microwave Plasma-Atomic Emission Spectroscopy (MP-AES). Most resource definition samples were sent to SGS on-site laboratory for crushing and analysis by photon at SGS, Kalgoorlie. A small number of samples were sent to SGS, Perth for 50g fire assay, AAS finish. • Field duplicates, blanks and standards were submitted for QAQC analysis.. Field duplicates, blanks and standards were submitted for QAQC analysis.

Criteria	JORC Code Explanation	Commentary
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	• Aberfoyle/Bardoc - multiple methods at Sheen, Amdel, Genalysis, Classic, Comlabs and Australian Laboratories usually 50g fire assay for RC and aqua regia or 50g fire assay for RAB. QA samples unknown • Consolidated Gold/ DPPL – RC and RAB - Mixermill prep with fire assay 50g charge at AMDEL, Minilab or Analabs Laboratories in Kalgoorlie. Core was diamond sawn, jaw crushed, milled using LABTECHNICS mill at AMDEL for 50g charge by fire assay. Gannet standards submitted to monitor lab accuracy for infill resource drilling. Pulp umpire analysis was done but frequency unknown (1995). Screen fire assays of selected high grade samples. Quartz blanks between each diamond sample • Croesus - Samples analysed for Au by Fire Assay/ICPOES by Ultratrace in Perth. Samples were dried, crushed and split to obtain a sample less than 3.5kg, and then fine pulverised prior to a 50gm charge being collected and analysed. Every 20th sample was duplicated in the field and submitted for analysis. Gannet standards and blank samples made by Croesus were submitted with split sample submissions. QAQC analysis of repeats was analysed by Croesus Mining NL. for their drilling completed during 2000 • Monarch - ALS Laboratory procedures: The samples were sort and dried where necessary. The samples were split via a riffle splitter to <3 kg and round in a ring mill pulverized using a standard low chrome steel ring set to >85% passing 75 micron. If sample was >3 kg it was split prior to pulverising and the remainder retained or discarded. Then a 250g representative split sample was taken and the remaining residue sample stored. A 50g sample charge was taken from the 250g representative sample, fused with a lead concentrate using the laboratory digestion method FA-Fusion, then digested and analysed by Atomic Absorption Spectroscopy (Au-AA26) against matrix matched standards. Ultra Trace procedures: The samples were sort and dried where necessary. 2.5 – 3kg sample was pulverized using a vibrating disc then split into a 200 -300g charge and the residue sample stored. A 40g sample charge is taken and analysed for gold (Au) by lead collection fire assay. • Texas Gulf - Samples crushed, disc pulverized then split to 250g. Bromine digest followed by ketone extraction at Pilbara Las, Kalgoorlie. Noted as not suitable in presence of sulphides. Values greater than 0.8g/t re-assayed by Fire Assay. • WMC - Drill samples were assayed by aqua regia method, unknown laboratory. • WESCEF - Commercially prepared standard samples and blanks are inserted in the sample stream at a rate of 1:25 for standards and 1:25 for blanks, when analysing for gold. Sizing results (percentage of pulverised sample passing a 75$_{\mu}$m mesh) are undertaken on approximately 1 in 40 samples. Duplicate samples are submitted for RC holes only at a rate of approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are acceptable • OBM – Up to 2022, samples sent to Nagrom in Perth. The samples have been analysed by Firing a 50gm portion of the sample. Lower sample weights may be employed for samples with very high sulphide and metal contents. This is the classical fire assay process and will give total separation of gold. An ICPOES finish is used. Commercially prepared standard samples and blanks are inserted in the sample stream at a rate of 1:25 for standards and 1:25 for blanks. Sizing results (percentage of pulverised sample passing a 75$_{\mu}$m mesh) are undertaken on approximately 1 in 40 samples. Duplicate samples are submitted for RC holes only at a rate of approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are acceptable. For all drilling from 2022, All samples were sent to the accredited onsite SGS laboratory at Davyhurst for sample preparation. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) with MP-AES finish or ~400g Photon analysis. Commercially prepared standard samples and blanks are inserted in the sample stream at an average rate of 1:25. Sizing results (percentage of pulverised sample passing a 75$_{\mu}$m mesh) are undertaken on approximately 1 in 20 samples. The accuracy (standards) and precision (repeats) of assaying are acceptable. Standards and blanks were inserted into the sample stream at a rate of approximately 1:12. Duplicates were submitted at a rate of approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are acceptable. Holes not deliberately twinned.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• OBM - Geological and sample data logged directly into field computer at the drill rig or core yard using Geobank Mobile. Data is transferred to Perth via email or through a shared server and imported into Geobank SQL database by the database administrator (DBA). Assay files are received in .csv format and loaded directly into the database by the DBA. Hardcopy and/or digital copies of data are kept for reference if necessary. • WESCEF – Geological logging and Li sampling data all supplied to OBM. Gold sampling and assay verification same as for OBM. procedures • Monarch Gold Mining Company Ltd; Geological and sample data was logged digitally and .csv or .xls files imported into Datashed SQL database with in-built validation. Samples bags were put into numbered plastic bags and then cable tied. Samples collected daily from site by laboratory.

Criteria	JORC Code Explanation	Commentary
		• Data entry, verification and storage protocols for remaining operators is unknown. • No adjustments have been made to assay data.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• RAB and AC holes are/were not routinely collar surveyed or downhole surveyed due to their limited use in resource estimation. To this end, discussion of RAB and AC drilling is omitted from this section. RC/GC (grade control) and shallow RC holes are/were not routinely downhole surveyed due to their shallow nature reducing the chance of significant deviation. Barren exploration RC holes not routinely downhole surveyed or collar surveyed. DD holes routinely collar and downhole surveyed by most operators or have been re-surveyed by subsequent operators. • The influence of magnetic rocks on the azimuths of magnetic down hole surveys is minor. Early holes surveyed in AMG zone 51 and converted to MGA using Geobank and or Datashed data management software. • Aberfoyle/Bardoc (RC, RC/DD, DD) Various local grids which have undergone 2 point transformations. RC collars and downhole surveys known to be surveyed at times, presumably when anomalous gold intersected. DD holes downhole surveyed by Eastman single shot (25m interval average) or Multishot (5m interval average) • Cons Gold/DPPL (RC, DD) Local grids and AMG84 zone 51 used. RC and DD Collars surveyed by licensed surveyors to respective grids. Holes of all types routinely collar surveyed whist RC resource holes routinely downhole surveyed by various methods including gyro and EMS with average intervals ranging between 10-25m. • Croesus (RC, DD) Various local grids and AMG zone 51. RC, DD holes routinely collar surveyed and downhole surveyed using Electronic Multishot (EMS), GRYO, Eastman single shot or combination thereof at 10-15m average interval. • Monarch (RC) -Various local grids and MGA. Holes routinely collar surveyed and downhole surveyed using EMS, or GYRO at 5m interval average or Eastman single shot (28m interval average). • Texas Gulf (RC) Local grid: MC30/1317 based on 351.5^{0}baseline, parallel to tenement boundary. MC30/1327 based on 355.5 • WMC (RC, DD) - Digital data provided by ConsGold. (Wamex report a50226). Downhole surveys when performed were by undocumented method with a 16m interval average • EGL and Swan; Collar locations were surveyed by DGPS and downhole surveys were collected using electronic multishot by the drillers. Subsequent to drilling holes were open hole gyro surveyed by ABIMS where possible. The gird system used is GDA1994 MGA Zone 51. • WESCEF - MGA94, zone 51. Drill hole collar positions were picked up by an OBM mining surveyor using RTKGPS subsequent to drilling. All downhole surveys were taken every 10m by Gyro. • OBM (RC, DD) MGA94, zone 51. Drill hole collar positions were picked up by a contract surveyor using RTKGPS subsequent to drilling. Drill-hole, downhole surveys are recorded every 30m using a reflex digital downhole camera. Some RC holes not surveyed if holes short and/or drilling an early stage exploration project. For all drilling from 2022 Drill hole collar positions were picked up by an OBM mining surveyor using RTKGPS subsequent to drilling. All downhole surveys were taken every 10m by Gyro.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• Data spacing highly variable from wide spaced ~800m x ~80m regional RAB to close spaced resource drilling ~10m x ~10m and grade control drilling at ~5m x ~5m. • Drill hole spacing is adequate to establish geological and grade continuity for the deposits that currently have resources reported. • Drill intercepts are reported at a Lower cut off of 0.5g/t with a secondary cut off of 1.0g/t **or** a Lower cut off of 1.0g/t with a secondary cut off of 10.0g/t. Maximum 4m internal dilution.
Orientation of data in relation to	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	• Drilling by Aberfoyle/Bardoc, Consolidated Gold, Croesus, DPPL, EGS, Monarch, Texas Gulf and WMC was predominately inclined at between -50 and -60 degrees towards local grid east (~80^{0} MGA Azi). Some early exploration RAB holes drilled vertically • OBM – RC drilling is predominately inclined at between -50 and -60 degrees towards local grid east (~80^{0} MGA Azi). Drilling inclined to

Criteria	JORC Code Explanation	Commentary
geological structure	• *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	the west is only done when lodes are deemed to be vertical or if local landforms prevent access. • WESCEF – Holes primarily drilled for lithium exploration in varying orientations that are frequently not perpendicular to gold mineralisation.
Sample security	• *The measures taken to ensure sample security.*	• Unknown for earlier operators. • West coast holdings - Residues stored on site but security measures unknown • Texas Holdings - Residues stored on site but security measures unknown • Monarch - Pre-numbered sample bags were put into numbered plastic bags. These numbers were written on the submission forms which were checked by the geologist. Plastic bags were then securely cable tied and placed in a secure location. Samples were then picked up by the Lab in Kalgoorlie or deliver to Perth via courier. Awork order conformation was emailed to Monarch personnel for each sample submission once samples were received by the Laboratory. • Swan Gold – Samples are bagged, tied and in a secure yard. Once submitted to the laboratories they are stored in cages within a secure fenced compound. Samples are tracked through the laboratory via their LIMS. • WESCEF – Same as OBM for samples assayed for gold. • OBM – Samples are bagged into cable-tied polyweave bags and stored in bulka bags in a secure yard. Once submitted to the laboratories they are stored in cages within a secure fenced compound. Samples are tracked through the laboratory via their LIMS
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• No audits of sampling techniques have been done.

Section 1 Sampling Techniques and Data – Waihi

Information for historical (Pre Ora Banda Mining Limited from 1980's to 2010) drilling and sampling has been extensively viewed and validated where possible. Information pertaining to historical QAQC procedures and data is incomplete but of a sufficient quality and detail to allow drilling and assay data to be used for resource estimations. Further Ora Banda Mining Limited has undertaken extensive infill and confirmation drilling which confirm historical drill results. Sections 1 and 2 describe the work undertaken by Ora Banda Mining Limited and only refer to historical information where appropriate and/or available.

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure*	• Billiton - RAB and RC 1m samples with RAB being composited to 2m. Diamond core of NQ size. Assay sample techniques undocumented • Consolidated Exploration (Consex) – RAB 1m samples usually dispatched as 3m composites but occasional 1m. RC a mix of 1m sampling or 2m composites. Lady Eileen programs RC drilling made use of roller, Blade or hammer with crossover sub all nominally 5.5-inch diameter to obtain 2-3kg sample. Composite 2m samples were hammer milled, mixed and split to 200g then pulverised. 1m samples single stage mix and ground. Subsamples taken for aqua regia and fire assay. • Cons Gold (Consolidated Gold) – RC 1m samples where alteration is visible. Remainder of hole composited to 4m. 2 to 3 kg samples, including core, sent to laboratory for crushing, pulverising and 50g Fire Assay.

Criteria	JORC Code explanation	Commentary
	sample representivity and the appropriate calibration of any measurement tools or systems used. • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.*	• Croesus – RC 1m samples collected under cyclone. 5m comps assayed for gold by 50g Fire assay. NQ diamond except for geotechnical purposes (HQ triple). • DPPL (Davyhurst Project Pty. Ltd.)- 4.25 to 5.5-inch RC drilling with face hammer. Potential mineralisation sampled and assayed on a metre basis otherwise 4m composites. Samples jaw crushed and pulverised before taking a 50gm charge for fire assay. • Ora Banda Mining Limited (OBM) - RC samples collected from the levelled cone splitter directly off rig into calico bags. Splitter maintained on level site to ensure sample representivity. 1m samples are dried, crushed, pulverised and a 50g charge is analysed by Fire Assay. Half core samples, cut by saw. Core sample intervals selected by geologist and defined by geological and/or mineralisation boundaries, or sampled to 1m. Samples are crushed, pulverized and a 40g or 50g charge is analysed by Fire Assay. For all drilling since 2022, - 1m RC samples using face sampling hammer with samples collected under cone splitter. 4m composite RC samples were taken outside of mineralised zone, collected using a scoop from the sample piles at the drill site. 1m cone spilt samples were taken within the expected mineralised zones. Core sample intervals selected by geologist and defined by geological boundaries. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay. From 7 March 2025 samples were analysed by ~400g photon analysis by SGS. • WMC - RC Sampling on 1m basis, assayed by aqua regia method, unknown laboratory.
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Billiton RAB and RC (Conventional hammer) diameter undocumented with use of roller/blade and hammer. NQ Diamond core • Consex - RC drilling with roller, blade or hammer with crossover sub. • Cons Gold – NQ diamond and HQ (triple) for geotechnical holes. RAB and RC. 4.25 to 5.5-inch RC drilling with stabilisers and face sampling hammers. • Croesus – Diamond holes NQ2 diameter. RC and RAB details undocumented but assumed to be industry standard at the time being 5.5-inch face sampling hammers and 4-inch diameter respectively. • Delta – RAB - details undocumented • DPPL - NQ core and HQ for geotechnical holes. RC drilling with stabilisers and face sampling hammers. • OBM - HQ3 coring to approx. 40m, then NQ2 to BOH. Early core (2016 and 2019) was oriented by reflex instrument, 2025 and 2026 drill core was oriented by an axis instrument. RC drilled with face sampling hammer, 5.5" – 5.625" diameter. • WMC – Conventional RC hammer, diameter unknown and RAB drilling details undocumented.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• RC drill recoveries were not recorded by Aberfoyle/Bardoc, Anaconda, Ashton, Consolidated Gold, Croesus, Delta, DPPL, Hill Minerals, Intrepid, Monarch, Mt Kersey, Normandy, Pancontinental, Texas Gulf, West coast holdings or WMC • Billiton – Recoveries for some RC drilling programs were examined in 1986 but raw data not available. • Consex – 2 metre plastic pipe inserted into cyclone vent. Cyclone washed at the end of each hole or if water injected. Sample weights measured for Homeward bound (no bias observed) and Lady Eileen prospects (generally no bias observed aside from two high grade samples perceived to be due to coarse grained gold) • OBM - Diamond drill recoveries are recorded as a percentage calculated from measured core against downhole drilled intervals (core blocks). RC sample recoveries are approximated based on the size of the bulk sample and recorded in drill log tables. RC sample weights are received from the laboratory. • It is unknown whether a relationship exists between sample recovery and grade or whether sample bias may have occurred.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Billiton - Qualitative: lithology, alteration for Diamond and RAB. RC logging details unavailable • Consolidated Exploration- Qualitative: lithology, colour, alteration, grainsize (at times). Quantitative: Quartz mineralisation at times • Consolidated Gold/ DPPL - Qualitative: lithology, colour, oxidation, alteration, with grainsize, texture and structure often recorded in diamond drilling. Quantitative: Quartz veining. Core photographed. Logging entered directly into HPLX200 data loggers. • Croesus - Most holes photographed, geologically logged and geotechnical and magnetic susceptibility measurements were taken. Qualitative: Lithology, colour, grainsize, alteration, oxidation, texture, structures, regolith. Quantitative: Quartz veining • OBM - Qualitative: Lithology, colour, oxidation, grainsize, texture, structure, hardness, regolith. Quantitative: estimates are made of quartz veining, sulphide and alteration percentages. Core photographed wet and dry. Magnetic susceptibility recorded for core holes. Bulk density measurements taken at regular intervals for core holes (determined by Archimedes Principle). pXRF used extensively to assist with classification of lithology. • WMC RC: Qualitative: Lithology, Colour, Grainsize, Alteration and oxidation

Criteria	JORC Code explanation	Commentary
		• Some logging detail was lost during translation from one logging system to another. This has been rectified by referring back to original logs. • Entire holes were logged by all operators
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in-situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Billiton – Sub-sampling methods undocumented. 1m repeat fire assays of 2m RAB comps at Lady Eileen were done. Duplicates for RAB and RC inserted however frequency unknown. • Consex – RC holes sampled on 1m basis and riffle split to 1-2kg samples for 3m composites or 2-3kg samples for 2m composites. Composite 2m samples were hammer milled, mixed and split to 200g then pulverised to 200#. 1m samples single stage mix and ground to 200#. • Consgold - RC Samples collected via cyclone at 1m intervals and passed through 3 stage riffle splitter. A 2-3kg fraction was calico bagged for analysis, the residue collected in plastic bags and stored on site. Potentially mineralised zones were sampled at 1m intervals, the remainder composited to 4m by unknown method. Composite samples returning >0.19g/t were re submitted at 1m intervals. Samples underwent mixer mill preparation (2-3kg) by Amdel Laboratories. RAB 4m composite samples using PVC spear. Samples returning >0.19g/t were re submitted at 1m intervals. Diamond drill samples were sawn into half core. One half was jaw crushed, then pulverised using a labtechnics mill. A quartz blank was pulverised between each sample to avoid contamination. Field duplicates from residues at 1 in 20 frequency submitted. • Croesus RC/RAB - 1m samples collected under cyclone. 5m comps, spear sampled with 50mm PVC pipe. Wet RC drill samples were thoroughly mixed in the sample retention bag and scoop sampled to form a composite sample. 3-5kg five metre composite analytical samples, returning values greater than 0.1g/t gold, were riffle split at 1m intervals, were samples where dry, and grab sampled where wet. RAB 1m resampling method undocumented. Samples were dried, crushed and split to obtain a sample less than 3.5kg, and then fine pulverised prior to a 50gm charge being collected and analysed. Every 20th sample was duplicated in the field and submitted for analysis. Diamond tails were cut to half core and sampled based on geological boundaries and identified prospective zones. Samples size varied from 0.2m to1m. Core samples were sent to Ultratrace Laboratories of Perth • DPPL – RC 3 stage riffle split then 4m compositing. RAB 4m composites sampled using PVC spear. Both RC and RAB composites returning >0.19ppm Au re-submitted as 1m samples. Field duplicates from residues at 1 in 20 frequency submitted. • OBM – RC samples were submitted either as individual samples taken from the onsite cone splitter or as four metres composite samples taken by metal scoop. Core sample intervals selected by geologist and defined by geological boundaries, cut by saw and submitted as half core. All samples were dispatched to the SGS laboratory at the Davyhurst site for pulverising. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10). Field duplicates, blanks and standards were submitted for QAQC analysis. From 10 March 2025 samples were analysed by ~400g photon analysis by SGS. Field duplicates, blanks and standards were submitted for QAQC analysis. • WMC - RC Sampling on 1m basis, methods undocumented. Assay by aqua regia method, unknown laboratory.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	• Billiton - Laboratory and methods undocumented. Standards for RAB and RC inserted however frequency unknown • Consex – Genalysis composite 2m samples were hammer milled, mixed and split to 200g then pulverised to 200#. 1m samples single stage mix and ground to 200#. Phase 1 standard wet chemical multi acid digestion and AAS. Second phase were also pre-roasted. Results of >1g/t re-assayed by fire assay. Check assays at umpire lab (Classic labs) for Lady Eileen drilling - significant differences in high grade samples, otherwise considered good. • Consolidated Gold/ DPPL – RC and RAB - Mixer mill prep with fire assay 50g charge at AMDEL, Minilab or Analabs Laboratories in Kalgoorlie. Half core was diamond sawn, jaw crushed, milled using LABTECHNICS mill at AMDEL for 50g charge by fire assay. Gannet standards submitted to monitor lab accuracy for infill resource drilling. Pulp umpire analysis was done but frequency unknown (1995). Screen fire assays of selected high grade samples. Quartz blanks submitted between each diamond core sample. • Croesus samples analysed for Au by Fire Assay/ICPOES by Ultratrace in Perth. Gannet standards and blank samples made by Croesus were submitted with split sample submissions. QAQC analysis of repeats was analysed by Croesus Mining NL. for their drilling completed during 2000. • OBM - Up to 2022 Samples sent to Nagrom in Perth. The samples have been analysed by Firing a 50gm portion of the sample. Lower sample weights may be employed for samples with very high sulphide and metal contents. This is the classical fire assay process and will give total separation of gold. An ICPOES finish is used. Commercially prepared standard samples and blanks are inserted in the sample stream at a rate of 1:25 for standards and 1:25 for blanks. Sizing results (percentage of pulverised sample passing a 75μm mesh) are undertaken on approximately 1 in 40 samples. Duplicate samples are submitted for RC holes only at a rate of

Criteria	JORC Code explanation	Commentary
		approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are acceptable. For all drilling from 2022, All samples were sent to the accredited onsite SGS laboratory at Davyhurst for sample preparation. Prepared samples were then despatched to SGS laboratories in Kalgoorlie for a 50g charge Fire Assay (GO_FAP50V10) with MP-AES finish or ~400g Photon analysis. Commercially prepared standard samples and blanks are inserted in the sample stream at an average rate of 1:25. Sizing results (percentage of pulverised sample passing a 75μm mesh) are undertaken on approximately 1 in 20 samples. The accuracy (standards) and precision (repeats) of assaying are acceptable. Standards and blanks were inserted into the sample stream at a rate of approximately 1:12. Duplicates were submitted at a rate of approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are acceptable. Commercially prepared standard samples and blanks are inserted in the sample stream at a rate of 1:25 for standards and 1:25 for blanks. Sizing results (percentage of pulverised sample passing a 75μm mesh) are undertaken on approximately 1 in 40 samples. Duplicate samples are submitted for RC holes only at a rate of approximately 1:30. The accuracy (standards) and precision (repeats) of assaying are deemed acceptable. • WMC drill samples were assayed by aqua regia method, unknown laboratory. • Fire assay and photon are considered a total technique and aqua regia is considered a partial technique. • Historic operators assayed by "AAS". This is assumed to be aqua regia.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• OBM geologists have viewed selected diamond holes from certain deposits, including Waihi and verified the location of mineralised intervals. • Cons Gold – Each metre interval geologically logged directly into HPLX2000 with standardised logging codes. • Twinned holes were occasionally used by previous operators, but this practice was not common. • OBM - Geological and sample data logged directly into field computer (Panasonic Toughbook CF-31) using Geobank Mobile. Data is exported onto company servers and imported into Geobank SQL database by the database administrator (DBA). Assay files are received in .csv format and loaded directly into the database by the DBA. Hardcopy and/or digital copies of data are kept for reference if necessary. • Data entry, verification and storage protocols for remaining operators is unknown. • No adjustments have been made to assay data
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• RAB and AC holes are/were not routinely collar surveyed or downhole surveyed due to their limited use in resource estimation. To this end, discussion of RAB and AC drilling is omitted from this section. RC/GC (grade control) and shallow RC holes are/were not routinely downhole surveyed due to their shallow nature reducing the chance of significant deviation. Barren exploration RC holes were not routinely downhole surveyed, or collar surveyed. DD holes were routinely collar and downhole surveyed by most operators or have been re-surveyed by subsequent operators. • The influence of magnetic rocks on the azimuths of magnetic down hole surveys is minor. Early holes surveyed in AMG zone 51 and converted to MGA using Geobank and or Datashed data management software. • Billiton (RC, DD) Local Lights of Israel grid undergone 2-point transformation. Downhole surveys when performed were by undocumented method with a 25m interval average • Consex (RC). Drilled on local grids (possibly truncated AMG84, zone 51). Holes appear to have been surveyed using AMG, zone 51 grid at a later stage. Numerous vertical holes not down-hole surveyed. Downhole surveys when performed were by undocumented method with a 9m interval average • Cons Gold/DPPL (RC, DD) Local grids and AMG84 zone 51 used. RC and DD Collars surveyed by licensed surveyors to respective grids. Holes of all types routinely collar surveyed whist RC resource holes routinely downhole surveyed by various methods including gyro and EMS with average intervals ranging between 10-25m. • Croesus (RC, DD) Various local grids and AMG zone 51. RC, DD holes routinely collar surveyed and downhole surveyed using Electronic Multishot (EMS), GRYO, Eastman single shot or combination thereof at 10-15m average interval. • Hills (RC) Local grid used. • OBM (RC, DD) MGA94 Zone 51. Drill hole collar positions were picked up by a contract surveyor using RTKGPS subsequent to drilling. Drill-hole, downhole surveys are recorded every 30m using a reflex digital downhole camera for pre 2022 drilling. Some RC holes not surveyed if holes short and/or drilling an early stage exploration project. For all drilling from 2022 Drill hole collar positions were picked up by an OBM mining surveyor using RTKGPS subsequent to drilling. All downhole surveys from post 2022 drilling were taken every 10m by Gyro. • WMC (RC, DD) - Digital data provided by Cons Gold. (Wamex report a50226). Downhole surveys when performed were by undocumented

Criteria	JORC Code explanation	Commentary
		method with a 16m interval average
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• Data spacing is nominally 20m x 20m but down to circa 10m x 10m and grade control drilling at circa 5m x 5m. Deeper drilling is more widely spaced and down to approx. 30m x 30m • Drill hole spacing is adequate to establish geological and grade continuity for the Waihi deposit for the purpose of Mineral Resource and Ore Reserve estimation. • Composites of drill intercepts are length weighted, 1g/t lower cut-off, not top-cut, maximum 2m internal dilution
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Mineralised structures at Waihi are steep dipping and strike circa 320º to 350º Drilling is dominantly oriented to the east on a Waihi local grid which is rotated -14 degrees from the MGA north. Drilling is therefore oriented towards 76º on the MGA grid and to a lesser extent 256º, orthogonal to the mineralisation strike. Drill hole inclinations range from -50 to -90º. At Homeward bound some drill holes were drilled down the structure in an attempt to better define the then interpreted folding present. • It is unknown whether the orientation of sampling achieves unbiased sampling, though it is considered unlikely as the majority of holes have optimally intersected the mineralised lodes.
Sample security	• *The measures taken to ensure sample security.*	• Undocumented for most early operators. • Cons Gold – RC residues stored onsite • OBM – Samples are bagged into cable-tied polyweave bags and stored in bulka bags in a secure yard. Once submitted to the laboratories they are stored in cages within a secure fenced compound. Samples are tracked through the laboratory via their LIMS.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• OBM has reviewed historic digital data and compared it to hardcopy and digital (Wamex) records. Changes were made to the SQL database where necessary. • No audits of sampling techniques have been done.

Section 2 Reporting of Exploration Results – Riverina

(Criteria listed in the preceding Missouri & Sand King section also apply to this section.)

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td>Mineral tenement and land tenure status</td><td>• Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.
• The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</td><td>• All tenure pertaining to this report is listed below.
<table>
<tr><th>TENEMENT</th><th>HOLDER</th><th>EXPIRY DATE</th><th>AGREEMENTS</th></tr>
<tr><td>M30/256</td><td>CARNEGIE GOLD PTY LTD.</td><td>20/04/2038</td><td>FARM-IN AND JV BETWEEN DAVYSTON EXPLORATION PTY LTD (71%) AND CARNEGIE GOLD PTY LTD (29%) FOR ALL MINERALS OTHER THAN GOLD AND ITS BYPRODUCTS
DAVYSTON EXPLORATION PTY LTD HAS A CONSENT CAVEAT & A REGISTERED MORTGAGE AGAINST THE TENEMENT</td></tr>
</table></td></tr>
</table>

		<table><tr><td></td><td></td><td></td><td>SOUTH32 LTD HOLDS ROYALTY RIGHTS (portion of tenement only) PROVINCE RESOURCES LTD HOLDS ROYALTY RIGHTS (portion of tenement only) HAWKES POINT HOLDINGS L.P HAS A REGISTERED MORTGAGE AGAINST THE TENEMENT ANZ FIDUCIARY SERVICES PTY LTD HAS A REGISTERED MORTGAGE AGAINST THE TENEMENT</td></tr></table> • Carnegie Gold PTY LTD is a wholly owned subsidiary of OBM. • There are no known heritage or native title issues. • There are no known impediments to obtaining a licence to operate on this tenement area.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• Drilling, sampling and assay procedures and methods as stated in the database and confirmed from Wamex reports and hard copy records are considered acceptable and to industry standards of the time.
Geology	• *Deposit type, geological setting and style of mineralisation.*	• The geology of the Riverina area consists of an interlayered sequence of meta-basalts, meta-sediments and ultramafics, rarely cross-cut by narrow pegmatite dykes. The local stratigraphy strikes roughly N-S with primarily steep east to sub-vertical dips. The area has been affected by upper greenschist to lower amphibolite grade metamorphism with many minerals exhibiting strong preferred orientations. All rock units exhibit strain via zones of foliation, with strongly sheared zones more common in ultramafic lithologies. Contemporaneous strike faults and late stage thrust and wrench faults have dislocated the stratigraphy and hence, mineralisation. • Gold mineralisation is hosted by quartz-sulphide and quartz-Fe oxide veining primarily in the metabasalts. Metasediments and ultramafics may also contain gold mineralised quartz veining, although much less abundant. Gold mineralisation is also seen in silica-biotite-sulphide and silica-sericite-sulphide alteration zones in the metabasalts.

Drillhole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drillholes:*
	  ○ *easting and northing of the drillhole collar*
	  ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drillhole collar*
	  ○ *dip and azimuth of the hole*
	  ○ *down hole length and interception depth*
	  ○ *hole length.*
	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*
		• See list of drill intercepts.

Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Original assays are length weighted. Grades are not top cut. Lower cut off is nominally 1.0g/t. Due to the narrow nature of mineralisation a minimum sample length of 0.2m was accepted when calculating intercepts. Maximum 2m internal dilution. • Metal equivalents not reported.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drillhole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	• Intercept widths are down hole lengths. True widths are not reported given the varying orientation of drilling and mineralisation at each deposit/prospect mentioned in the report. • The geometry of the mineralisation at Riverina South is approx. N-S and sub vertical. Surface drilling is oriented perpendicular the strike of the mineralisation. UG drilling from drill cuddy with hole radiating in fans. Holes testing strike extremities are at lower angles to the ore lode and therefore not true widths, while those perpendicular to the lode can approximate true widths.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drillhole collar locations and appropriate sectional views.*	• See plans, cross-sections and long sections.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• The location of drillhole intersections is shown on the plans and 2D/3D diagrams and are coloured according to grade to provide context for the highlighted intercepts

Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• Riverina has no known reported metallurgical issues and is currently being successfully mined.
		• Results from previous processing have demonstrated that good gold recovery can be expected from conventional CIL processing methods.
		• Baseline metallurgical test work demonstrated the following gold recoveries:
		  ○ Oxide – 90%
		  ○ Transitional – 97%
		  ○ Fresh – 94.3%

Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).*	• Further GC drilling at Riverina underground will continue as the access into the mine is deepened. • Further resource definition drilling will be conducted from the surface, when beyond the reach of the underground drills, aimed and continued mineral resource growth and resource conversion.

	• *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	

Section 2 Reporting of Exploration Results – Sand King

(Criteria listed in the preceding Missouri & Sand King section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• Sand King deposit is on Tenement M24/960 held by Siberia Mining Corporation Pty Ltd, a wholly owned subsidiary of Ora Banda Mining. The tenement is in good standing. • .

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td></td><td>
<table>
<tr><th>TENEMENT</th><th>HOLDER</th><th>EXPIRY DATE</th><th>AGREEMENTS</th></tr>
<tr><td>M24/0960</td><td>SIBERIA MINING CORPORATION PTY LTD</td><td>1/12/2037</td><td>SIBERIA GRANTED GARDNER THE RIGHT TO EXPLORE FOR NICKEL AND COBALT MINERALS (portion of tenement only)

ROB MITCHELL AND HANK SHRERS (SURFACE ALLUVIAL RIGHTS TO 2M DEPTH) (portion of tenement only)

STONEHORSE ENERGY LIMITED HAVE RIGHTS TO EXPLORE FOR NICKEL AND ASSOCIATED MINERALS (portion of the tenement only)

RAMELIUS RESOURCES LTD HOLDS ROYALTY RIGHTS (portion of tenement only)

FARM-IN AND JV BETWEEN DAVYSTON EXPLORATION PTY LTD (71%) AND CARNEGIE GOLD PTY LTD (29%) FOR ALL MINERALS OTHER THAN GOLD AND ITS BYPRODUCTS

DAVYSTON EXPLORATION PTY LTD HAS A CONSENT CAVEAT & A REGISTERED MORTGAGE AGAINST THE TENEMENT

ANZ FIDUCIARY SERVICES PTY LTD HAS A REGISTERED MORTGAGE AGAINST THE TENEMENT</td></tr>
<tr><td>M24/39</td><td>CHARLES ROBERT GARDNER</td><td>15/01/2027</td><td>GARDNER GRANTED SIBERIA THE RIGHT TO EXPLORE FOR GOLD MINERALS (GOLD AND SILVER MINERALISATION IN ANY FORM)(entire tenement). IN RELATION TO THE “REDUCED AREA”, SIBERIA HAS CONTINUED EXCLUSIVE AND OVERRIDING RIGHTS TO CARRY OUT EXPLORATION AND MINING OPERATIONS.

WMC RESOURCES LTD HOLDS A CAVEAT AGAINST THE TENEMENT

CITY OF KALGOORLIE-BOULDER HOLDS AN ABSOLUTE CAVEAT AGAINST THE TENEMENT

SIBERIA HOLDS A CONSENT CAVEAT AGAINST THE TENEMENT</td></tr>
</table>

There are no known heritage issues
There are no known impediments to operating in the area.

</td></tr>
<tr><td>Exploration done by other parties</td><td>Acknowledgment and appraisal of exploration by other parties.</td><td>Drilling on the tenements was completed by numerous operators, but the majority of work was completed by WMC, Gilt Edged Mining, Siberia Mining Corporation, Monarch Gold and EGS. All work by these companies was to industry standards of the time.</td></tr>
<tr><td>Geology</td><td>Deposit type, geological setting and style of mineralisation.</td><td>Sand King is an orogenic lode style deposit hosted by mafic rocks, predominantly basalt.
Gold mineralisation at Sand King takes the form of stacked quartz-biotite-feldspar-sulphide shear lodes within the basalt. Widths vary from sub 1m to ~ 6m true width. Occasionally blow outs occur with >6m true width. Mineralised structures are NE-SW striking in the south and normally steeply dipping (~80 degrees) to the north-west while in the north-eastern end of the deposit most mineralisation is interpreted to strike E-W and dip steeply to the north (~80 degrees)</td></tr>
<tr><td>Drillhole Information</td><td>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drillholes:
easting and northing of the drillhole collar
elevation or RL (Reduced Level – elevation above sea level in metres) of the drillhole collar</td><td>See Significant Intercepts in document
The significant intercept table provides details of drillholes with intercepts of >= 1 gram metres. In cases where drilling has intercepted a lode position with grades below this value, NSI (no significant intercept) is listed. This provides context to the number of holes in the project area with significant gold intercepts versus the number of holes with lesser or no significant intercepts.
Widths reported in the Significant Intercepts table are all down hole lengths.</td></tr>
</table>

Criteria	JORC Code explanation	Commentary
	○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Original assays are length weighted. Grades are not top cut. Lower cut off grade is nominally 1.0g/t. Maximum 2m internal dilution and minimum width of 0.2m. • No metal equivalents reported.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drillhole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	• Drilling is predominantly angled at -60º to the south, optimally intersecting the steep north dipping mineralisation. This drill orientation does not intersect all lodes at optimal angles and as such some drill intercepts are longer than true widths. • All intercept widths reported are down hole lengths. The geometry of mineralisation is known for the Sand King deposit. However, no attempt has been made to report true widths. • Some drill programs required shallow angle (~30º) diamond drilling to hit specific targets within the constraints of existing mining infrastructure (existing pit and dumps). • UG drilling from drill cuddys with hole radiating in fans. Holes testing strike extremities are at lower angles to the ore lode and therefore not true widths, while those perpendicular to the lode can approximate true widths.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drillhole collar locations and appropriate sectional views.*	• See plans and sections.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• All drill intercepts from recent drilling are reported. • Results reported include both low and high gram metre (g/t x down hole length) values.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• Metallurgical, geotechnical, environmental and engineering work has been completed for Sand King deposit and is included in the ORE.
Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).*	• Additional deep and lateral drilling to grow the UG resource. • Statutory approvals for UG mining are in place

Criteria	JORC Code explanation	Commentary
	• *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	

Section 2 Reporting of Exploration Results – Round Dam

(Criteria listed in the preceding Missouri & Sand King section also apply to this section.)

<table>
<tr><th>Criteria</th><th>JORC Code Explanation</th><th>Commentary</th></tr>
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• The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</td><td>• All tenure pertaining to this report is listed below:
<table><tr><th>TENEMENT</th><th>HOLDER</th><th>Expiry Date</th><th>AGREEMENTS</th></tr><tr><td>M30/255</td><td>CARNEGIE GOLD PTY LTD.</td><td>10/01/2038</td><td>FARM-IN AND JV BETWEEN DAVYSTON EXPLORATION PTY LTD (71%) AND CARNEGIE GOLD PTY LTD (29%) FOR ALL MINERALS OTHER THAN GOLD AND ITS BYPRODUCTS

DAVYSTON EXPLORATION PTY LTD HAS A CONSENT CAVEAT & A REGISTERED MORTGAGE AGAINST THE TENEMENT
HAWKES POINT HOLDINGS L.P HAS A REGISTERED MORTGAGE AGAINST THE TENEMENT
ANZ FIDUCIARY SERVICES PTY LTD HAS A REGISTERED MORTGAGE AGAINST THE TENEMENT</td></tr></table>• Carnegie Gold PTY LTD is a wholly owned subsidiary of OBM.
• There are no known heritage or native title issues.
• There are no known impediments to obtaining a licence to operate in the area.</td></tr>
<tr><td>Exploration done by other parties</td><td>• Acknowledgment and appraisal of exploration by other parties.</td><td>• Drilling, sampling and assay procedures and methods as stated in the database and confirmed from Wamex reports and hard copy records are considered acceptable and to industry standards of the time. There is sufficient understanding of drilling, sampling and assay methodologies for the majority of drilling in the Round Dam area. The company is confident that previous operators completed work to standards considered acceptable for the time. As part of each resource upgrade, OBM will commit to additional drilling to</td></tr>
</table>

Criteria	JORC Code Explanation	Commentary
		confirm the style, widths and tenor of mineralisation at each deposit.

Geology	• *Deposit type, geological setting and style of mineralisation.*	• **Regional Geology** - Rocks of the Coolgardie domain (Kalgoorlie Terrane) are prevalent in the Davyhurst area. Rocks of the Coolgardie Domain are not well exposed at Davyhurst and the distribution of rock types suggests that it is mainly represented by the upper part of the stratigraphic sequence, namely basalts, felsic volcanics and sedimentary rocks. The abundant ultramafic-mafic sills of the Ora Banda Domain do not occur in the Coolgardie Domain. Granitoids in the Davyhurst Project area can be classified by magnetic signature into three types: low, medium and high magnetic response. Binns et al. (1976) distinguished 'static style' and 'dynamic style' regional metamorphism. Static style areas generally occupy the central, low-strain part of the greenstone regions away from the granitoids and typically have lower metamorphic grades (prehnite–pumpellyite to upper greenschist facies). Strain is concentrated in narrow zones so that textures are well preserved in more massive and competent rocks. Dynamic-style areas of greenstone have higher metamorphic grades (upper greenschist to upper amphibolite facies) and are characterized by more pervasive foliation, particularly along the contacts with large granitoid terrains. There appears to be two major controls on mineralisation in the Davyhurst area. Both mineralisation styles rely on mineralisation taking place during reactivation of earlier ductile shear zones. In the case of the Lights of Israel group of deposits, the early shears are moderately to gently west dipping, whereas in the Federal Flag – Lady Eileen group of deposits, the early shear is steeply west dipping. In the northern portion of the Davyhurst tenements most gold mineralisation is aligned in planar corridors that have N- to NW-trends. The overall dip of the mineralised corridors is mostly steep (>75º) E- or W-dipping with moderate to steep (~60º) and shallow-dipping (~15º) ore zones at the Federal Flag and Lady Gladys deposits, respectively. Within these planar corridors of mineralisation linear trends to gold distribution are mostly shallowly plunging. Internal variations within the corridors at individual deposits are common and discussed later. Mineralisation at the Lights of Israel and Makai deposits differs from the other examined deposits in that mineralisation has a linear form that plunges moderately (~20º) to the NNW.
		• **Local Geology**
		  • EAST – Interbedded volcaniclastic sediments / tuffs
		  • CENTRAL – mafic / ultramafic sequence consisting of:
		  • Eastern Ultramafic unit (chlorite tremolite schist), sometimes contains internally a wedge of high-Mg pillow basalt (chlorite schist)
		  • Western Basalt unit, this basalt weathers much deeper than the UM
		  • Potentially a thin (~5m) unit of interflow sediment lies along the contact of the basalt and UM
		  • WEST – Interbedded shales and volcaniclastic sediments
		• **Mineralisation**
		Four principal gold lodes identified at Round Dam:
		Basalt Lode
		  • Gold lode wholly within the basalt
		Basalt / UM Contact Lode
		  • Highly altered basalt immediately in hanging wall to ultramafic / basalt contact. Strong banded biotite-silica-sulphide (pyrrhotite) alteration + py/cpy. Possible narrow interflow sediment on this contact
		UM Quartz Vein Lode(s)
		  • Highly deformed early quartz veining within ultramafic unit acts as preferential host for gold mineralisation due to rheological contract. Visible gold associated with pyrrhotite + py/cpy/apy

Criteria	JORC Code Explanation	Commentary
		• Main lode is consistent thick zone of quartz veining approximately 40m east of UM/Mb contact. Minor other lodes come and go along strike • Plunge of mineralisation defined by plunge of folded / boudined quartz veins Eastern Lode • High-grade lode in eastern portion of the mafic/ultramafic sequence. No available access to map this lode and define its controls / alteration – diamond drilling required
• ***Drill hole Information***	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	• See list of drill intercepts. • Widths reported in the Significant Intercepts table are all down hole lengths.
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Original assays are length weighted. Grades are not top cut. Intercepts are reported at a Lower cut off of 0.5g/t with a secondary cut off of 1.0g/t **or** a Lower cut off of 1.0g/t with a secondary cut off of 10.0g/t. Maximum 4m internal dilution. • No metal equivalents reported
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	• Intercept widths are down hole lengths. True widths are not reported. • The geometry of the mineralisation on the Round Dam Trend is approx. 350° and 60° to 70° West dipping. Drilling is oriented perpendicular to the strike of the mineralisation.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• See plans and sections.

Criteria	JORC Code Explanation	Commentary
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• Results from all holes in the current drilling have been reported. • Results reported include both low and high gram metre (g/t x down hole length) values. • The significant intercept table provides details of drill hole intercepts shown on diagrams. There is no lower cut-off grade, the holes listed include those with NSI (no significant intercept). Holes in the significant intercept table are shown on diagrams coloured according to gram metre grade bins. This provides spatial context to the number of holes in the project area with significant gold intercepts versus the number of holes with lesser or no significant intercepts
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• Preliminary Metallurgical leach tests have demonstrated gold recoveries of >95% using standard CIL processing • Numerous deposits on the Round Dam Trend were previously mined and processed at Davyhurst plant with no known metallurgical issues. • Geotechnical work is ongoing. • Waste rock characterisation is progressing.
Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Exploration and Resources Development drilling is continuing • Statutory approvals for mining in progress.

Section 2 Reporting of Exploration Results – Waihi

(Criteria listed in the preceding Golden Eagle section also apply to this section.)

Criteria	JORC Code Explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• All tenure pertaining to this report is listed below

TENEMENT	HOLDER	Expiry Date	AGREEMENTS
M30/255	CARNEGIE GOLD PTY LTD.	10/01/2038	FARM-IN AND JV BETWEEN DAVYSTON EXPLORATION PTY LTD (71%) AND CARNEGIE GOLD PTY LTD (29%) FOR ALL MINERALS OTHER THAN GOLD AND ITS BYPRODUCTS DAVYSTON EXPLORATION PTY LTD HAS A CONSENT CAVEAT & A REGISTERED MORTGAGE AGAINST THE TENEMENT

Criteria	JORC Code Explanation	Commentary
		<table><tr><td></td><td></td><td></td><td>HAWKES POINT HOLDINGS L.P HAS A REGISTERED MORTGAGE AGAINST THE TENEMENT ANZ FIDUCIARY SERVICES PTY LTD HAS A REGISTERED MORTGAGE AGAINST THE TENEMENT</td></tr></table> • Carnegie Gold PTY LTD is a wholly owned subsidiary of OBM. • There are no known heritage or native title issues. • There are no known impediments to obtaining a licence to operate in the area.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• Modern exploration commenced at the Davyhurst sites in the 1980s. Three companies, Jones Mining, Western Mining Corporation (WMC) and Hill Minerals pegged claims surrounding the historic Davyhurst sites. In 1986, WMC established a 300,000 tonne per annum carbon-in-pulp (CIP) treatment plant at Davyhurst and commenced open pit mining at Golden Eagle and Waihi. In 1988 WMC's and Jones Mining's assets were acquired by Consolidated Exploration Ltd. Consolidated Exploration then developed open cut mines at Great Ophir, Lady Eileen, Lady Eileen South and Homeward Bound. At about the same time Aberfoyle Resources / Hill Minerals commenced open-pit mining at the Lights of Israel Deposit and trucked the ore 80 km to the Bardoc processing plant. During 1995/96 Consolidated Exploration Ltd. restructured as Consolidated Gold NL (CGNL) and commenced tenement acquisition and exploration activities in the area. This resulted in the consolidation of holdings in the district. In December 1996 CGNL acquired the assets of Aberfoyle Resources in the area, including the Bardoc Processing plant, in an equity transaction. The Bardoc plant was relocated to the Davyhurst site and upgraded to 1.2 Mt/y. In October 1998 Davyhurst Project Pty Ltd (DPPL), a subsidiary of NM Rothschild and Sons (Australia), acquired the project. In 2000, Croesus Mining NL ("Croesus") acquired the Davyhurst Project and continued operations until 2005. In January 2006, Monarch Gold Mining Company Limited (Monarch) acquired Davyhurst and operated the project until 2008. • Drilling, sampling and assay procedures and methods as stated in the database and confirmed from Wamex reports and hard copy records are considered acceptable and to industry standards of the time. There is sufficient understanding of drilling, sampling and assay methodologies for the majority of drilling in the Waihi area. The company is confident that previous operators completed work to standards considered acceptable for the time. As part of each resource upgrade, OBM is committed to additional drilling to confirm the style, widths and tenor of mineralisation at each deposit.
Geology	• *Deposit type, geological setting and style of mineralisation.*	• Regional Geology - Waihi and Golden Pole are the northern-most exploited gold deposits in a chain of deposits which stretch at least 14 km to the south along the Round Dam trend. Waihi and Golden Pole are located within the Coolgardie Domain of the Kalgoorlie Terrane, Eastern Goldfields Province, Western Australia. The deposit is hosted within Archaean mafic to ultramafic volcanic rocks of the Hampton Hill Formation, comprising a fractionated ultramafic to mafic volcanic sequence metamorphosed from lower to upper greenschist facies. • Local Geology - Lithogeochemistry, particularly Cr and Zr signatures obtained from pXRF provides a reliable method for differentiating volcanic units and confirming stratigraphic position where visual logging alone is insufficient or difficult due to metamorphic and hydrothermal alteration. Elements such as Cr, Ni, Ti, and Zr are especially effective in discriminating ultramafic flows, komatiitic basalts, mixed chrome basalts and more evolved tholeiitic units. All units are intruded by late-stage pegmatite dykes. Lithologies in the area strike just west of N-S, and dip steeply to the west (~70°) along Waihi Central and Waihi North and to the east at Waihi South and Homeward Bound. Structurally Waihi has undergone a multitude of shortening events with rock fabrics displaying crenulations and a pervasive west dipping foliation. • Mineralisation - Gold is primarily concentrated within biotite–quartz–sulphide assemblages developed during high-strain D4a–D4b transpressional shearing. Early D2 quartz veins occur throughout the sequence and, depending on local strain, are either preserved undeformed or, within high-strain domains, are folded, boudinaged, and locally transposed into foliation. In mineralised zones, these veins commonly exhibit smoky, isoclinal folding. Sulphides are dominated by pyrrhotite with minor pyrite and chalcopyrite and occur both disseminated within biotite schist and concentrated along vein selvages, with gold spatially associated. A later CO_2-rich fluid event produced carbonate veining and discontinuous calc-silicate assemblages, with calcite partially to completely replaced by diopside; while some of these veins contain gold, diopside development alone is not predictive, and gold is more closely controlled by structural focusing and high-strain zones. Retrograde alteration, comprising Mg-chlorite, sericite, carbonate, and minor epidote, variably overprints all lithologies along microfractures, shear bands, and vein margins, reflecting late-stage fluid ingress.

Criteria	JORC Code Explanation	Commentary

Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*
	  ○ *easting and northing of the drill hole collar*
	  ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar*
	  ○ *dip and azimuth of the hole*
	  ○ *down hole length and interception depth*
	  ○ *hole length.*
	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*
		• Individual drill intercepts are previously reported. For previous announcements relating to Waihi please refer to ASX announcement dated 22 February 2017, 29 July 2019, 14 October 2019, 6 November 2019, 22 November 2019, 24 December 2019, 21 January 2020, 10 June 2025, 4 September 2025, 15 January 2026 and 21 April 2026.
		• Any widths reported in a Significant Intercepts table are all down hole lengths.

Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Original assays are length weighted. For reporting exploration results grades are not top cut. Lower cut off is nominally 0.5g/t. Maximum 2m internal dilution. For reporting Resource Development results, lower cut-off is nominally 1g/t. • No metal equivalents reported
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	• Intercept widths are down hole lengths. True widths are not reported given the varying orientation of drilling and mineralisation at each deposit/prospect mentioned in the report.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• See plans and sections provided within this announcement.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be*	• Results reported include both low and high gram metre (g/t x down hole length) values. • The significant intercept table (previously reported – see references in Section on Drill hole Information) provides details of drill hole intercepts shown on diagrams. Holes listed include those with NSI (no significant intercept). Holes in the significant intercept table

Criteria	JORC Code Explanation	Commentary
	practiced to avoid misleading reporting of Exploration Results.	are shown on diagrams coloured according to gram metre grade bins. This provides spatial context to the number of holes in the project area with significant gold intercepts versus the number of holes with lesser or no significant intercepts
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• Metallurgical and geotechnical work has been completed for numerous previously mined deposits, including Waihi. • Waihi deposit was previously mined and processed at Davyhurst plant with no known metallurgical issues. • Ongoing geological/ structural evaluation to determine the controls on mineralisation. • Comminution and extractive Metallurgical testwork is ongoing. • Waste characterization studies are in progress. • Geotechnical holes have been drilled for open pit assessment. • External and internal underground Geotechnical Studies have been completed.
Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Additional drilling to convert inferred material to indicated. • Local exploration targeting extensions to the south and east of Waihi are proposed.

Section 3 Estimation and Reporting of Mineral Resources – Riverina

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	• Data from EGL and early OBM drilling captured into Field Marshall logging software. More recent drilling capture in Geobank Mobile. Data sent from site and imported into SQL database via DBMS. Validation checks in SQL database ensure data integrity is not compromised. • The data is verified by company geologists before being sent to the DBA for validation or passing Geobank Software validation protocols. • Historic data has been verified by checking historical reports on the project. • The Competent Person has undertaken a number of validation checks on the database, using Micromine software which include, but are not limited to, checks for overlapping intervals, checks for missing data/records, visual checks on drillhole locations and traces to identify any possible survey issues. No major issues were detected.

Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*
	• *If no site visits have been undertaken indicate why this is the case.*
		• Numerous site visits completed to:
		  ○ View and map geology in existing open pit
		  ○ View and manage drilling operations
		  ○ View and log drill core
		  ○ View Underground exposure

Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.*	• Mineralised structures are roughly N-S striking, sub-vertical to steeply east dipping. The main lodes have been previously mined and are sub-vertical. Late stage south dipping thrust structures are mapped in the pit and underground workings and would extend east towards the Murchison and Reggie lodes. Minor sinistral offsets of up to 5m are noted in underground workings and are observed as offsets of mineralised drill intercepts. Three late structures have been modelled with offsets, two south dipping pegmatite filled thrusts and a pegmatite filled back thrust known as "The Slide". An additional thrust mapped in the north pit, usually gouge filled, has been modelled without offsetting mineralisation, though in reality minor offsets will occur. An additional lower thrust has been modelled from drill core

Criteria	JORC Code explanation	Commentary
	• *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	observations, again without offsetting mineralisation. An increase in drill density will enable potential offsets to be better defined. • Structural data from OBM drilling was used to guide the orientation of mineralised lodes where possible. • Inspection of core and ore shows the mineralisation to be associated with silica sericite alteration and quartz-carbonate veining. Resource interpretations are guided by presence and intensity of veining and/or alteration noted in logging. The two dominant mineralised structures, ME1 and MW1 were modelled as a central vein, surrounded by a lower grade shear zone. • Geological continuity of N-S mineralised structures are well defined, although sometimes terminate abruptly, possibly due to the minor offsets caused by the E-W structures and/or structures entering pods of sediment/ultramafic which are poorer hosts for gold mineralisation. The main lodes at Riverina are geologically continuous over 1.6km and limited only by drilling depth. • Mineralisation is also locally stoped by intruding pegmatite dykes along late structures, the location of which are well understood.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The main lodes at Riverina are geologically continuous over 1.6km in a N-S direction and defined to a depth of 1000m below surface. • The central Murchison and East (Reggie) lodes exhibit similar dimensions

Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.*
	• *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.*
	• *The assumptions made regarding recovery of by-products.*
	• *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).*
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*
	• *Any assumptions behind modelling of selective mining units.*
	• *Any assumptions about correlation between variables.*
	• *Description of how the geological interpretation was used to control the resource estimates.*
	• *Discussion of basis for using or not using grade cutting or capping.*
	• *The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.*
		• Assay results were composited to 0.3m, starting from the point where drillholes enter the domains. Residual assay intervals were distributed over the interval. The narrow, mineralised domains and minimum sample width of 0.3m led to the adoption of the 0.3m composite.
		• Prior to 2026, Riverina MRE's used a 2-dimensional estimation technique where an 'accumulation' variable (gram-metres) and lode width were estimated and the grade back-calculated from the estimated 'accumulation' and width variables. The current MRE uses a traditional estimation of gold grade into a 3-dimensional block model.
		• Spatial continuity, using Supervisor™ software, of composite gold grades was evaluated using variography and the parameters defined were applied in the estimation process. Search neighbourhoods were defined using Kriging Neighbourhood Analysis implemented in Supervisor™. Top cuts were applied to the composite gold grades on a domain basis in order to reduce the influence of sometimes extreme grades. Control over spread of high grades was further implemented for some lodes by using distance limiting and grade thresholds. Both top-cutting and distance limiting grade thresholds were implemented to control metal risk.
		• Estimation of gold grades was by ordinary kriging using Leapfrog™ software into a parent block size of 6.4mE x 10mN x 10mRL. The domain wireframes were used to constrain lode volumes using suitable sub-celling. A three-pass search strategy was implemented with successive passes having fewer minimum and maximum samples. Search anisotropy mirrored the variogram anisotropy. Locally variable anisotropy was adopted for the estimation to re-orient the search and variogram according to local lode undulations. The outcome of this should be improved local estimates.
		• The model has been depleted to account for existing mining, both underground up to 1 April 2026 and previous open pit.
		• No estimation of deleterious elements was carried out. Only Au was interpolated into the block model.
		• Previous resource estimates have been completed in 2020, 2021 and 2023, 2024, 2025 & 2026.
		• No assumptions have been made regarding recovery of by-products.
		• Selective mining units were not modelled in the Mineral Resource.
		• No assumptions have been made regarding correlation between variables
		• The validation was carried out by three methods:
		  ○ Visual comparison of long section block grades with nearby drill assay results.
		  ○ Statistical comparison of estimated grades and composite grades on a domain by domain basis.
		  ○ Trend analysis of estimated block model grades versus composite grades on north and RL swaths

Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages and grades were estimated on a dry in situ basis. No moisture values were reviewed.

Criteria	JORC Code explanation	Commentary
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The Mineral Resources have been reported at a diluted cut-off of 0.8g/t Au inside simulated Auto Stope Designer (ASD) shapes of 10m x 10m with a minimum width of 1.6m.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• Reasonable prospects for eventual economic extraction for the Riverina underground Resource was confirmed by applying ASD solids with dimensions of 10mN x 10mRL, a minimum width of 1.6m and a diluted cut-off grade of 0.8g/t. Individual ASD solids were assessed and removed if above the top of fresh DTM surface and if above the A$2400 optimised pit shell from within which the Riverina open pit resources are reported.

Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	• Riverina has no known reported metallurgical issues.
		• Results from previous processing have demonstrated that good gold recovery can be expected from conventional CIL processing methods.
		• Recent baseline metallurgical test work demonstrated the following gold recoveries:
		  ○ Oxide – 90%
		  ○ Transitional – 97%
		  ○ Fresh – 94.3%

Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• Riverina Underground is currently being mined and all approvals are currently in place. • All environmental impacts are accounted for in the current approvals
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.*	• Bulk density determinations were derived from 5684 measurements (immersion method) made on core samples drilled by OBM/EGS. • Historic bulk densities for fresh basalt collected from underground in 1988 were analysed. The mean fresh rock density from recent drilling compared closely with the mean density of underground samples. • Bulk density values used in the underground resource were applied based on several domains, including ore/waste, weathering and lithology. • It is assumed there are minimal void spaces in the rocks within the Riverina deposit.

Criteria	JORC Code explanation	Commentary
	• *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	

Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.*
	• *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).*
	• *Whether the result appropriately reflects the Competent Person's view of the deposit.*
		Mineral Resources were classified in accordance with the Australasian Code for the Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC, 2012). The classification takes account of confidence in the geological interpretation, sample density and assay QAQC.
		
		Underground - Wireframe solids were constructed to encompass areas considered to adequately fulfil the requirement to be classified as either, measured, indicated or inferred:
		
		• Measured
		  ○ Near surface areas defined by close spaced RC grade control drilling
		  ○ UG areas with development above and below and/or very closed (<5m) spaced drilling
		• Indicated – Areas with:
		  ○ drill spacing in long section of approximately 30mN x 30mRL where there is reasonable confidence in the geological interpretation and grade continuity.
		  ○ reasonable estimation quality as defined by the conditional bias slope > 0.5
		• Inferred – Areas with:
		  ○ drill spacing in long section in excess of 30mN x 30mRL and where grade continuity is poorer as defined by a lower sample density, even though geological continuity may be apparent.
		  ○ poorer estimation quality as defined by the conditional bias slope > 0.2 and < 0.5
		
		• The input data is comprehensive and of sufficient quality for use in the MRE's. Significant recent drilling, covering the entire deposit, has confirmed the location and tenor of many historic drill-holes. Assay QAQC is of sufficient quality for the assays to be used in the MRE. There is sufficient understanding of the geology to support the current interpretation in terms of geological continuity.
		• The Mineral Resource estimates appropriately reflects the view of the Competent Person.

Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• The Underground MRE has been internally peer reviewed.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence*	• The Riverina Mineral Resource estimate is reported with a reasonable degree of confidence. The data quality is good and the drillholes from recent drilling have detailed logs produced by qualified geologists. Historic logging has been reviewed. • The Mineral Resource statements relate to global estimates of tonnes and grade. Confidence in the estimate allows reasonable quantification of global metal content. The interpretation is considered globally robust but at a local scale, variations to ore geometry and grade could be expected. • All Measured and Indicated resources are relevant to economic evaluation. • The deposit is currently being mined – Underground. • Production data from current mining is used to calibrate MRE's

Criteria	JORC Code explanation	Commentary
	of the estimate should be compared with production data, where available.	

Section 3 Estimation and Reporting of Mineral Resources – Sand King

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary

Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*
	• *Data validation procedures used.*
		• Data from EGS/OBM drilling captured into Field Marshall or Geobank Mobile logging software. Data sent to Perth for import into SQL database via DBMS. Validation checks in SQL database ensure data integrity is not compromised.
		• Data for use in resource estimation derived directly from SQL via queries (views) and a data warehouse database
		• Data validation included:
		  ○ review of historic digital data versus original hardcopy records
		  ○ Inspection of mineralised intervals in historic core

Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*
	• *If no site visits have been undertaken indicate why this is the case.*
		• Numerous site visits completed to:
		  ○ View and log historic core
		  ○ Map the Sand King pit
		  ○ Log recent drill core
		  ○ View underground exposures

Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	• Sand King pit mapped by structural geological consultants (Model Earth Pty. LTD) Additional mapping completed by OBM geology team. Current pit mapping identifies early 010 and 330 ductile shears and 060 and 090 (semi) steep north dipping brittle extension veins. Extension veins form the bulk of the mineralisation. This structural architecture has been verified during underground mining. • An extensive relog program of historic diamond core was completed to provide consistency with 2016 (EGS) and 2020 (OBM) geological logging. • Inspection of core and pit ore shows the mineralisation to be associated with quartz-carbonate veining and biotite-sulphide alteration either side of the veining. Resource interpretations guided by presence and intensity of veining and/or biotite noted in logging. • Geological continuity of extension structures is well defined, although not strike extensive and can terminate abruptly. Quartz tension veins oriented 090°-100° form stacked lodes and the intersection of these with the shear-lodes and 060° lodes is the most likely control for high grade shoots and plunge steeply towards the N-NNE. Mineralising structures post date locally intruding aplite dykes and these can be (weakly) mineralised.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The Sand King deposit extends for over 800m in NE-SW direction and approximately 300m in a SE-NW direction. The Resource extends for ~400m below the surface RL of 420m AHD. • A mine grid is employed at Sand King. This has a 60º rotation so that 060º (MGA) is 000º (Mine Grid). 4000m is added to the MGA RL.
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* • *The availability of check estimates, previous*	• Interpolation was done using Ordinary Kriging (OK) estimation method. • 1m composite samples coded to the mineralised domains were used as inputs to estimation. Only RC (including RC grade control) and diamond drilling samples were used for estimation. • OK was used to estimate gold grades into a 3-dimensional block model. Estimation parameters were derived from modelled semi-variograms. Micromine™ software was used for the OK estimation. • Grade capping was applied on a domain by domain basis due to the usually positively skewed grade populations. High grade cuts up to 60g/t were applied to 1m composite data based on analysis of individual domains. • The parent block dimensions (Mine Grid) for OK estimates were 4m EW by 10m NS by 10m vertical. Sub-cells of 0.5m by 1m by 1m were

Criteria	JORC Code explanation	Commentary

	estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.
	• *The assumptions made regarding recovery of by-products.*
	• *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).*
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*
	• *Any assumptions behind modelling of selective mining units.*
	• *Any assumptions about correlation between variables.*
	• *Description of how the geological interpretation was used to control the resource estimates.*
	• *Discussion of basis for using or not using grade cutting or capping.*
	• *The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available.*
		applied to the OK model. Drillhole spacing in better drilled areas is approximately 20m between section and 20m along section. The parent block size is approx. 50% of data spacing.
		• An orientated ellipsoid search was used to select data and was based on parameters derived from the variography defined using Supervisor™ software.
		• Estimation completed in 3 runs each with less restrictive search, and minimum sample parameters. The initial interpolation pass was used with a maximum range equal to the range of the principal direction of the modelled semi variograms. Maximum number of samples was 20, minimum was 6. Range increased progressively and number of samples required was reduced for each subsequent run.
		• No estimation of deleterious elements was carried out. Only Au was interpolated into the block model.
		• Previous OK resource estimates have been completed in 2017, 2020 2021 and 2022 all tailored for Open Pit MRE's. The 2024 MRE was used to estimate UG reserves.
		• No assumptions have been made regarding recovery of by-products.
		• No assumptions have been made with respect to modelling of selective mining units.
		• Only Au was estimated so correlation analysis was not possible.
		• The deposit mineralisation was constrained by wireframes constructed using an approx. 1 g/t Au cut-off grade (based on inflection point in log probability plot of raw assays) in association with logged geology, particularly the presence of quartz veining and biotite-sulphide alteration. Ore lode continuity is preserved reasonably well at the relatively high interpretation cut-off grade. The wireframes were applied as hard boundaries in the estimate.
		• The validation was carried out by three methods:
		  ○ Visual comparison of block grades with nearby drill assay results on a section by section basis.
		  ○ Comparison of estimated grades and composite grades on a domain by domain basis.
		  ○ Trend analysis of estimated block model grades versus composite grades.

Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages and grades were estimated on a dry in situ basis. No moisture values were reviewed.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The Underground Mineral Resource has been reported at a diluted 0.9 g/t Au cut-off from within Mine Stope Optimiser shapes (MSO) with 10mN x 10mRL dimensions and minimum 1.6m width. All fresh material above cut-off grade within MSO shapes below 350RL are included in the report.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• Reasonable prospects for eventual economic extraction for the Sand King underground Resource was confirmed by applying a Mine Stope Optimiser (MSO) with dimensions of 10mN x 10mRL, a minimum width of 1.6m and a cut-off grade of 0.8 g/t. Costs applied to the MSO process approximate current OBM mining costs and a gold price of A$4000 was used.
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical*	• Sand King deposit is currently being mined with underground methods. • Metallurgical test-work was undertaken in 2019/2020 and again in 2023/2024 as part of mining studies. • Gold recovery adopted for the underground mine is 87% (Fresh)

Criteria	JORC Code explanation	Commentary
	assumptions made.	
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• The previous mining operations included the development of waste dumps and tailings at the site. Waste rock from underground is used to cap historic tailings. • The area is not located in an environmentally sensitive area and all environmental approvals are in place
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	• 4069 density measurements (water immersion method) were taken from ore and waste material derived from older and recent OBM drilling. Bulk density values used in the resource were 1.5t/m3, 2.43t/m3 and 2.81t/m3 for oxide, transitional and fresh mineralisation respectively. Densities of 1.57t/m3, 2.61t/m3 and 3.0t/m3 for oxide, transitional and fresh waste were assigned. • A fresh rock ore density of 2.88 g/cm^3 was determined by Oretest laboratory on a bulk ore sample in 1998. • These bulk density estimates are similar to values determined for comparable basalt hosted gold deposits, and in particular Missouri deposit 600m to the south.

Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.*
	• *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).*
	• *Whether the result appropriately reflects the Competent Person's view of the deposit.*
		• Mineral Resources were classified in accordance with the Australasian Code for the Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC, 2012). The Mineral Resource was classified as Indicated and Inferred Mineral Resource on the basis of data quality, sample spacing, and lode continuity.
		• The Indicated portion of the Mineral Resource was defined where:
		  ○ Good support from drilling, averaging a nominal 40mN x 40mE.
		  ○ Areas where the estimation quality is reasonable mainly assessing kriging slope.
		• The remaining portions of the deposit were classified as Inferred Mineral Resource where:
		  ○ Data support is poorer with drilling typically greater than 40m x 40m.
		  ○ Areas where the estimation quality is poorer mainly assessing kriging slope.
		• The definition of mineralised zones is based on sound geological understanding of the controls on mineralisation. This is largely due to recent detailed pit mapping and exposure in underground workings which has produced a robust model of mineralised domains.
		• Inferred resources are typically at the periphery of mineralised domains and at depth where drill density and therefore confidence is generally lower.
		• The Mineral Resource estimate appropriately reflects the view of the Competent Person.

Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• The Waihi MRE has been internally peer reviewed
Discussion of relative	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure*	• The Sand King Mineral Resource estimate is reported with a reasonable degree of confidence. The data quality is good and the drillholes from recent drilling by EGS/OBM have detailed logs produced by qualified geologists. Historic logging has been reviewed. • Confidence in the estimate allows reasonable quantification of global metal content. The interpretation is considered globally robust but

Criteria	JORC Code explanation	Commentary
accuracy/ confidence	*deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	at a local scale, variations to ore geometry and/or grade could be expected. • All Measured and Indicated resources are relevant to economic evaluation. • The deposit is currently being mined. • Historical production records are available for the deposit.

Operator	Period	Tonnes Mined	Head Grade	Recovered Grade	Recovery	Ounces Produced
WMC	1980 - 1986	321,853	5.2	4.77	0.92	49,388
	1986 - 1987	Production Suspended				
	1987 - 1991	425,202	3.11	2.85	0.91	38,907
	Total Production	**747,055**	**4.01**	**3.68**	**0.92**	**88,295**
Monarch Gold	2007/2008	48,073		2.27		3,478
EGS*	2018	118,400		1.12		4,233
OBM	2023 - 2024	122,002	1.97			7,710

* Includes Laterite and Low-Grade Stockpile

Section 3 Estimation and Reporting of Mineral Resources – Round Dam

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	• Data from EGL/OBM drilling captured into Field Marshall or Geobank Mobile logging software. Data sent from site and imported into SQL database via DBMS. Validation checks in SQL database are carried out to ensure data integrity is not compromised. • The data is verified by company geologists before being sent to the DBA for validation or passing Geobank Software validation protocols • A drill hole database validation report was completed on the historical and recent drilling. This included collar location, downhole survey confidence and assay reviews. • The Competent Person has undertaken a number of validation checks on the database, using Leapfrog and Micromine software which include, but are not limited to, checks for overlapping intervals, checks for missing data/records, visual checks on drillhole locations and traces to identify any possible survey issues. No major issues were detected.

Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*
	• *If no site visits have been undertaken indicate why this is the case.*
		• Numerous site visits have been completed by the Competent Person with the following objectives:
		  ○ View geology in existing open pit
		  ○ View and log drill core

Criteria	JORC Code explanation	Commentary
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	• Lodes were generally interpreted on E-W sections and flitches using LeapfrogTM software. Round Dam mineralisation is generally 60-70° west dipping, 350° striking parallel lodes. The mineralisation follows along the contacts of the Ultramafic in the HW and FW as well as internally in the Ultramafic. Mineralisation in the HW mafic and FW sediments is present but not well constrained or defined. • Late stage E-W structures have been mapped and may offset the mineralised lodes slightly. These structures have also been exploited by thin pegmatite dykes. • Gold mineralization along The Round Dam Trend is associated with shear folding and shear structures producing boudinage quartz veins. The main high-grade shoot or plunge of mineralization ranges from -20 to -35 degrees to the North. This is matched with the measured fold hinges, lineations and boudinage quartz veins in both diamond drill core and from mapping within the historic open pits of Federal Flag and Walhalla. • The proximity to the Zulieka shear likely had a great impact on the amount of simple shearing that occurred along the Round Dam Trend. We can observe this in the shear jog at Walhalla North, with approximately 100m of West – East offset of the lithology and lodes. Resulting in the high-grade shoots forming on either side of the jog. • Inspection of core, RC chips and pit exposures shows the mineralisation to be associated with biotite and silica alteration and quartz-carbonate veining. • Geological continuity of mineralised strictures are well defined, although sometimes terminate abruptly, possibly due to the minor offsets caused by the E-W structures. The Lynx and Grizzly lodes at Round Dam are geologically continuous over 8 km. Grade continuity is less extensive but well defined at a low cut-off grade (0.3g/t)
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	• The Lynx and Grizzly lodes at Round Dam are geologically continuous over 8 km in an NNW-SSE direction and defined to a depth of 310m below surface.
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* • *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* • *The assumptions made regarding recovery of by-products.* • *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).* • *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* • *Any assumptions behind modelling of selective mining units.* • *Any assumptions about correlation between variables.* • *Description of how the geological interpretation was used to control the resource estimates.* • *Discussion of basis for using or not using grade cutting or capping.* • *The process of validation, the checking process used,*	• 1m composite samples coded to the mineralised domains were used as inputs to estimation. Only RC and diamond drilling samples used for estimation. • Ordinary Kriging (OK) was used to estimate gold grades into a 3-dimensional block model. Estimation parameters derived from modelled semi-variograms. Leapfrog software was used for the estimation. • For some of the mineralised zones categorical subdomains were created and estimated with Ordinary kriging. Thresholds for categorical subdomains are chosen from log probability plot inflections that are representative of the geological understanding of grade populations. Typically, only a single low-grade threshold was chosen to allow separation of lower grade and higher grade zones. This prevents smearing of high grades across the entire lode. • Lodes with a low number of samples or discrete lodes with a low coefficient of variation were interpolated by Inverse Distance Squared (ID2). • High grade cuts up to 80 g/t were applied to 1m composite data based on analysis of individual domains. • The parent block dimensions used were 20mN by 5mE by 10mRL with sub-cells of 1.25m by 1.25m by 1.25m. Drillhole spacing is approximately 50m between section and 50m along section. The parent block size was selected (approx. 50% of data spacing) using QKNA. • An orientated ellipsoid search was used to select data and was based on Kriging Neighbourhood parameters derived from the variography. • Estimation completed in 3 runs each with less restrictive search, and minimum sample parameters. The initial interpolation pass was used with a maximum range greater than the range of the principal direction of the modelled variograms. Maximum number of samples was 12, minimum was 4. Range increased progressively and the minimum number of samples reduced. • No estimation of deleterious elements was carried out. Deleterious elements have not been recorded during mining by previous operators Only Au was interpolated into the block model. • No assumptions have been made regarding recovery of by-products. Silver has not been routinely assayed. • Selective mining units were not modelled in the Mineral Resource • Only Au was estimated so correlation analysis was not possible • The deposit mineralisation was constrained by wireframes constructed using a 0.3 g/t Au cut-off grade in association with logged geology, particularly the presence of quartz veining and biotite-sulphide alteration. The wireframes, including sub-domains, were applied as hard boundaries in the estimate.

Criteria	JORC Code explanation	Commentary

	the comparison of model data to drillhole data, and use of reconciliation data if available.	• Grade capping was applied on a domain by domain basis due to the usually highly positively skewed grade populations
		• The validation was carried out by three methods:
		  ○ Visual comparison of block grades with nearby drill assay results on a section by section basis.
		  ○ Statistical comparison of estimated grades and composite grades on a domain by domain basis.
		  ○ Trend analysis of estimated block model grades versus composite grades on 40m northing and 20m vertical intervals.

Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages and grades were estimated on a dry in situ basis. No moisture values were reviewed.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The Mineral Resource has been reported at a 0.3 g/t Au cut-off within an optimised pit shell, based on assumptions about economic cut-off grades for open pit mining.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• It is intended to adopt a selective open cut mining practise at the deposit. • The MRE is reported under conditions that are considered to be RPEEE through open pit mining operations. Resources have been reported within a $5000 reporting pit shell derived from contractor derived mining costs, projected processing costs and pit wall angles determined from geotechnical assessment. Reporting shells were produced using diluted grades derived from Auto Stope Designer (ASD) shapes with 2.5m minimum width.
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	• Round Dam has no known reported metallurgical issues and several deposits along the trend (Walhalla, Federal Flag, Lady Eileen) have been previously mined. • Preliminary Metallurgical leach tests have demonstrated gold recoveries of >95% using standard CIL processing
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• Flora and Fauna surveys are complete. • Waste rock characterisation is ongoing
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method*	• Bulk density determinations were derived from measurements (immersion method) made on recent core samples drilled by OBM and from downhole density (gamma) measurements taken from selected RC and diamond holes. Downhole density measurements are

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td>used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.
The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.
Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</td><td>corrected for moisture content to obtain a dry bulk density.
Bulk density values used in the MRE were assigned by lithology and oxidisation and shown below in the table.
<table><tr><td>LITH</td><td>OX</td><td>TRANS</td><td>FRESH</td></tr><tr><td>Mafic</td><td>1.71</td><td>2.33</td><td>2.80</td></tr><tr><td>Pegmatite</td><td>2.00</td><td>2.59</td><td>2.63</td></tr><tr><td>Sediments</td><td>2.09</td><td>2.41</td><td>2.57</td></tr><tr><td>Ultramafic</td><td>1.78</td><td>2.50</td><td>2.90</td></tr><tr><td>Dolerite</td><td>1.71</td><td>2.33</td><td>2.80</td></tr></table></td></tr>
<tr><td>Classification</td><td>The basis for the classification of the Mineral Resources into varying confidence categories.
Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).
Whether the result appropriately reflects the Competent Person's view of the deposit.</td><td>Mineral Resources were classified in accordance with the Australasian Code for the Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC, 2012). The classification takes account of confidence in the geological interpretation, sample density and assay QAQC. In order to avoid a mosaic style of classification, solid wireframes were constructed to encompass areas considered to adequately fulfil the requirement to be classified as either, measured, indicated or inferred:
Measured – No areas of the current resource attained Measured status.
Indicated – Areas with drill spacing up to approximately 25m x 25mN up to 25m x 40m along strike and with reasonable confidence in the geological interpretation and grade continuity
Inferred – Areas with drill spacing up to approximately 50m x 50mN up to 50m x 80m along strike and where grade continuity is poorer as defined by a lower sample density, even though geological continuity may be apparent.
Areas of some lodes, particularly at depth have fairly low/no sample support and were not classified.
The input data is comprehensive and of sufficient quality for use in the MRE. Significant recent drilling, has confirmed the location and tenor of many historic drill-holes. Assay QAQC is of sufficient quality for the assays to be used in the MRE. There is sufficient understanding of the geology to support the current interpretation in terms of continuity.
The Mineral Resource estimate appropriately reflects the view of the Competent Person.</td></tr>
<tr><td>Audits or reviews</td><td>The results of any audits or reviews of Mineral Resource estimates.</td><td>The MRE has been internally peer reviewed and externally reviewed as part of an Independent Technical Experts Report.</td></tr>
<tr><td>Discussion of relative accuracy/ confidence</td><td>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.
The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.
These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</td><td>The Round Dam Mineral Resource estimate is considered to be reported with a reasonable degree of confidence. The data quality is good and the drillholes from recent drilling have detailed logs produced by qualified geologists. Historic logging has been reviewed.
The Mineral Resource statement relates to global estimates of tonnes and grade. Confidence in the estimate allows reasonable quantification of global metal content. The interpretation is considered globally robust but at a local scale, variations to ore geometry and/or grade can be expected.
The deposit is not currently being mined.</td></tr>
</table>

Section 3 Estimation and Reporting of Mineral Resources – Waihi

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* • *Data validation procedures used.*	• Data from EGL/OBM drilling captured into Field Marshall/Geobank Mobile logging software. Data sent from site and imported into SQL database via Geobank DBMS. Validation checks in SQL database are carried out to ensure data integrity is not compromised. • The data is verified by company geologists before being sent to the DBA for validation or passing Geobank Software validation protocols • Historic data has been verified by checking historical reports on the project. • The Competent Person has undertaken a number of validation checks on the database, using Micromine software which include, but are not limited to, checks for overlapping intervals, checks for missing data/records, visual checks on drill hole locations and traces to identify any possible survey issues. No major issues were detected.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	• Numerous site visits have been completed by the Competent Person with the following objectives: • View geology in existing open pit • View drilling operations • View and log drill core
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	• Waihi is located within the Coolgardie Domain of the Kalgoorlie Terrane, Eastern Goldfields Province, Western Australia. The deposit is hosted within Archaean mafic to ultramafic volcanic rocks of the Hampton Hill Formation, comprising a fractionated ultramafic to mafic volcanic sequence metamorphosed from lower to upper greenschist facies. Lithogeochemistry particularly Cr and Zr signatures obtained from pXRF provides a reliable method for differentiating volcanic units. Younging is established from east to west. Gold mineralisation is hosted within a metamorphosed mafic–ultramafic volcanic sequence that has undergone upper greenschist to lower amphibolite facies metamorphism and intense ductile deformation. Gold is primarily concentrated within biotite–quartz–sulphide assemblages developed during high-strain shearing. Early quartz veins occur throughout the sequence and, depending on local strain, are either preserved undeformed or, within high-strain domains, are folded, boudinaged, and locally transposed into foliation. Sulphides are dominated by pyrrhotite with minor pyrite and chalcopyrite and occur both disseminated within biotite schist and concentrated along vein selvages, with gold spatially associated. • Late stage E-W structures have been mapped and may offset the mineralised lodes slightly. These structures have also been exploited by thin pegmatite dykes. • Structural data from OBM drilling was used to guide the orientation of mineralised lodes where possible. • Inspection of core, RC chips and pit exposures shows the mineralisation to be associated with biotite and silica alteration and quartz-carbonate veining. • Geological continuity of mineralised strictures is well defined, although sometimes terminate abruptly, possibly due to the minor offsets caused by the E-W structures. The main lodes at Waihi are geologically continuous over 1.0 km and are known to extend a further 400m south to the Dexy prospect. Grade continuity is less extensive but well defined at a low cut-off grade (0.4g/t)
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan*	• The main lodes at Waihi are geologically continuous over 1.0 km in a N-S direction and defined to a depth of 400m below surface.

Criteria	JORC Code explanation	Commentary
	width, and depth below surface to the upper and lower limits of the Mineral Resource.	• The Homeward Bound Lodes are continuous over 0.3 km in a NW-SE direction and defined from surface to a depth of 360 m below surface.

Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.*
	• *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.*
	• *The assumptions made regarding recovery of by-products.*
	• *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).*
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*
	• *Any assumptions behind modelling of selective mining units.*
	• *Any assumptions about correlation between variables.*
	• *Description of how the geological interpretation was used to control the resource estimates.*
	• *Discussion of basis for using or not using grade cutting or capping.*
	• *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*
		• Ordinary Kriging (OK) was used to estimate gold grades into a 3-dimensional block model.
		• 1m composite samples coded to the mineralised domains used as inputs to estimation. Only RC and diamond drilling samples used for estimation.
		• Estimation parameters were derived from modelled semi-variograms. MicromineTM software was used for the OK estimation.
		• High grade cuts up to 40 g/t were applied to 1m composite data based on analysis of individual domains.
		• The parent block dimensions used were 10mN by 4mE by 10mRL with sub-cells of 1m by 0.5m by 1.0m. Drill hole spacing is approximately 20m between section and 20m along section in well drilled near surface portions of the deposit. The parent block size was selected (approx. 50% of data spacing) using QKNA.
		• An orientated ellipsoid search was used to select data and was based on Kriging Neighbourhood parameters derived from the variography.
		• Estimation completed in 3 runs each with less restrictive search, and minimum sample parameters. Locally varying search parameters were used and defined from the lode reference surface using Micromine's "Orientations from Wireframes" function. The initial interpolation pass was used with a maximum range at or slightly greater than the range of the principal direction of the modelled variograms. Maximum number of samples was 16, minimum was 6. A four-sector search was applied to maximise sample representivity in all directions. Range increased progressively and number of samples required reduced for the third run only. Grade thresholds were employed for some lodes to restrict the influence of high grade samples a significant distance from the block being estimated.
		• No estimation of deleterious elements was carried out. Deleterious elements have not been recorded during mining by previous operators. Only Au was interpolated into the block model.
		• Previous more recent MRE's have been completed in 2001 (Croesus) and 2020 (OBM).
		• The MRE makes use of RC grade control drilling from the previous mining episode in 2003 and recent RC Grade control drilling for the Open Pit mining at Waihi Central. Detailed production records are not available to make meaningful comparisons.
		• No assumptions have been made regarding recovery of by-products. Silver has not been routinely assayed.
		• Only Au was estimated so correlation analysis was not possible
		• The deposit mineralisation was constrained by wireframes constructed using a 0.4 g/t Au cut-off grade in association with logged geology, particularly the presence of quartz veining and biotite-sulphide alteration. The wireframes were applied as hard boundaries in the estimate.
		• Grade capping was assessed and applied to each domain. Additional distance limiting grade capping was applied on lodes where deemed appropriate.
		• The validation was carried out by three methods:
		  ○ Visual comparison of block grades with nearby drill assay results on a section by section basis.
		  ○ Statistical comparison of estimated grades and composite grades on a domain by domain basis.
		  ○ Trend analysis of estimated block model grades versus composite grades on 4/8m easting, 10/20m northing and 10m vertical intervals.

Criteria	JORC Code explanation	Commentary
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• Tonnages and grades were estimated on a dry in situ basis. No moisture values were reviewed.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• The underground Mineral Resource has been reported from fresh material within stope optimiser solids with dimensions of 10mN x 10mRL x 1.6mE at a diluted Au cut-off of 0.8 g/t. A small open pit is planned for Waihi Central and the classified material, above 0.5g/t, within the pit design are included in the Open Pit component of the MRE.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• It is intended to adopt a long hole open stoping underground mining method. • Open pit mining is by conventional drill, blast, load and haul. • Reasonable prospects for eventual economic extraction for the Waihi underground Resource was confirmed by applying Auto Stope Designer (ASD) solids with dimensions of 10mN x 10mRL, a minimum width of 1.6m and a diluted cut-off grade of 0.8 g/t.

Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	• Waihi has no known reported metallurgical issues and has been previously mined.
		• Results from previous processing (using CIP) have demonstrated that good gold recovery can be expected from modern conventional CIL processing methods.
		• Recent test work from Waihi ores give the following recoveries:
		  ○ Oxide – 94%
		  ○ Transitional – 92%
		  ○ Fresh – 90%
		• Additional metallurgical test work is ongoing

Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• The area is not located in an environmentally sensitive area. • Approvals are currently in place for open pit mining • Underground mining approvals are in progress.
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been*	• Bulk density determinations were derived from measurements (immersion method) made on recent core samples drilled by OBM. Results compared favourably with limited measurements taken by previous operators using the calliper method. • Bulk density values used in the resource were 1.9 t/m3 and 2.5 t/m3 for oxide and transitional material respectively. Densities for fresh ore is 2.91 t/m3. Fresh waste densities are based on lithology and range from 2.62 t/m3 (pegmatite) to 2.98 t/m3 (Ultramafic) • It is assumed there are minimal void spaces in the rocks within the Waihi deposit. Values applied in the Waihi block model are similar

Criteria	JORC Code explanation	Commentary
	measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit. • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	to other known bulk densities from similar geological terrains.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	• Mineral Resources were classified in accordance with the Australasian Code for the Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC, 2012). The classification takes account of confidence in the geological interpretation, sample density and assay QAQC. In order to avoid a mosaic style of classification, solid wireframes were constructed to encompass areas considered to adequately fulfil the requirement to be classified as either, measured, indicated or inferred: ○ Measured – No areas of the current resource attained Measured status ○ Indicated – Areas with drill spacing up to approximately 30 mE x 30 mN and with reasonable confidence in the geological interpretation and grade continuity ○ Inferred – Areas with drill spacing in excess of 30 mE x 30 mN and where grade continuity is poorer as defined by a lower sample density, even though geological continuity may be apparent. • The input data is comprehensive and of sufficient quality for use in the MRE. Significant recent drilling, covering the entire deposit, has confirmed the location and tenor of many historic drill-holes. Assay QAQC is of sufficient quality for the assays to be used in the MRE. There is sufficient understanding of the geology to support the current interpretation in terms of continuity. • The Mineral Resource estimate appropriately reflects the view of the Competent Person.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• The Waihi MRE has been internally peer reviewed and externally reviewed as part of an Independent Technical Experts Report.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• The Waihi Mineral Resource estimate is reported with a reasonable degree of confidence. The data quality is good and the drill holes from recent drilling have detailed logs produced by qualified geologists. Historic logging and core has been reviewed. • The Mineral Resource statement relates to global estimates of tonnes and grade. Confidence in the estimate allows reasonable quantification of global metal content. However, at a local scale there are risks associated with the estimation. The interpretation is considered globally robust but at a local scale, variations to ore geometry can be expected. • The deposit is not currently being mined. • Total Waihi Production records up to December 1996 are available. Total ore reserves were 761Kt @ 2.41 g/t for 59,000 ounces. Mill production was 704Kt @ 2.39 g/t for 54,000 ounces. Detailed bench by bench production data is not available.

Section 4 Estimation and Reporting of Ore Reserves

Criteria	JORC Code Explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• *Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.* • *Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.*	• All Mineral Resources were completed by Ora Banda Mining (OBM) using Ordinary Kriging and formed the basis for re-estimation of the Ore Reserve. • Riverina and Sand King underground Mineral Resources were depleted for mining to April 1, 2026. • The Waihi open pit and underground, Round Dam open pit were depleted for historical workings no further depletion was required no resource being mined as at the reporting date. • Mineral Resources are reported inclusive of the in situ Ore Reserves. The total Ore Reserve includes an estimated 600 kt at 0.9 g/t of economic material in surface stockpiles. • The Riverina underground Ore Reserve was estimated from a diluted Mineral Resource. The diluted Mineral Resource was created from the undiluted resource by constraining the model to a minimum width of 1.6 m with an additional 0.3m hanging wall and footwall dilution at a cut-off grade of 2.5 g/t with each lode evaluated on a spacing of 5 mN x 22 mRL. • The Sand King underground Ore Reserve was estimated from a diluted Mineral Resource. The diluted Mineral Resource was created from the undiluted resource by constraining the model to a minimum width of 1.6 m with an additional 0.3m hanging wall and footwall dilution at a cut-off grade of 2.4 g/t with each lode evaluated on a spacing of 5 mN x 22 mRL. • The Waihi Underground Ore Reserve was estimated from a diluted Mineral Resource. The diluted Mineral Resource was created from the undiluted resource by constraining the model to a minimum width of 1.6 m with an additional 0.3m hanging wall and footwall dilution at a cut-off grade of 2.2 g/t with each lode evaluated on a spacing of 5mN x 22 mRL. • The Waihi Open Pit Ore Reserve was estimated from a diluted Mineral Resource. The diluted Mineral Resource was created from the undiluted resource by constraining the model to a minimum width of 2.5 m at a cut-off grade of 0.8 g/ in an SMU of 2.5m wide 5x long and 5m high inclusive of unplanned dilution skins. • The Round Dam Open Pit Ore Reserve was estimated from a diluted Mineral Resource. The diluted Mineral Resource was created from the undiluted resource by constraining the model to a minimum width of 2.5 m at a cut-off grade of 0.5 g/t in an SMU of 2.5m wide 5x long and 5m high inclusive of unplanned dilution skins.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	• The Ora Banda site was initially visited by Mr Geoff Davidson on May 20th, 2020 and on several occasions subsequently. Mr Davidson is the Competent Person for portions of this Ore Reserve estimate relating to the open pit operations. Mr Davidson has not visited the Round Dam site; however is familiar with the general operating environment for the Ora Banda operations and has relied on site specific information provided by various subject matter experts within Ora Banda who have visited the site and have relayed information relevant to the preparation of the Ore Reserve estimate for Round Dam and Waihi. Mr Davidson is satisfied the conditions allowed for in this Ore Reserve estimate is consistent with the observations made during the site visit and information provided to him. • The site has been visited by Mr Leroy Savage on multiple occasions as he was formerly site based at the Siberia mining complex. He is currently part of Ora Banda Mining's corporate mining engineering team. Mr Savage is the Competent Person for Riverina, Sand King and Waihi Underground Ore Reserve estimate. Mr Savage has inspected representative diamond drill core for the Riverina, Sand King and Riverina for areas within the proposed mining envelope. In addition, inspections were made of the existing plant and associated infrastructure at Davyhurst. Mr Savage is satisfied the conditions allowed for Riverina Sand King and Waihi Underground Ore Reserve estimate are consistent with the observations made during various site visits. • The Competent persons are satisfied the parameters and modifying factors used to determine their respective Ore Reserve are appropriate.

Criteria	JORC Code Explanation	Commentary
Study status	• *The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.* • *The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.*	• This Ore Reserve estimate is an update for the DGP; the mining costs used to determine the economic mining envelopes and convert Mineral Resources into Ore Reserves are based on mining costs specific to the locations considered. The evaluation of the Ore Reserves is considered to be at a pre-feasibility level of confidence or better. Technically achievable mine plans were developed for each mining location and determined to be economically viable following the application of appropriate Modifying Factors and practical mining programs. The costs and parameters used are based on existing realised costs and current or recent hard dollar contracts implemented for the project or budget cost estimates received from contractors specifically for the project.
Cut-off parameters	• *The basis of the cut-off grade(s) or quality parameters applied.*	• Cut-off grade parameters were determined using realised costs from existing or recent project specific hard dollar contracts, as well as realised internal costs for OBM labour, plant and equipment. Ore haulage costs were based on contracts in place at the time. Processing costs were based on an assessment of realised costs to date and forward projections. Site general costs and administration overheads (G&A) were based on existing realised costs and forward projections specific to the mining operations. Selling costs were based on standard State Royalties and existing third party royalty agreements. Metallurgical process recoveries were based on recent demonstrated process plant performance and the most recent metallurgical test work for the relevant deposits. • Cut off grades for Waihi Underground, Sand King Underground and Riverina Underground reserves were based on a gold price of A$2,500 /oz. The cut off grade for Waihi Open Pit supports a gold price of A$2,400 /oz for High Grade and A$3,400 /oz for Low Grade. The cut off grade for Round Dam Open Pit supports a gold price of A$3,600 /oz for High Grade and A$5,000 /oz for Low Grade. The inclusion of underground mine Low Grade and Surface Stockpiles were based on a cut off grade determined at A$5,000 /oz. All Low Grade is blended with high grade to produce a head grade exceeding a cut of grade of 0.7 g/t based on a gold price of A$3,600/oz. • The cut off grade allows for ore haulage, crusher loading, processing, site G&A and corporate overhead contributions. The total of these costs were estimated to range between A$72 to A$89 per tonne depending on mining location. • The weight average processing recovery applied to Waihi material was 90% based on metallurgical testwork for oxide, transition and fresh material. The processing recovery applied to Riverina Underground was 88% and was based on metallurgical test work. The processing recovery applied to Sand King Underground was 87% and was based on metallurgical work. The processing recovery applied to Round Dam was 95% and was based on recent metallurgical work. The recovery performance was 92% through Davyhurst plant in FY26 to EOM March-26 for processing Riverina and Sand King ores. • Standard state royalties were included as well as an ad valorem third party royalty of 1% . • The cut off grade for the Riverina Underground was estimated to be 2.5 g/t for stoping. A cut off grade of 1.9 g/t was applied to ore from underground development. • The cut off grade for the Sand King Underground was estimated to be 2.4 g/t for stoping. A cut off grade of 2.0 g/t was applied to ore from underground development. • The cut off grade for the Waihi Underground was estimated to be 2.2 g/t for stoping. A cut off grade of 1.7 g/t was applied to ore from underground development. • The cut off grade for Round Dam was estimated to be 0.7g/t. The cut off grade for Round Dam Low Grade was estimated to be 0.5 g/t and is economic above A$5,000/oz. Low grade was treated as a blend material to produced a head grade above 0.7 g/t.

Criteria	JORC Code Explanation	Commentary
		• The cut off grade for Waihi was estimated to be 1.2 g/t. The cut off grade for Waihi Low Grade was estimated to be 0.8 g/t. • The respective cut-off grades were applied to the diluted Mineral Resource for each project. • The cut -off grade for surface stockpiles was estimated to be no less than 0.5 g/t. This material is economic above A$5,000/oz and is treated as a blend material to produced a head grade above 0.7 g/t. • Sand King Low Grade insitu material ranges from 0.6 g/t to 2.0 g/t. Riverina Low Grade insitu material ranges from 0.6 g/t to 1.9 g/t used. Waihi Low Grade insitu material ranges from 0.5 g/t to 1.7 g/t. Round Dam Low Grade material ranges from 0.5 g/t to 0.94 g/t
Mining factors or assumptions	• *The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).* • *The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.* • *The assumptions made regarding geotechnical parameters (e.g. pit slopes, stope sizes, etc), grade control and pre-production drilling.* • *The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).* • *The mining dilution factors used.* • *The mining recovery factors used.* • *Any minimum mining widths used.* • *The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.* • *The infrastructure requirements of the selected mining methods.*	<u>General</u> <u>Open Pit Mining Factors and Assumptions</u> • A combination of approved and preliminary mine designs were used as the basis for the Ore Reserve estimate. Preliminary designs were derived from economic envelopes determined from Whittle pit optimisations using slope parameters determined from site specific geotechnical assessment and modified to allow for ramps and minimum mining widths. The economics of the mine designs was validated in project specific cash flow models. The project average mining cost for Waihi pit was estimated to be A$12.06 per tonne and for Round Dam A$8.53 of material mined. These costs include provisions for grade control, drill, blast, load, haul, rehabilitation and OBM mine overheads. Cost were derived from recent contractor quotations for mining the Waihi pit and Round Dam pit and OBM mine overheads. • Conventional selective mining methods will be used for Waihi And Round Dam pits. The open pit operations will be mined using 120 t-class excavators and 90 t dump trucks. Waihi in-pit tails mining will also require the use of a low ground pressure dozer as part of the load and haul system. With the exception of existing in-pit backfill, historical waste dumps and in-pit tailings, all material mined will require drilling and blasting. The Competent Person considers the proposed mining method to be appropriate for the style and nature of the mineralisation. • Minimum mining widths of 20 m were allowed on all wall cutbacks adjacent to existing open pit workings. • The mining methods proposed are well-known and have been used successfully in the region. • Productivity rates considered historical performance and Industry standards. • Suitable and unhindered access exists to all open pits within this Ore Reserve. • The mining method contemplates selectively separating waste from the ore to minimise dilution and ore loss. Ore faces will be exposed by removing waste to the identified contact prior to removing the ore. • Subject matter experts comprising internal and external consultants were engaged to conduct a geotechnical analysis of the proposed excavation and waste rock storage methods. This analysis formed the basis of pit wall design criteria and tailings disposal methods proposed at Waihi. • Allowance was made for grade control activities, including in-pit reverse circulation drilling and face sampling. • Only the Indicated and Measured portion of the Mineral Resource was used to estimate the Ore Reserve. All Inferred material was treated as waste. Background grades were estimated into the mineral resource model and subsequently included as diluting material. The average grade of dilution included in the reserve were 0.16 g/t for

Criteria	JORC Code Explanation	Commentary
		Waihi and 0.11g/t for Round Dam. • Open pit mining blocks were diluted by applying a dilution skin to both footwall and hanging wall using Auto Stope Designer (ASD) functionality in Deswik™. The method also included internal and edge dilution resulting from forming practical mineable shapes using ASD. A skin thickness of 0.5 m was applied to Waihi to both hanging wall and footwall. A minimum mining width of 1.5 m was applied. The dilution parameters were determined from operational performance at previous OBM operations. Average dilution factors were estimated to be 27% for Waihi and 20% for Round Dam. Dilution was incorporated in the estimate at the background grades in the block model. The average grade of dilution for Waihi and Round Dam was 0.16 g/t and 0.11g/t respectively. • Planned ore loss was accounted for in the ASD process due to the variation between mineralised lode geometry and dig block geometry. In addition, a nominal 5% ore loss was applied for further mining losses occurring through normal operations. • Practical mine designs were completed for Waihi and Round Dam which formed the basis of scheduling and economic validation of the Ore Reserve. The strip ratio for Waihi was estimated to be 6.3 by mass inclusive of high grade and low grade ore. The strip ratio for Round Dam was estimated to be 9.9 by mass inclusive of high grade and low grade ore. • Most of the infrastructure required for the operations is already established at the DGP, including a processing plant and associated infrastructure, camp, airstrip, offices, power reticulation, borefields and coreyards. • Waihi Offices and Workshop complex for open pit operations is in place. Nominal provisions were made for site infrastructure. • Round Dam is 15km from Davyhurst and will require the establishment of an offices and workshop complex for the open pit operations. Provisions were made for site infrastructure and establishment. <u>Underground Mining Factors and Assumptions</u> Riverina Underground • The mining method proposed for Riverina is narrow-vein long hole open stoping using up-hole-benching techniques. This method has been successfully implemented at Riverina since 2023 along with similar styled deposits in the West Australian Goldfields region. The decline design parameters are nominally 5.5m wide x 5.7m high with an average design gradient of 1:7 down. Ore development has been planned at 4.5m wide x 4.5m high. The average floor to floor distance between levels will be 22 metres, with an average stope panel height of approximately 17.5 metres. • OBM geotechnical engineer conducted a geotechnical analysis to an appropriate level of detail. This forms the basis of stoping parameters and development ground support requirements. Stopes will be approximately 40m long x 22m high within the stable envelope of the unsupported span determined from geotechnical analysis. Provision is made for full height rib pillars between stopes and sill pillars, which will be reevaluated upon stope performance. This provision equates to a recovery of 86%. An additional 5% stope ore loss was also provisioned for operating losses. The overall mining recovery is estimated to be 83%. • The reserve inventories will be mined in proximity to known historical underground workings. The design has been stood-off an appropriate distance from known voids. Probe drilling and resultant dewatering will be undertaken prior to developing near any known voids. Appropriate procedures will be implemented during the mining episode when mining around historical underground voids.

Criteria	JORC Code Explanation	Commentary
		• Overall unit mining costs for the underground was estimated to be A$204/t ore inclusive of sustaining capital. • Stopes were defined by applying a 2.5 g/t cut-off to the diluted Mineral Resource. The cut-off allows for production stoping activities as well as load and haul downstream processing and sales. • A minimum stope mining width of 1.6m was applied in the dilution modelling process, with a dilution skin then applied. The dilution allows for a skin of 0.3 m on both hanging wall and footwall. In addition, a nominal allowance of 20% dilution at 0g/t was included to account for unidentified dilution sources. The global dilution of the diluted resource was estimated to be 51% of material. Dilution being all included material less than 0.6 g/t. • A cut off grade of 1.9 g/t was applied to ore drive development on a cut by cut basis. This cut-off allows for ore development mining costs, haulage, processing and sales. • Inferred material was not considered in defining the stoping envelopes; however, due to practical stope mining geometries a small portion of Inferred material was included within the Underground Ore Reserve. This material was included at the edges of the mining envelope and equates to approximately 1% of the Riverina Underground Ore Reserve inventories. • Grade control will be conducted primarily via face sampling and underground diamond drilling. • Infrastructure required for the underground operations is already established at Riverina. This includes a mining camp, offices, fuel farm, workshops, core shed, water storage & pump stations, diesel generated power and conventional underground mine services. Sand King Underground • The mining method proposed for Sand King is narrow-vein long hole open stoping using up-hole-benching techniques. This method has been successfully implemented at Sand King and similar styled deposits in the West Australian Goldfields region. The decline design parameters are nominally 5.5 m wide x 5.7 m high with an average design gradient of 1:7 down. Ore development has been planned at 4.5m wide x 4.5m high. The average floor to floor distance between levels will be 22 metres, with an average stope panel height of approximately 17.5 metres. • Internal Geotechnical Engineers conducted a geotechnical analysis to an appropriate level of detail. This forms the basis of stoping parameters and development ground support requirements. Stopes will be approximately 40m long x 22m high within the stable envelope of the unsupported span determined from geotechnical analysis. Provision is made for full height rib pillars between stopes, sill pillars will be evaluated upon stope performance. An additional 5% stope ore loss was also provisioned for operating losses. The overall mining recovery is estimated to be 82%. • Overall unit mining costs for the underground was estimated to be A$149/t ore, inclusive of sustaining capital. • Stopes were defined by applying a 2.4 g/t cut-off to the diluted Mineral. The cut-off allows for production stoping as well as load and haul downstream processing and sales. • A minimum stope mining width of 1.6m was applied in the dilution modelling process, with a dilution skin then applied. The dilution allows for a skin of 0.3m on the hanging wall and 0.3m on the footwall. In addition, a nominal allowance of 5% dilution was included to account for unidentified dilution sources. The global dilution of the diluted resource was estimated to be 23% of material and the global average grade of dilution was estimated to

Criteria	JORC Code Explanation	Commentary
		be 0.25 g/t. Dilution being all included material less than 0.6 g/t. • A cut off grade of 2.0g/t was applied to ore drive development on a cut by cut basis. This cut-off allows for ore development mining costs, haulage, processing and sales. • Inferred material was not considered in defining the stoping envelopes; however, due to practical stope mining geometries a small portion of Inferred material was included within the Underground Ore Reserve. This material was included at the edges of the mining envelope and equates to approximately 3% of the Sand King Underground Ore Reserve inventories • Grade control will be conducted primarily via face sampling and underground diamond drilling. • Infrastructure required for the underground operations is already established at Sand King Underground this includes the Davyhurst mining camp, site offices, fuel farm, workshops, core shed, water storage & pump stations, diesel generated power and conventional underground mine services. Waihi Underground • The mining method proposed for Waihi is narrow-vein long hole open stoping using up-hole-benching techniques. This method has been successfully implemented at Sand King & Riverina and similar styled deposits in the West Australian Goldfields region. The decline design parameters are nominally 5.5 m wide x 5.7 m high with an average design gradient of 1:7 down. Ore development has been planned at 4.5m wide x 4.5m high. The average floor to floor distance between levels will be 22 metres, with an average stope panel height of approximately 17.5 metres. • Internal Geotechnical Engineers conducted a geotechnical analysis to an appropriate level of detail. This forms the basis of stoping parameters and development ground support requirements. Stopes will be approximately 40 m long x 22 m high within the stable envelope of the unsupported span determined from geotechnical analysis. Provision is made for full height, 5 m along strike, rib pillars between adjacent stopes on each level. There are isolated areas in which stopes > 7.5 m wide occur. In these areas, stope strike spans are limited to no more than 25m and rib pillar strike spans of 10m. Sill pillars have been considered via a stope recovery of 72% where stoping extends more than 4 levels down dip on a mineralised lode. A 5% stope ore loss was also included for normal operational losses. A weighted average extraction ratio was estimated to be 82% across the Waihi underground. • The Waihi Underground Geotechnical Report provides stope and pillar analysis and guidance and formed the basis for the stope parameters used. Crown pillars were designed no less than 10m high for stopes <5 m wide and 15 m crown pillars for stopes >5m wide. The 15 m crown pillars include drill drives from which rockmass classification can be determined and suitable ground support can be installed if required. • After the mine achieves commercial production, the overall unit mining costs for the underground was estimated to be A$193/t ore, inclusive of sustaining capital. • Stopes were defined by applying a 2.2 g/t cut-off to the diluted Mineral Resource. The cut-off allows for production stoping as well as load and haul downstream processing and sales. • A minimum stope mining width of 1.6 m was applied in the dilution modelling process, with additional allowance for a dilution skin. The dilution allows for a skin of 0.3 m on the hanging wall and 0.3 m on the footwall. In addition, a nominal provision for unplanned dilution of 20% @ 0 g/t for stopes < 3.5 m wide (57 stopes) and 10% @0g/t for stopes >3.5m wide (37 stopes) was also included as a contingency to all stoping panels. The global planned dilution of the diluted resource was estimated to be 29% of material and the global average grade of dilution was estimated to be 0.14 g/t. Dilution was defined as all included material less than 0.5 g/t.

Criteria	JORC Code Explanation	Commentary
		• A cut off grade of 1.7 g/t was applied to ore drive development on a cut by cut basis. This cut-off allows for ore development mining costs, haulage, processing and sales. • Inferred material was not considered in defining the stoping envelopes; however, due to practical stope mining geometries a small portion of Inferred material was included within the Underground Ore Reserve. This material was included at the edges of the mining envelope and equates to approximately 2% of the Waihi Underground Ore Reserve inventories • Grade control will be conducted primarily via face sampling and underground diamond drilling. Some infrastructure required for the Waihi underground operations is already established or being established as part of the open pit operation. Additional infrastructure costs for Waihi Underground have been considered for additional site offices and workshop, Portal establishment, additional magazines, fuel farm, water storage & pump stations, diesel generated power and conventional underground mine services.
Metallurgical factors or assumptions	• *The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.* • *Whether the metallurgical process is well-tested technology or novel in nature.* • *The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.* • *Any assumptions or allowances made for deleterious elements.* • *The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole.* • *For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?*	• The process for treating ore is conventional carbon-in-leach (CIL) with some gold recovered via gravity circuit. This is a standard gold processing flowsheet used throughout the industry for this style of mineralisation. • A process recovery of 88% was applied to Riverina Underground based on metallurgical testing of samples taken from within the proposed mining envelope. This is confirmed by the Davyhurst processing performance. • A process recovery of 87% was applied to Sand King Underground based on metallurgical testing of samples taken from within the proposed mining envelope. This is confirmed by the Davyhurst processing performance. • A weight average process recovery of 90% was applied to Waihi based on metallurgical testing of oxide, transition and fresh samples taken from within the proposed mining envelope. This is in line with historical open pit recovery at Davyhurst processing plant. • A process recovery of 95% was applied to Round Dam open pit and was based on preliminary metallurgical testing of samples taken from areas proximal to the mining envelope. • The process plant has a nominal throughput rate of 1.2 Mtpa based on a grind size of 106 µm. The process plant has been successfully operated, and further operational improvements are proposed.
Environmental	• *The status of studies of potential environmental impacts of the mining and processing operation. Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.*	• Riverina, Sand King projects as well as the Waihi open pit have approved Mining Proposals along with clearing permits and appropriate water licences. • For Riverina, Sand King and Waihi the flora and fauna baseline studies have been completed for areas that may potentially be influenced by mining operations contemplated in this Ore Reserve estimate. No conservation significant taxa were identified as being at risk. • Searches of Indigenous and European State Heritage Registers have not identified any sites that require active management. • Both historical and recent geochemical data indicate the majority of waste rock mass is non-acid forming. Sulphidic sedimentary units at Riverina will be intersected occasionally by underground development and will be classed as Potential Acid Forming (PAF) . The storage of PAF waste is being managed through co-mingling with Acid Neutralising Capacity(ANC) waste in accordance with the approved Mine Closure plan. Test work on Waihi tails has determined that there is no PAF risk. Provisions for the management of PAF were allowed for in this estimate. Test work on Sand King underground has reported that there is no PAF risk. Geochemical testing of Round Dam waste rock is ongoing, and no condition has been identified that cannot be mitigated through conventional methods of waste rock management. • Tailings from ore processing will be stored within the existing Tailings Storage Facility (TSF). Allowance has been made for expansions to this facility as required by the mine plan. • The MDCP addendum for Waihi underground mine and infrastructure has been submitted for approval. The

Criteria	JORC Code Explanation	Commentary
		regulator is familiar with the project with the approval expected to be received prior to planned commencement. • The company is currently advancing through the regulatory approval phase of the Round Dam Project which seeks the necessary environmental approvals to support its planned mining development. As part of this process, it is undertaking comprehensive baseline studies to collect environmental data which will form the foundation for impact assessments and management strategies. • At this time, the Competent Person is not aware of any condition relating to the propose mining of Round Dam that will prevent the permitting and approval of the project.
Infrastructure	• *The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.*	• The majority of required infrastructure is established and commissioned. Capital provisions for Waihi Underground and Round Dam infrastructure were made. These sites are within 15 km of existing Davyhurst complex. Small temporary satellite facilities for Waihi will be required and preliminary provisions were made within the financial analysis for these facilities. • Additional accommodation camp capacity has been constructed at both Davyhurst(387 rooms) and Riverina (220 rooms). Communication is established at all operating locations. • The operation is currently serviced by an existing airstrip adjacent to the Callion mine workings, an airstrip at Riverina as well as from the Kalgoorlie airport. • Round Dam WRL footprints are over both Mining and Exploration tenements owned by a subsidiary of OBM. OBM is in the process of making an application for a mining lease to facilitate associated mining infrastructure. The Competent Person is not aware of any condition that would prevent the granting of the mining lease. • The existing TSF has sufficient capacity for in excess of two years of production at current throughput rates and is not considered a constraint on the current Ore Reserve. A $2/t allowance has been included in the Ore Reserve cost assumptions to account for future tailings disposal infrastructure beyond the existing facility. Future TSF site selection is currently under review, with a feasibility study and regulated approval process required prior to development of any new facility.
Costs	• *The derivation of, or assumptions made, regarding projected capital costs in the study.* • *The methodology used to estimate operating costs.* • *Allowances made for the content of deleterious elements.* • *The source of exchange rates used in the study.* • *Derivation of transportation charges.* • *The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.* • *The allowances made for royalties payable, both Government and private.*	• Sustaining capital was allowed for in the financial analysis . • Underground mine startup capital costs are based on the recent Sand King and Riverina actuals with the application of inflation and 10% contingency. • Open Pit mine startup capital costs for Waihi are based on the recent Waihi tender and FID with the application of 15% contingency. • Sand King, Riverina, Waihi Underground and Waihi Open Pit mining costs were estimated from hard dollar contracts for the project current at the date of the Ore Reserve. • Round Dam mining costs were estimated from practical designs and schedules and budget level cost estimates specific to the project and provided by an established mining contractor. • Ore haulage costs were estimated from hard dollar contracts for the project current at the date of the Ore Reserve • Power, diesel and accommodation costs were based on current realised costs and FY26 budget forecasts. Staff costs were based on current employment contracts in place. • Processing operating costs were based on current performance and FY26 budget forecasts. • Unit costs for haulage, processing and site overheads were estimated based on scheduled utilisation of process capacity using material above the economic cut-off grade. • Waihi Open Pit Mining operations specific overhead costs were included based on recent FID estimates and FY26 Budget. • Sand King and Riverina operations specific overhead costs were included based on FY26 Budget. • Corporate overhead were assigned based on the estimated costs attributable to operations. • Any identified deleterious elements within ore and waste rock have been considered in the design, performance

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		and costing. • All costs were quoted and compiled in Australian dollars. • The standard WA state government royalty for gold was allowed for. Third party royalties of 1% ad valorem were applied in the financial analysis.
Revenue factors	• *The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.* • *The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.*	• Revenue calculations were based on detailed mine plans and mining factors including provision for dilution and ore loss. • A financial analysis was completed on A$3,600/oz before selling costs and is below the current spot price as of the date of this announcement.
Market assessment	• *The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.* • *A customer and competitor analysis along with the identification of likely market windows for the product.* • *Price and volume forecasts and the basis for these forecasts.* • *For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.*	• There are no known major gold producers expecting to influence the global supply of gold over the period of the project. • Demand for gold is expected to be subject to usual global factors.
Economic	• *The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc.* • *NPV ranges and sensitivity to variations in the significant assumptions and inputs.*	• The Ore Reserve estimate was validated using a financial model prepared to a budget level of accuracy for the purpose of project evaluation using realised costs to date and existing contract pricing. • All inputs from open pit and underground operations, processing, transportation and sustaining capital as well as contingencies have been scheduled and evaluated to generate a life of mine financial model. • Economic inputs have been sourced from operational budgets, contractors and DGP accounts for internal costs. • Unit costs for ore haulage, processing and site overheads were estimated based on full utilisation of process plant capacity using material above the economic cut-off grade. • No escalation of gold price or costs is included. • A discount rate of 8% pa was applied. • The NPV of the Project is positive at an assumed commodity price of A$3,600/oz and the Competent Persons are satisfied that the project economics retains a suitable margin of profitability based on the reserve assumptions. • A sensitivity analysis of variable factors such as cost, gold price, grade and metallurgical recovery were conducted at an operational level and the operation demonstrated an acceptable level of robustness.
Social	• *The status of agreements with key stakeholders and matters leading to social licence to operate.*	• The Competent Persons understand that the majority of agreements for Round Dam Project are in place with key stake holders; however, negotiations with traditional owners as well as the management of lithium pegmatites that are in joint ownership with a third party and are associated with Round Dam are still to be concluded.
Other	• *To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:* • *Any identified material naturally occurring risks.* • *The status of material legal agreements and marketing arrangements.* • *The status of governmental agreements and*	• Riverina, Sand King and Waihi Open pit are active mines. • A formal process to assess and mitigate naturally occurring risks will be undertaken prior to execution of new mining projects. Currently, all naturally occurring risks are assumed to have adequate prospects for control and mitigation. • Riverina, Sand King and Waihi mining operations are contained within granted mining leases 100% owned by Ora Banda Mining. Round Dam pits are entirely on a granted Mining Lease 100% owned by Ora Banda Mining, the designed WRL's footprints extend over both Mining and Exploration tenements 100% owned by Ora Banda Mining .

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	approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.	OBM is in the process of making an application for a mining lease to facilitate associated mining infrastructure • All approvals are in place for Riverina Underground, Sand King Underground and Waihi Open Pit which are currently operating. • The MDCP addendum for Waihi underground mine and infrastructure has been submitted for approval. The regulator is familiar with the project with the approval expected to be received prior to planned commencement. • The company is currently advancing through the regulatory approval phase of the Round Dam Project which seeks the necessary environmental approvals to support its planned mining development. As part of this process, it is undertaking comprehensive baseline studies to collect environmental data which will form the foundation for impact assessments and management strategies. • Discussions with Traditional Owners over Round Dam are currently in progress. No provision was made at this time for royalty payments in this regard. The final agreed terms are not expected to be material to Round Dam portion of this Ore Reserve estimate. • OBM is a minor stakeholder to lithium baring pegmatites within or proximal to the Round Dam mineralisation. No specific provision was made to account for this material. Final WRL configuration and separate stockpiling will contemplate this mineralisation in the next phase of the study. Any additional cost associate with the management of this material is not considered material to this Ore Reserve by the Competent Person.
Classification	• *The basis for the classification of the Ore Reserves into varying confidence categories.* • *Whether the result appropriately reflects the Competent Person's view of the deposit.* • *The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).*	• The Proved and Probable Ore Reserves were based on that portion of the Measured and Indicated Mineral Resource respectively within the mine design that may be economically extracted and includes an allowance for dilution and ore loss. • The result appropriately reflects the Competent Person's view of the deposit and how it will be exploited. • The Ore Reserve is inclusive of surface stockpiles above the relevant cut-off grade and total 600 kt at 0.9 g/t . All surface stockpiles were classified as Proved. • Measured material was classified as Proved in the Ore Reserve. • Inferred material within the Riverina Underground Ore Reserve equates to 12,634t at a grade of 1.62g/t. This material is included at the edges of the mining envelope and equate to 0.7% of the Ore Reserve inventories. • Inferred material within the Sand King Underground Ore Reserve equates to 36,064t at a grade of 2.0g/t . This material is included at the edges of the mining envelope and equate to 2.6% of the Ore Reserve inventories. • Inferred material within the Waihi Underground Ore Reserve equates to 55,202t at a grade of 2.01g/t . This material is included at the edges of the mining envelope and equate to 2.9% of the Ore Reserve inventories. • Within the open pit portion of the Ore Reserve material was reclassified based on the dominant value within each SMU. Only SMU dig blocks with a dominant value of Indicated were included in the Ore Reserve, noting that there was no Mineral Resource classified as Measured withing the mining envelope.
Audits or reviews	• *The results of any audits or reviews of Ore Reserve estimates.*	• The Ore Reserve estimate, along with the mine design, life of mine plan and modifying factors, has been peer-reviewed by both internal and external parties.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the*	• The design, schedule and financial model on which the Ore Reserve is based was completed to a pre-feasibility level of accuracy or better for project evaluation purposes. Costs were taken from existing contracts, contractor budget quotations and internal realised costs reported from OBM accounts. • The Ore Reserve is a global estimate based on the Mineral Resource Estimate. • There is a degree of uncertainty associated with geological estimates. The Reserve classifications reflect the levels of geological confidence in the estimates. • There is always a degree of uncertainty regarding estimates of impacts of natural phenomena including geotechnical assumptions, hydrological assumptions and the modifying mining factors, commensurate with the current status of the project. The Competent Person is satisfied that the analysis used to generate the modifying factors is appropriate, and that a suitable margin exists under current market conditions to allow for the Reserve estimate to remain economically viable despite reasonably foreseeable negative modifying factor results.